

Continuation of the Appendices to the Thesis :

" ACCEPTANCE SAMPLING : ROBUST ALTERNATIVES FOR
SAMPLING BY VARIABLES "

V O L U M E (II)

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APPENDIX (B.1.)

Sub-Program Name : ' CONVOL '

Purpose and general description :

This Routine :

1. produces the smoothed-out version of the probability distn mixing both Discrete and continuous parts in the convolution;
2. compresses the convolution DP(.) onto the single probability SP(.) ; and similarly for DPD(.) onto SPD(.), which in turn are the "discrete contributions" to the smoothed-out distribution. These discrete contributions, or "jumps", are spread out in the distribution by the convolution process of course, and are irretrievable by the simple process of just subtracting the TRINOMIAL terms.
3. Collapses the SP(.)+s that are too small or zeros such that their cumulative sum is below the TOLERance level defined by TOLER...

The Descriptions of the Subroutine Parameters are:

- (1) INPUT Parameters :
- N the number of probability cells .
 - SCALE the scaling factor adjusted with every compression of the convolved distribution ,initially set at 1/N .
 - QMIN,QMAX minimum and maximum values of average quality score initially set at 0,1 respectively .
 - TOL Maximum Tolerable total of absolute discrepancies in the probability that can be forsaken for compression.
- (2) OUTPUT Parameters :
- QMIN,QMAX give the values after compression processes .
 - SCALE the scaling factor of the distribution after compressions.
 - KOUNT Controls number of convolutions so as to meet the required number determined by the INPUT parameter KN .
 - AMU the mean of the Normal Distribution such that the proportion below 0.0 is equal to p0 (predetermined).
 - SIGMA standard deviation for Normal Dist. (set equal to 1) .
 - IFault Failure parameter supposed to score 0 if subroutine is successful ,and a positive integer otherwise .
 - IFLAG a checking indicator to show whether cell compression has taken place or not (0 or 1) .It could also be used as a counter for number of compressions made as herebelow.

SUBROUTINE CONVOL(N , SCALE ,QMIN ,QMAX ,TOL ,IFLAG,KOUNT,KN
 * ,AMU ,SIGMA ,IFault)
 COMMON/CON/ CP(0:101),SP(0:101),SPD(0:101),CPD(0:101)
 REAL DP(0:201),DPD(0:201)
 LOGICAL WITH1,WITHN

```

IFLAG=0
KOUNT=0
NN=N + N + 1
100 KOUNT=KOUNT + 1
DO 10 L=0,NN
DP(L)=0.0
DPD(L)=C.C
10 CONTINUE

LIM1=0
LIM2=N+1
IF(QMIN .EQ. 0.0) LIM1=1
IF(QMAX .EQ. 1.0) LIM2=N
LIM3=LIM1 + 1
LIM4=LIM2 + N
DO 500 K=LIM3,LIM4
LIM5=MAX0(LIM1,K-LIM2)
LIM6=MIN0(LIM2,K-LIM1)
DO 450 I=LIM5,LIM6

Distributing the continuous part of probabilities over 2 intervals
assuming Uniformity within each cell

AHALF=0.5*SP(I)*SP(K-I)
DHALF=0.5*SPD(I)*SPD(K-I)
DP(K)=DP(K) + AHALF
DP(K-1)=DP(K-1) + AHALF
DPD(K)=DPD(K) + DHALF
DPD(K-1)=DPD(K-1) + DHALF
450 CONTINUE
KN1=K - N
LIM7=LIM2+1
K1=K-1
WITH1=LIM1 .EQ. 1 .AND. K.LE.LIM7
WITHN=LIM2 .EQ. N .AND. KN1 .GE. LIM1
IF(.NOT. WITH1) GO TO 460
DP(K1)=DP(K1)+SP(0)*SP(K1)*2.
DPD(K1)=DPD(K1)+SPD(0)*SPD(K1)*2.
460 IF(.NOT. WITHN) GO TO 500
DP(K)=DP(K)+SP(N+1)*SP(KN1)*2.
DPD(K)=DPD(K)+SPD(N+1)*SPD(KN1)*2.0
500 CONTINUE
IF(LIM1 .NE. 1 .OR. LIM2.NE. N) GO TO 600

Distribute Discrete probablties at boundry over neighbrng intervls

ONE = SP(0)*SP(N+1)
DP(N)=DP(N) + ONE
DP(N+1)=DP(N+1) + ONE
DPD(N)=DPD(N) + SPD(0)*SPD(N+1)
DPD(N+1)=DPD(N+1) + SPD(0)*SPD(N+1)

600 DP(0) = DP(0) + SP(0) * SP(0)
DP(NN)=DP(NN) + SP(N+1) * SP(N+1)
DPD(0) = DPD(0) + SPD(0) * SPD(0)
DPD(NN) = DPD(NN) + SPD(N+1)*SPD(N+1)

These were the End terms dealt with in either disc. or contin. case
---
Now , Compressing DP( ) on to SP( )

SP(0) = DP(0)
DCUM=SPD(0)
CUMCP= SP(0)
DO 100 K= 1, N
K2 = K+K
SP(K) = ( DP(K2-1) + DP(K2) )
SPD(K)=(DPD(K2-1) + DPD(K2) )
DCUM=DCUM+SPD(K)
CPD(K)=DCUM
CUMCP=CUMCP+SP(K)
CP(K)=CUMCP
100 CONTINUE
SP(N+1) = DP(N+N+1)

SPD(N+1)=DPD(N+N+1)
DCUM=DCUM+SPD(N+1)
CPD(N+1)=DCUM
CUMCP=CUMCP+SP(N+1)
CP(N+1)=CUMCP
IF(CUMCP .LE. 1.0000001.AND.CUMCP.GT.0.99999999 ) GO TO 110
IF(CUMCP.LE.1.00001.AND.CUMCP.GT.0.999995) GO TO 120
IF AULT=3
STOP ' In CONVOL ; CUMCP .not. "reasonably" 1.0 ...STOPPED'
120 CPP=0.0
DO 103 II=0,N+1
SPP=SP(II)/CUMCP
SPPD=SPD(II)/CUMCP
CPP=CPP+SPP
SP(II)=SPP
SPD(II)=SPPD
103 CONTINUE

Collapsing, or Truncation, of Distribution

110 CONTINUE
PTOT = C.C
NOVR2= N/2 + 1
NMIN = 0
NMAX = N+1
210 I= NMIN
J= NMAX
LEFT=NMAX-NMIN
IF(LEFT .EQ. NOVR2 ) GO TO 320
IF( SP(I) .LT. SP(J) ) GO TO 290
PTOT = PTOT + SP(J)
IF(PTOT.GT.TOL) GO TO 320
INCR = -1
NMAX = NMAX + INCR
GO TO 310
290 PTOT = PTOT + SP(I)
IF(PTOT.GT.TOL) GO TO 320
INCR = 1
NMIN = NMIN + INCR
310 IF( PTOT .LT. TOL ) GO TO 210
320 CONTINUE
LEFT=NMAX-NMIN
IF( LEFT .GT. NOVR2) GO TO 400
IF(NMIN .GE. NOVR2) NMIN=N/2

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330 IF(NMAX.LT.NOVR2) NMAX=NOVR2
   IFLAG=IFLAG + 1
   QMIN = QMIN + NMIN*SCALE
   SCALE=SCALE * 0.5
   QMAX = QMIN + N * SCALE
   CP(N+1)= 1.0
   NMIN2=2*NMIN
   DO 350 I=1,N
   SP(I)=DP(NMIN2+I)
   SPD(I)=DPD(NMIN2+I)
350 CONTINUE
   STOT1=0.0
   DTOT1=0.0
   DO 360 M=C,NMIN2
   STOT1=STOT1+DP(M)
   DTOT1=DTOT1+DPD(M)
360 CONTINUE
   STOT2=0.0
   DTOT2=0.0
   DO 370 M=NMIN2+N+1,NN
   STOT2=STOT2+DP(M)
   DTOT2=DTOT2+DPD(M)
370 CONTINUE
   SPD(0)= DTOT1
   SPD(N+1)= DTOT2
   SP(0)=STOT1
   SP(N+1)=STOT2
400 CONTINUE
   IF(KOUNT.GE.KN) GO TO 1000
   GO TO 105
1000 RETURN
      END
C ----- E n d -----

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APPENDIX (B.2.)

```

C
C
C Name of Program : " DRAMP.FOR "
C -----
C
C Purpose :
C -----
C This FORTRAN Program is responsible for the production of the
C numerical distributions for the r.v. of the Ramp average quality
C function . It prepares the information for and then uses the FORTRAN
C subroutine CONVOL . This is as discussed theoretically in Chapter III .
C The results of this Program are shown in Appendix ( ) in the form of
C tables of the distribution for different sample sizes .
C
C
C Subroutines Called by the Program :
C -----
C CONVOL performs the Convolution process ( It is listed
C and explained in appendix() ).
C INVPHI (or GAUINV) for finding the Normal percentage point given
C the cumulative probability .
C ALNORM the function that evaluates the Cumulative probability
C for a given percentage point of a standard Normal r.v.
C ( Due to I.D. Hill Applied Statist. Vol 66 )
C
C -----
C
REAL CDMTRX(0:101,8),DISCON(0:101,8),DIS(8)
REAL QMN(8),SCAL(8),QMX(8),P1(8)
INTEGER IFLG(8)
REAL DCUMU(8)
COMMON/CON/CP(0:101),SP(0:101),SPD(0:101),CPD(0:101)
N=100
DO 2000 K0=2,7
KN=K0
DATA NOUT,NOUT2/1,0/
DATA A/C,0/
DATA B1,SB,BN/0.5,0.2,1.9/
DATA AMU1,SMU,AMUN/2.3,-0.1,1.2/
NSIZE=2**KN
IAMU1=(10.*AMU1+0.1)
ISMU =((10.*SMU)+0.1)
IAMUN=(10.*AMUN+0.1)
WRITE(5,*) IAMU1,IAMUN,SMU
WRITE(NOUT,9)
AMUU=AMU1-SMU
DO 550 IMUU=IAMU1,IAMUN,-1
AMUU=AMUU+SMU
AMAMU=A-AMUU
PC=ALNORM(AMAMU, .FALSE.)
WRITE(NOUT,800) KN
WRITE(NOUT,401) AMUU,PC

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WRITE(NOUT,411) B1,SB,BN
B=B1-SB
DO 450 JB=1,8
B = B + SB
BSTD=B - AMUU
P1(JB)= ALNORM( BSTD ,.FALSE.) - PO
TOLER=0.001
QMIN=0.0
QMAX=1.0
100 SCALE=1.0/FLOAT(N)
QL = QMIN
QUU=QU
XU = QU * ( B - A)
XSTD=XU - AMUU
CP(0) = ALNORM(XSTD, .FALSE.)
SP(0) = CP(0)
DO 100 I=1,N
QU = QU + SCALE
QUU=QU

C
C The functional value given for XU below is for Ramp quality function
C It could possibly be replaced by a suitable value for the Normality
C or Logistic Quality Function ....
C
XU = QU * ( B - A)
XSTD=XU - AMUU
CP(I) = ALNORM(XSTD, .FALSE.)
SP(I) = CP(I) - CP(I-1)
SPD(I)=C.C
CPD(I)=SP(0)
100 CONTINUE
CP(N+1)=1.0
SP(N+1)=1.0 - CP(N)
P2=SP(N+1)
NSIZ=2**KN
DCUMU(JB)=(P0+P2)**NSIZ
SPD(0)=SP(0)
SPD(N+1)=SP(N+1)
CPD(N+1)=CPD(N)+SPD(N+1)
C NOW WE'VE THE INITIAL DATA FOR THE CONVOLUTION
Kont=KN
IFault=C
CALL CONVOL(N,SCALE,QMIN,QMAX,TOLER,IFLAG,KOUNT,Kont,AMU,SIGMA,
* IFault)
IF(IFault.EQ. 3) STOP 'PROG stopped,in CONVOL: CUMCP .NE. 1.0 !!'
DISCON(0,JB)=SPD(0)
CDMTRX(0,JB)=SP(0)-SPD(0)
DIS(JB)=SPD(0)
DO 290 I=1,N
DISCON(I,JB)=SPD(I)+DISCON(I-1,JB)
DIS(JB)= DIS(JB)+SPD(I)
CDMTRX(I,JB)=CDMTRX(I-1,JB)+SP(I)-SPD(I)
290 CONTINUE
DISCON(N+1,JB)=SPD(N+1)+DISCON(N,JB)
DIS(JB)=DIS(JB)+SPD(N+1)
CDMTRX(N+1,JB)=1.0-DIS(JB)

C
QMN(JB)=QMIN
SCAL(JB)=SCALE
QMX(JB) =QMAX

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450 CONTINUE
490 CONTINUE
WRITE(NOUT,701) (P1(J),J=1,8)
WRITE(NOUT,810)
WRITE(NOUT,601) (QMN(J),J=1,8)
WRITE(NOUT,602) (SCAL(J),J=1,8)
WRITE(NOUT,603) (QMX(J),J=1,8)
WRITE(NOUT,604) (IFLG(J),J=1,8)
480 WRITE(NOUT,810)
DCUM=0.0
DO 315 I=C,N+1
DCUM=DCUM+SPD(I)
WRITE(NOUT,900) I,(CDMTRX(I,J),J=1,8)
315 CONTINUE
WRITE(NOUT,810)
550 CONTINUE
2000 CONTINUE
C
C ##### F O R M A T S #####
C
9 FORMAT(4X,"RAMP"case, Smoothed-out version of dist. [Disc.contrb.
* removed] . Use is made of the Algorithm using DP(0:201) "!!"/)
401 FORMAT(20X," AMU=",F6.4," ,i.e., PO=",F10.8)
411 FORMAT(2X," That is for all B =",F6.4," ('',F4.2,')',F6.4)
701 FORMAT(2X,"P1(AMU,B)",8F14.8)
601 FORMAT(2X,"QMINs:",8F16.5)
602 FORMAT(2X,"SCALES",8F16.5)
603 FORMAT(2X,"QMAXs:",8F16.5)
604 FORMAT(2X,"FLAGS:",8(I10,6X))
800 FORMAT(14X," KOUNT=",I3)
812 FORMAT(10X," EXECTN. TIME CUMULATIVE=",I6,6X,F5.2)
815 FORMAT(12X," * IWRITEing Time=",I6," *")
810 FORMAT(" *****
*****')
900 FORMAT(2X,"('',I3,')',8(F14.8,X))
910 FORMAT(" DISCR",8('',F12.8,''))
END
C
C -----

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APPENDIX (B.3.)

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C
C
C      Program Name :      " TESTC.FOR "
C      -----
C      Purpose :
C      -----
C      To find and properly tabulate the percentage points of the tabulated
C      distributions of the Ramp r.v. ( average quality function ) , under the
C      assumption of a Normally distributed process with variance 1 and a mean
C      such that the proportion below 0 is fixed at p0 . It uses the tabulated
C      results of the convolved Distribution and so a file containing such
C      data is OPENned as an INPUT media . Extensive use of interpolation methods,
C      especially cubic splines from FORTRAN NAG Routine Library ,is made to
C      facilitate the purpose of this Program .
C      Results and output :
C      -----
C      Results are given in the tables of the Test Criteria
C      displayed in appendix (C.2.) .
C
C      Subroutines CALled and used :
C      -----
C      ( a ) Numerical Analysis Group ( NAG ) routines are :
C      E01BAF  determines a cubic-spline interpolant to a set of data
C      E02BBF  evalutes cubic-spline from its B-spline (see FORTRAN NAG Library Manual Mark 10 Vol 2 )
C      ( b ) Other specially-designed routines are :
C      BINOM  evaluates the standard Cumulative Binomial Probability
C             for given p , n and r .....
C      FLOG  finds the natural logarithm of the factorial of an
C            integer ( useful in evaluating BINOMial Coefficients)
C      FUN   evaluates a Zero of a numerical function within a level
C            of accuracy of the parameter ETA1 . Used to locate the
C            position of the "jump" for interpolation purposes .
C
REAL Q(102),G(102),PX(0:2)
REAL XG(102),YQ(102),KK(106),C(106),WRK(628)
REAL QKINK(0:256),TRJMP(0:256),BOTOM(0:256)
REAL CP(0:101,8),P1(8),PROB(27),AVQ(27,8)
REAL QMN(8),SCAL(8),QMX(8)
COMMON/FU/TOT(0:256)
INTEGER IFLG(8)
N=100
DATA IPAGE,IADD/1,0/
DATA JEND,IMUN/8,32/
DATA NUMBK,TOL,TOLCP/15,0.00001,1.0E-6/
DATA( PROB( IK ),IK=1,15)/0.01,0.02,0.03,0.04,0.05,0.06,0.49,
*0.50,0.51,0.89,0.90,0.91,0.94,0.95,0.96/
DATA IN,NOUT/1,20/,NOUT2/0/
WRITE(5,985)
985  FORMAT(6X,' Which ALL*.DAT ??? , Type value of KN , ""RETURN""')
ACCEPT *, KNT
NSIZ = 2 ** KNT
NSIZ1=NSIZ + 1
ENTRV = FLOAT( N )/NSIZ
QKNK1 = - ENTRV

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DO 100 I= 0,NSIZ
QKNK1 = QKNK1 + ENTRV
QKINK( I ) = QKNK1
100 CONTINUE
OPEN(UNIT=NOUT,DEVICE='DSK',FILE='AL.DAT',ACCESS='SEQIN')
READ(NOUT,9)
IMU = 0
WRITE(IN,996)
WRITE(IN,997) IPAGE
11 IMU = IMU + 1
IF( IMU .EQ. IMUN) GO TO 550
READ(NOUT,800) KN
READ(NOUT,401) AMUU,P0
READ(NOUT,411) B1,SB,BN
READ(NOUT,701) (P1(J),J=1,8)
READ(NOUT,810)
READ(NOUT,601) (QMN(J1),J1=1,8)
READ(NOUT,602) (SCAL(J1),J1=1,8)
READ(NOUT,603) (QMX(J1),J1=1,8)
READ(NOUT,604) (IFLG(J1),J1=1,8)
READ(NOUT,810)
DO 305 II=0,N+1
I=II
305 READ(NOUT,909) I,(CP(I,J1),J1=1,8)
CONTINUE
READ(NOUT,810)
NSIZ=2**KN
P0MU=P0
NSIZE = 2 * * KN
J = 0
B=0.3
2 J = J + 1
IF(J .EQ. JEND+1) GO TO 1230
P1MUB=P1(J)
P2MUB=1.0-(P0MU+P1MUB)
B=B+0.2
SCALE=SCAL(J)
TRUNC = 0.00063
IF(SCALE.EQ.TRUNC) SCALE=0.000625
CUMHR=0.0
QMIN=QMN(J)
QMAX=QMX(J)
I=-1
KIN=0
11 KIN=KIN+1
IF(KIN.GT.NSIZ1) GO TO 61
C
C The BINOM parameters n,p,ir {(nsiz , p0/(p0+p2) , max defs)}
C " Note that originally the problem TRINOMIAL but conditioned."
C
DENOM=(P0MU+P2MUB)
SCLING=DENOM**NSIZ
SINGP=P2MUB/(P0MU+P2MUB)
MAXEFF=KIN-1
IF(KIN.EQ.1) PREV=0.0
CALL BINOM ( NSIZ , SINGP , MAXEFF , TRIJMP )
TRJ=SCLING * TRIJMP
CURR=TRJ
TRJMP(KIN-1)=CURR
PREV=CURR

```

GO TO TU

```

C
C Cubic Spline fit for G(Q) (( i.e. Contin. Prob as Functn of Q ))
C
DO 63 IP1=1,N+1
Q(IP1)=QMIN+SCALE*(IP1-1)
G(IP1)=CP(IP1-1,J)
63 CONTINUE
M=101
LCK=M+4
LWRK=6*M + 16
IFAIL=0
CALL E01BAF(M,Q,G,KK,C,LCK,WRK,LWRK,IFAIL)
BOTOM(0)=G(1)
TOT(0) =BOTOM(0)+TRJMP(0)
DO 64 JMP=1,NSIZ-1
QKNK=QKINK(JMP)
QJUMP=QMIN + QKNK * SCALE
IFAIL=0
CALL E02BBF(M+7,KK,C,QJUMP,SVALUE,IFAIL)
TOT(JMP)=SVALUE + TRJMP(JMP)
IF(JMP .NE. 0 ) BOTOM(JMP)=SVALUE + TRJMP(JMP-1)
64 CONTINUE
TOT(NSIZ)=1.0
botom(NSIZ)=1.0-trjmp(NSIZ)+trjmp(NSIZ-1)
C
C The Spline-fitting of the inverse (( i.e. Q as functn of Cont Pr))
C
DO 65 I=0,N
IPLUS1=I+1
XG(IPLUS1)= CP(I,J) + (I-50)*0.000001
YQ(IPLUS1)= QMIN+(I)*SCALE
665 format(2x,8f14.8)
65 CONTINUE
M=101
LCK=M+4
LWRK=6*M+16
IFAI=0
CALL E01BAF(M,XG,YQ,KK,C,LCK,WRK,LWRK,IFAI)
C
C Trying to Locate the Inter-jump open interval Containing PROBK :
C
BOUND1=0.0
BOUND2=1.0
EPS1 = 1.0/NSIZ
ETA1 = 0.0001
DO 900 K=1,NUMBK
PROBK=PROBK(K)
PX(0)=BOUND1
PX(2)=BOUND2
CALL FUN(NSIZ,PROBK,PX,EPS1,ETA1,X,IFAU)
IF(IFAU.GT.C) WRITE(NOUT,99998) IFAU,AMUU,B,PROBK
99998 FORMAT(' IFAU=',I3,'; meaning that LOC is .GT. NSIZ in "FUN",
* For case of AMU=',F8.2,' B=',F7.2,' & PROBK=',F12.4)
INTXN=INT(X*NSIZ + 0.00001)
TOT1 = TOT(INTXN)
TOT2 = TOT(INTXN + 1)
BOTTOM= BOTOM(INTXN + 1)
QSOLN=QMIN + QKINK(INTXN + 1)*SCALE
IF( IFAU.EQ.0) GO TO 160
IF( BOTTOM .GT. PROBK ) GO TO 180

```

```

AVERG= - C.1
GO TO 200
16C AVERG=QSOLN
99991 FORMAT(2X,' Percent point is EXACTLY at the Jump, in the case of
* AMUU=',F5.2,' ; B =',F4.2,' For PROBK=',F12.5,'**',/)
go to 200
12C XVAL=PROBK - TRJMP(INTXN)
trjmp1=TRJMP(INTxn)
IFAL=0
CALL EQ2BBF(M+7, KK, C, XVAL, SVAL, IFAI)
AVERG=SVAL
200 AVQ(K, J)=AVERG
9CC CONTINUE
SCAL(J)=100*SCAL(J)
QMN(J)=100*QMN(J)
P1(J)=100*P1(J)
GOTO 2
1230 CONTINUE
990 NSIZE= 2 ** KN
WRITE(IN, 1890) NSIZE, AMUU, PO
WRITE(IN, 810)
WRITE(IN, 1601) (QMN(J), J=1, JEND)
WRITE(IN, 1602) (SCAL(J), J=1, JEND)
WRITE(IN, 1701) (P1(J), J=1, JEND)
WRITE(IN, 810)
WRITE(IN, 1589)
1589 FORMAT(9X,'P[Q < T] .....TEST CRITERION ,T .....',/)
DO 500 K=1, NUMBK
500 WRITE(IN, 1599) PROBK(K), (AVQ(K, J), J=1, JEND)
WRITE(IN, 995)
IF(IADD .EQ. 0) GO TO 501
WRITE(IN, 996)
IPAGE=IPAGE+1
WRITE(IN, 997) IPAGE
IADD=0
GO TO 1
501 CONTINUE
IADD=1
GO TO 1
2000 write(5, 2001)
2001 format(2x,' It is impermissible !! QKINK(i) not be exceeded')
550 CONTINUE
CLOSE(UNIT=NOUT, DEVICE='DSK')
9 FORMAT(4X,' "RAMP" case, Smoothed-out version of dist. [Disc. contrb.
* removed] . Use is made of the Algorithm using DP(0:201) "!!", /)
401 FORMAT(20X,' AMU=',F6.4,' , i.e., PO=',F10.8)
411 FORMAT(2X,' That is for all B =',F6.4,' (' ,F4.2, ')', F6.4)
701 FORMAT(2X,' P1(AMU, B)', 8F14.8)
601 FORMAT(2X,' QMINS:', 8F16.5)
602 FORMAT(2X,' SCALES:', 8F16.5)
603 FORMAT(2X,' QMAXS:', 8F16.5)
604 FORMAT(2X,' FLAGS:', 8(I10, 6X))
800 FORMAT(14X,' KOUNT=', I3, ' ')
810 FORMAT(9X,' *****')
1*****
811 format(2x,' For PROBK =', f5.2, ' :', /, 2x, '=====')
909 FORMAT(2X,' (' , I3, ')', 8(F14.8, X))
920 FORMAT(' DISCR', 8(' ', F12.8, ' '))
995 FORMAT(' -----', /)
* -----', /)

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997 FORMAT(7X,' .....')
1599 FORMAT(11X, F5.2, 5X, 8F7.4)
16C1 FORMAT(9X,' * QMIN x100:', 8F7.4, ' *')
16C2 FORMAT(9X,' * SCALEx100:', 8F7.4, ' *')
17C1 FORMAT(9X,' * P1 x 100:', 8F7.2, ' *')
1890 FORMAT(/, 9X, ' * S.SIZE=', I3, 6X, ' " Ramp case"', 10X, 'AMU=', F4.2
* , '(i.e. PO=', F8.5, ') *')
END
-----
SUBROUTINE FUN(NSIZE, PROB, PX, EPS1, ETA1, SOLUTN, IFAULT)
REAL F(0:2), PX(0:2)
COMMON/FU/TOT(0:8), QMIN
DATA ZERO/D.0/, TOLER/1.0E-4/
IF(PROB .GT. TOT(0)) GO TO 1
IFAULT=0
SOLUTN=QMIN
RETURN
10 PX(1)=(PX(0) + PX(2)) / 2
DO 100 I=0, 2
LOC=INT(NSIZE*PX(I) + TOLER)
10C F(I) = TOT(LOC) - PROB
ABSF1 = ABS(F(1))
IF(ABSF1 .LE. ETA1) GO TO 110
IF((F(1)*F(2)) .LT. ZERO) PX(0)=PX(1)
IF((F(1)*F(0)) .LT. ZERO) PX(2)=PX(1)
DELTA = PX(2) - PX(0)
IF(DELTA .LE. EPS1) GO TO 120
GO TO 1
11C IFAULT=0
SOLUTN=PX(1)
RETURN
12C IFAULT=-1
PX(1)=(PX(0) + PX(2)) / 2
SOLUTN=PX(1)
RETURN
END
-----

```



```

DATA IN,NOUT/1,20/,NOUT2/0/
OPEN(UNIT=NOUT,DEVICE='DSK',FILE='SUMKN.DAT',ACCESS='SEQIN')
READ(NOUT,1890) NSIZ,AMUU,PO
CLOSE(UNIT=NOUT,DEVICE='DSK',FILE='SUMKN.DAT')
write(1,91)
91 format(2X,'The Key to this output of "EQUIVALENCE" is :',/,
1' "Ours": EXST,NSIZ,B,T,P50 **',/,
1' "Attr": NSO,N95,C **',/,
1' "S": NSPLAN,QSPLAN **',/,
1' "SigM": NSIGMA,KSIGMA **',/)

AM95=2.4
DO 660 L=1,12
AM95=AM95-0.1
write(5,*) am95
===== R A M P =====
===== Fixing the 95% AQL Point =====
OPEN(UNIT=NOUT,DEVICE='DSK',FILE='SUMKN.DAT',ACCESS='SEQIN')
IMU=0
IMU=IMU+1

READ(NOUT,1890) NSIZE,AMUU,PO
READ(NOUT,810)
READ(NOUT,1601) (QMN(J),J=1,8)
READ(NOUT,1602) (SCAL(J),J=1,8)
READ(NOUT,1701) (P1(J),J=1,8)
READ(NOUT,810)
READ(NOUT,1589)
DO 15 K=1,NUMBK
15 READ(NOUT,1599) PROB(K),(AVQ(K,J),J=1,8)
READ(NOUT,810)

DO 16 J=1,8
16 AVQ14(IMU,J)=AVQ(14,J)
CONTINUE
IF(AMUU.LT.AM95-0.00001) GO TO 1
DO 25 J=1,8
25 IF(AVQ(5,J).LT.0.0) JFO(J)=-90
Q95(J)=AVQ(5,J)
CLOSE(UNIT=NOUT,DEVICE='DSK',FILE='SUMKN.DAT')
AQL=ALNORM(-AM95,.FALSE.)
IM95=INT((AM95-0.3)*10+0.001)
DO 5 J=1,8
5 JFOUND(J)=1
IF(JFO(J).EQ.-90) JFOUND(J)=-90
===== R a m p =====
===== SEARCH for the 50% Point MATCH =====
OPEN(UNIT=NOUT,DEVICE='DSK',FILE='SUMKN.DAT',ACCESS='SEQIN')
AMUU=0.3
IM=0
17 IM=IM+1
AMUU=AMUU+0.1
IF(IM.EQ.IM95+1) GO TO 550
1589 FORMAT(1X,'PR [Q < T] .....TEST CRITERION ,T ',/)
DO 11 J=1,8
11 AVE50=AVQ14(IM,J)
-----
IF(JFOUND(J).EQ.-1 OR JFOUND(J).EQ.0) GO TO 11
IF(AVE50.LT.0.0) GO TO 8
IF(Q95(J).GT.AVE50+0.0005) GO TO 11
Q50(J)=AVE50
AMU50(J)=AMUU
IF(Q95(J).LT.AVE50-0.0005) JFOUND(J)=-1
IF(Q95(J).LT.AVE50-0.0005) GO TO 11
Q50(J)=AVE50
AMU50(J)=AMUU
JFOUND(J)=0
IF(AVE50.LT.0.0) JFOUND(J)=-90
Q50(J)=AVE50
AMU50(J)=AMUU
11 CONTINUE
J=0
20 J=J+1
IF(JFOUND(J).GT.0) GO TO 7
IF(J.LT.8) GO TO 20
550 CONTINUE
DO 30 J=1,8
IEXIST=C
IF AULT=4
IF(JFO(J).EQ.-90) GO TO 29
MU50=(AMU50(J))*10-3
mu50=mu50+1
AVER50=AVQ14(MU50-1,J)
IF AULT=C
IF(JFOUND(J).EQ.0) GO TO 19
IF AULT=2
Some Interpolation data:
XABOVE(C)=AVQ14(MU50-1,J)
XABOVE(1)=AVQ14(MU50,J)

IF(JFOUND(J).EQ.-90 OR AVQ14(MU50-1,J).LT.0.0) GO TO 17
Hereafter ,JFOUND=-1 meaning it is likely to have a plan by
linear interpolation ,possibly
IF AULT=1
TDIFF = AVER50 - AVQ14(MU50,J)
AMFTY=AMU50(J) + 0.1*((AVQ14(MU50,J)-Q95(J))/TDIFF)
AMU50(J)=AMFTY
IEXIST=1
GO TO 29
17 CONTINUE

Hereafter; JFOUND=-90 or AVQ14(MU50-1,J) < 0.0 and so,we have
to extrap frm below and above using AVQ14(MU50-1) if JOUNDF=-90
and from above only if AVQ14(MU50-1)<0.0 and JFOUND=-90

IF AULT=-3
IF(JFOUND(J).EQ.-1) GO TO 18
IF AULT=-5
IEXIST=C
IF(AVQ14(MU50-1,J).LT.0.0) GO TO 29
JFOUND=-90 and AVQ14(MU50-1) > 0.0 and so we use AVQ14(L) for
L=MU50-2,-1 unless one of these is < 0.0 ((WHICH IS TO REPORT))

Firstly, Extrapolate from below :
EMU0=AMU50(J)-0.2
EMU1=EMU0+0.1

```

```

TBEL0=AVQ14(MU50-2,J)
IF(TBELC .LT. 0.0) GO TO 29
IEXIST=1
TBEL1=AVQ14(MU50-1,J)
DT= TBEL1 - TBEL0
AM = AMU50(J)+0.1*(Q95(J)-TBEL1)/DT
AMU50(J)=AM
GO TO 29
18 CONTINUE
C 2ndly, from Above ;
IEXIST=0
IF(XABOVE(0) .LT. 0.0) GO TO 29
IEXIST=1
TD= XABOVE(0)-XABOVE(1)
FTYMU=AMU50(J)+0.1*(Q95(J)-XABOVE(1))/TD
AMU50(J)=FTYMU
GO TO 29
19 ACURCY=Q95(J)-Q50(J)
IEXIST=1
29 CONTINUE
EXISTS(J)=IEXIST
30 CONTINUE
C-----
C ----- Print out of the 2 matching points of the 0.C curve -----
C-----
81C FORMAT(' *****
*****')
1595 FORMAT(4X,F5.2,8(F8.4,2X,X))
1601 FORMAT(2X,' QMIN ',8(F7.5,3X,X))
1602 FORMAT(2X,'SCALE ',8(F8.6,2X,X))
1701 FORMAT(1X,'* P1 ',8(F10.8,X))
189C FORMAT(/,14X,'* S.SIZE=',I3,' AMU=',F4.2,' (i.e. P0=',f10.8,') *')
C-----
C ***** The "EQUIVALENT" 2-Class Attribute Evaluations *****
C-----
DATA PAP5C,PAQL/0.50,0.95/
WRITE(0,95) AQL,AM95
95 FORMAT(2X,' For AQL =',F7.4,' (AMU95=',F5.2,' the following
+shows EQUIVALENTS :',/)
WRITE(0,99) NSIZ,PAQL,PAP50
99 format(2x,' For "our" plan of n=',I3,';Pa(AQL)=',f6.3,' Pa(p50)
+=',f7.3,' for the given " B " ',/ ,4X,'*** B ***** T *** Att
+ (n50 to n95,C) *** p50 *** SGMPlan(Nsgma,Ksgma)',/)
C
C
C WRITE(1,9988) AQL
9988 FORMAT(/,2X,'For AQL=',F10.5,' (at 95%) :',/)
B=0.3
DO 200 I=1,8
B=B+0.2
IF(JFO(I).EQ.-90 ) GO TO 190
IF(EXISTS(I).EQ.C) GO TO 197
AMU2=AMU50(I)
C
C ----- Next few lines establish the SIGMA-plan EQUIVALENT -----
C-----
C N.B. : Following the analytical relations of the Normal Distribution
C corresponding to the 95% and 50% risk points , viz. :
C Sqrt(Nsgma)*(Ksgma - Amu95 )/Sigma = -1.6449
C
C if can compute Ksgma and Nsgma , as follows :
C
105 CONTINUE
DELMU =AM95 - AMU50(I)
ROOTN =1.6449 * SIGMA / DELMU
NSIGMA = ROOTN * ROOTN
KSIGMA = AMU50(I)
C
C ===== The S-plan parameters deduced iteratively from the SGMA-plan=====
C ===== parameters as initial approximates ...Due to Hamaker(1976) =====
C == ( The reasoning & method of approx. is in Bravo & Wetherill( ) ) ==
C =====
QSO = KSIGMA
QS = QSC
ANO = FLOAT(NSIGMA)
ITERAT=C
110 ITERAT=ITERAT+1
AN2=AN1
AN1=ANO*(1. + QS*QS/2)
QS = QSC * ( 4. * AN1 - 4.)/( 4. * AN1 - 5.)
IF(AN1-AN2.LT. 1.0) GO TO 220
IF(ITERAT .GT. 10 ) GO TO 220
GO TO 110
220 NSPLAN = AN1
QS = QSC * (4*NSPLAN-4)/(4*NSPLAN-5)
QSPLAN = QS
WRITE(5,*) ITERAT
C-----
P50=ALNORM(-AMU2,.FALSE.)
CALL MATCH(AQL,PAQL,P50,PAP50,N95,N50,IDF,IFAUULT)
IF(IFAUULT .NE. 6) GO TO 180
WRITE(0,9991) I,EXISTS(I)
9991 FORMAT(/,2X,'EXISTS(',I1,')=',I4,':')
WRITE(0,179) B,IFAUULT,NSIGMA,KSIGMA
175 FORMAT(/,23X,'***** Warning *****',/ ,2X,F7.1,' :',13X,'
+*No Convergence in* <IFAUULT=',I2, '>',7X,I4,2X,F7.3, /
+ ,23X,'* "MATCH" (C1>n1) *',/ ,23X,'*****',/)
C
WRITE(1,9992) EXISTS(I),NSIZ,BZERO,QZERO,P50
WRITE(1,9909)
9909 FORMAT(////)
C
GO TO 200
180 CONTINUE
WRITE(0,9991) I,EXISTS(I)
WRITE(0,189) B,Q95(I),N50,N95,IDF,P50,NSIGMA,KSIGMA
189 FORMAT(2x,F7.1,' :',4X,F7.4,4X,i4,' ',i4,2x,i3,5X,
+'(',F7.4,')',9X,I4,2X,F7.3,/)
C
WRITE(1,9992) EXISTS(I),NSIZ,B,Q95(I),P50
WRITE(1,9993) N50,N95,IDF
WRITE(1,9994) NSPLAN,QSPLAN
WRITE(1,9995) NSIGMA,KSIGMA
WRITE(1,9997)
9992 FORMAT(2X,' "Ours"=',I5,I5,F10.5,F10.5,' For P50=',F10.5)
9993 FORMAT(2X,' "Attr"=',5X,I5,I5,I5)
9994 FORMAT(2X,' " S " ',5X,I5,F10.5)

```

```
9995 FORMAT(2X,"SGMA":,5X,I5,F10.5)
9997 FORMAT()
C
GO TO 200
190 CONTINUE
WRITE(0,9991) I,EXISTS(I)
WRITE(0,195) B,AM95
195 FORMAT(2X,F7.1,": * Problem of"non-existence" of plan
+ for "AMU95"=",F6.3,"*",/,16X,"* Since PA=0.95 lies in the JUMP
+ , T is undetermined*",/,21X,"*(Try Plan matched at 96% or
+ 94% in stead)*",/)
C
WRITE(1,9992) EXISTS(I),NSIZ,BZERO,QZERO,P50
WRITE(1,9909)
C
GO TO 200
197 CONTINUE
WRITE(0,9991) I,EXISTS(I)
WRITE(0,199) B,AM95
199 FORMAT(2X,F7.1,": ** Another "Non-existing" plan for
+"AMU95"=",F6.3,"*",/,16X,"**[ Interpolation hindered by
+ Unsuitable T-values ]**",/)
C
WRITE(1,9992) EXISTS(I),NSIZ,BZERO,QZERO,P50
WRITE(1,9909)
C
200 CONTINUE
WRITE(0,805)
805 FORMAT(/,' =====
+=====')
660 CONTINUE
END
```

```
+++++
+ + + + + S U B R O U T I N E S + + + + +
+++++
```

```
FUNCTION CHISQD( PP, N )
DIMENSION C(21), A(19)
DATA ( C(I),I=1,21)/
* 1.565326E-3, 1.060438E-3,
* -6.950356E-3, -1.323293E-2,
* 2.277679E-2, -8.986007E-3,
* -1.513904E-2, 2.530010E-3,
* -1.450117E-3, 5.169654E-3,
* -1.153761E-2, 1.128186E-2,
* 2.607083E-2, -2.237368E-1,
* 9.780499E-5, -8.426812E-4,
* 3.125580E-3, -8.553069E-3,
* 1.348028E-4, 4.713941E-1, 10.000886E-1 /
DATA ( A(I),I=1,19)/1.264616E-2, -1.425296E-2,
* 1.400483E-2, -5.836090E-3,
* -1.091214E-2, -2.304527E-2,
* 3.135411E-3, -2.728484E-4,
* -9.699681E-3, 1.316872E-2,
* 2.618914E-2, -2.222222E-1,
* 5.406674E-5, 3.483789E-5,
* -7.274761E-4, 3.292181E-3,
* -8.729713E-3, 4.714045E-1, 10.0E-1 /
```

```
IF ( N.E. 2) TO, 20, 50
CALL INVPHI ( P50, XINV )
CHISQD = XINV * XINV
RETURN
20 CHISQD = -2. * ALOG ( P )
RETURN
30 F = N
F1 = 1. / F
Q = 1.-P
CALL INVPHI ( Q, T )
F2 = SQRT( F1) * T
IF ( N.GE.(2*INT(4.*ABS(T) ))) GO TO 40
CHISQD = (((((( C(1)*F2+C(2))*F2+C(3))*F2+C(4))*F2
* +C(5))*F2+C(6))*F2+C(7))*F1 + (((((( C(8)+C(9))*F2)*F2
* +C(10))*F2+C(11))*F2+C(12))*F2+C(13))*F2+C(14))*F1 +
* ((((( C(15)*F2+C(16))*F2 + C(17))*F2+C(18))*F2
* +C(19))*F2+C(20))*F2 + C(21)
GO TO 50
40 CHISQD = ((( A(1)+ A(2)*F2)*F1+((( A(3)+ A(4)*F2)*F2
* + A(5))*F2+ A(6))*F1+(((( A(7)+ A(8)*F2 )*F2+ A(9))*F2
* + A(10))*F2+ A(11))*F2+ A(12))*F1 + ((((( A(13)*F2
* + A(14))*F2+ A(15))*F2+ A(16))*F2+ A(17))*F2*F2
* + A(18))*F2 + A(19)
50 CHISQD = CHISQD * CHISQD * CHISQD * F
RETURN
END
```

```
-----
INVPHI INVERTS ANY VALUE "P" OF CUM. NORMAL PROBABILITY
INTO ITS CORRESPONDING PERCENTAGE POINT.....
CAUTION:- HOWEVER, THERE WILL BE A TRUNCATION AT THE
"*****" TAILS AS, FOR EXAMPLE :
```

```
IF(PROB .LE. 0.00001) XINV= -5.0
SUBROUTINE INVPHI(PROB,XINV)
LOGICAL PR50
DATA TOL50,TOL01/0.1E-5,0.1E-9/
DATA CC,C1,C2,D1,D2,D3/2.515517,0.802853,0.010328,1.432788,
* 0.189269,C.001308/
PR50 = PROB.LE.0.5+TOL50 .AND. PROB.GE.0.5-TOL50
QXP=1.0 - PROB
XINV= -5.0
IF(QXP .GE. 0.99999) RETURN
XINV= 5.0
IF(PROB .GE. 0.99999) RETURN
IF(QXP .GT. 0.5) GO TO 50
SIGNX= 1.0
40 T = SQRT(ALOG(1.0/(QXP*QXP)))
TT = T*T
TTT = T*TT
POLY2= CC + C1*T + C2*TT
POLY3= 1.0 + D1*T + D2*TT + D3*TTT
XINV = T - POLY2/POLY3
XINV = SIGNX* XINV
RETURN
C
C The Inverse is Negative < 0.0
C
50 QXP = PROB
SIGNX= -1.0
```

```

GO TO 40
RETURN
60 XINV = CO
RETURN
70 XINV = CO
RETURN
END
-----
SUBROUTINE MATCH(AQL,PAQL,P50,PAP50,N95,N50,C,IFault)
C Gives the parameters ( n , c ) of a matching OC of "By-attributes"
C Actually ,sometimes ,it assigns two values for N ,called N50 & N95
C To decide which one to use depends on whether one needs to be closer
C to either of the points (AQL,PA1) & (p50,PA2) ,respectively..
LOGICAL COND
INTEGER C,CO,ifault
IFault = 6
P1 = AQL
P2 = P50
10 PRATIO = P50/AQL
CO = 0
20 C = CO
IC = 2*C
IC1= IC + 2
ALPHA=1.- PAQL
QAP50 =1. - PAP50
30 CHIP1 = CHISQD ( ALPHA ,IC)
CHI1P1 = CHISQD ( ALPHA ,IC1)
CHIP2 = CHISQD ( QAP50, IC )
CHI1P2 = CHISQD ( QAP50,IC1)
ROFC1 = CHI1P2 / CHI1P1
ROFC = CHIP2 / CHIP1
IF (ROFC1 .LT. PRATIO .AND. ROFC .GT. PRATIO) GO TO 35
CO = CO + 1
GO TO 20

35 AN1 = 0.5 * CHI1P2 / P2
AN2 = 0.5 * CHI1P1 / P1
N2 = AN2
N0 = AN1
ANG=FLOAT(N0)
N1 = AN1
IF ( ANG.EQ.AN1 ) GO TO 55
55 IFLAG = N2 - N1 + 1
IF (IFLAG) 65,85,85
65 C = C+1
ICC = 2*(C+1)
if(icC .gt. n1) go to 69
ifault=6
return
65 CHI1P1 = CHISQD( ALPHA,ICC)
CHI1P2 = CHISQD( QAP50,ICC)
GO TO 35
85 N95 = N2
N50 = N1
IFault = C
RETURN
END

```

```

-----
C THE NORMAL INTEGRAL.....DUE TO I.D.HILL...AS66-
C EVALUATES TAIL AREA OF STAND. NORML CURVE FROM MINUS INF.TO
C X IF UPPER IS FALSE.
REAL LTONE,UTZERO,HALF,ONE,CON,Z,Y,X
LOGICAL UPPER,UP
C LTONE,UTZERO SET TO SUIT PARTIC. COMPUTER (SEE INTROD. TEXT)
C
DATA LTONE,UTZERO/7.0,18.66/
DATA ZERO,HALF,ONE,CON/0.0,0.5,1.0,1.28/
UP=UPPER
Z=X
IF(Z.GE.ZERO) GO TO 10
UP=.NOT.UP
Z=-Z
10 IF(Z.LE.LTONE.OR.UP.AND.Z.LE.UTZERO) GO TO 20
ALNORM=ZERO
GO TO 40
20 Y=HALF*Z*Z
IF(Z.GT.CON) GO TO 30
C
ALNORM=HALF-Z*(0.398942280444-0.399903438504* Y/
1 (Y + 5.75885480458 - 29.8213557808 /
2 (Y + 2.62433121679 + 48.6959930692/
3 (Y + 5.92885724438 )))
GO TO 40
C
30 ALNORM = 0.398942280385 * EXP(-Y)/
1 (Z - 3.8052E-8 + 1.00000615302/
2 (Z + 3.98064794E-4 + 1.98615381364/
3 (Z - 0.151679116635 + 5.29330324926/
4 (Z + 4.8385912808 - 15.1508972451/
5 (Z + 0.742380924027 + 30.789933034/
6 (Z + 3.99019417011 )))
C
140 IF(.NOT.UP) ALNORM = ONE - ALNORM
RETURN
END

```

```

-----
SUBROUTINE NEVIL(XINT,X,FX,N,POLY,P,IFA)
REAL X(C:N),FX(O:N),POLY(N)
DO 10 I=0,N
10 X(I)=XINT - X(I)
NP=1
DO 20 I=NP,N
20 POLY(I)=(X(I-NP)*FX(I)-X(I)*FX(I-1))/(X(I)-X(I-NP))
25 NP=NP+1
IF(NP.GT.N) GO TO 60
DO 30 I=NP,N
POLYI=(X(I-NP)*POLY(I)-X(I)*POLY(I-1))/(X(I)-X(I-NP))
30 POLY(I)=POLYI
GO TO 25
60 P=POLY(N)
RETURN
END

```

APPENDIX (B.5.)

 program Name : ' UNIFRM.FOR '

Purpose :
 ----- To assess the performance of the different but "equivalent"
 plans when the process under inspection by such plans are Uniformly
 distributed (as one of Non-normal Distribution-effect robustness
 studies) .

Input Data :
 ----- The "equivalences" and their resultant decision rules
 imbedded in the plans parameters are fed to this program via the
 data file SAMYS.DAT . SAMYS.DAT contains all the information on the
 "equivalences" established earlier on .

Routines and Sub-programs used :

1. UNFRMF : Calculates the Uniform Cumulative Probability for
 any given sample size and mean .
 However , as is well known that the rate at which the
 convolved distribution is compressed rises with respect
 to n such that a point could be reached where this
 routine UNFRMF becomes numerically unstable . A normal
 approximation is then used the routines for such an
 approximation are APPROX and RMPAPP .
2. UNRAMP : To evaluate the performance of the Ramp plan
 given the values of its parameters . It CALLS ON
 UNFRMF (for uniform cumulative probability), SINGLE (a
 routine that gives the simple Trinomial weighting for
 conditional content of the 3 quality classes) and
 BINOM which gives two-class cases, i.e. when there
 are no marginals).
3. UNVAR : To evaluate the performance of the orthodox
 By-Variables "equivalent" plans under Uniformity
 assumption .

 DATA NOUT / 20 / ,PAAQL / 0.95 /
 OPEN (UNIT=NOUT,DEVICE='DSK',FILE='SAMYS.DAT',ACCESS='SEQINOUT')
 VARPA=PAAQL*(1.0-PAAQL)
 BERNOU=SQRT(VARPA)
 DO 1000 KNT=2,6
 NNN=2**KNT
 READ (NOUT,109)
 DO 200 IAQL=1,12
 WRITE (0,999)


```

READ(NOUT,209) AQL
PO=AQL
IF ( IAQL .GE. 12) GO TO 10
WRITE(0,209) AQL
WRITE(0,5)
5  FORMAT(2X,'=====','/,
+56X,'Uniform-Robustness',/,54X,' Pa   ROB',
+/,54X,' -----')
10  CONTINUE
DO 100 JB=1,8
READ(NOUT,309) IEXIST,NSIZ,B,T,P50
IF(IEXIST .EQ. 1) GO TO 20
READ(NOUT,409)
BB = 0.3 + 0.2 * JB
IF ( IAQL .LT. 12 ) WRITE(0,490) NSIZ,BB
GO TO 100
20  CONTINUE
READ(NOUT,509) NS0,N95,IC
READ(NOUT,609) NSPLAN,QSPLAN
READ(NOUT,609) NSIGMA,AKSGMA
IF ( IAQL .GE. 12 ) GO TO 30
SDPA = BERNOU / SQRT(FLOAT(N95))
CALL UNRAMP(PO,B,NSIZ,T,PARAMP)
ROB=(PAAQL-PARAMP)/SDPA
WRITE(0,99) NSIZ,B,T,PARAMP,ROB
WRITE(0,91) NS0,N95,IC,P50
CALL UNVAR(PO,NSPLAN,QSPLAN,CC1,CC2,PAS)
ROB=(PAAQL-PAS)/SDPA
WRITE(0,103) NSPLAN,QSPLAN,PAS,ROB
CALL UNVAR(PO,NSIGMA,AKSGMA,C1,C2,PASGMA)
ROB=(PAAQL-PASGMA)/SDPA
WRITE(0,101) NSIGMA,AKSGMA,PASGMA,ROB
20  FORMAT(2X,'"Attr":',5X,I5,I5,I5,3X,'(for p50=',F7.4,')')
101  FORMAT(2X,'"SGMA":',5X,I5,F10.5,25X,F10.4,' (',F6.3,')',/)
99   FORMAT(2X,'"Ramp":',5X,I5,' B=',F6.2,3X,' T=',F7.4,
+11X,F10.4,' (',F6.3,')')
103  FORMAT(2X,'" S  ":',5X,I5,F10.5,25X,F10.4,' (',F6.3,')')
30  CONTINUE
READ(NOUT,909)
100  CONTINUE
200  CONTINUE
490  FORMAT(2X,'"Ramp":',5X,I5,' B=',F6.2,3X,' T= *
+16X,' * * ',/,16X,' ( " Non-Existent " )',/)
1000 CONTINUE
CLOSE(UNIT=NOUT,DEVICE='DSK')
1005 format(2X,'The Key to this output of "EQUIVALENCE" is :',/,
1'  "Ours": EXST,NSIZ,B,T,P50  **',/,
1'  "Attr": NS0,N95,C  **',/,
1'  " S  ": NSPLAN,QSPLAN  **',/,
1'  "SigM": NSIGMA,KSIGMA  **',/)
209  FORMAT(/,2X,'For AQL=',F10.5,' (at 95%) :',10X,'Uniform Model',/)
309  FORMAT(2X,'"Ours":',I5,I5,I5,F10.5,F10.5,' For P50=',F10.5)
509  FORMAT(2X,'"Attr":',5X,I5,I5,I5)
609  FORMAT(2X,'" S  ":',5X,I5,F10.5)
809  FORMAT(2X,'"SGMA":',5X,I5,F10.5)
909  FORMAT()
409  FORMAT(////)
END

```

```

-----
c  Assumes given :p0,p1,B,nsiz,T ( &may be AMU95,AMU50 of B)
SUBROUTINE UNVAR(PO,NV,AK,C1,C2,PA)
DOUBLE PRECISION SUM1
DATA SQRT12/3.4641016/
C1= - SQRT12 * PO
C2=SQRT12+C1
AMSTD=(AK-C1)/(C2-C1)
SUM1 = AMSTD * NV
IF(NV .GT. 10) GO TO 30
10  CALL UNFRMF(SUM1,NV,F)
20  PA=1.0 - F
RETURN
30  CALL APPROX(AMSTD,NV,F)
PA=F
RETURN
END

```

```

=====
C  ----- INVERSE OF NORMAL FUNCTION -----
C  INVPHI INVERTS ANY QUALITY FUNCTION OF NORMALITY PLAN..
C  CAUTION:- HOWEVER, THERE WILL BE A TRUNCATION AT THE
C  "*****" TAILS AS ,FOR EXAMPLE :
C  IF(PROB .LE. 0.001) XINV= - 3.09
SUBROUTINE INVPHI(PROB,XINV)
LOGICAL PR50
DATA TOL50,TOL01/0.1E-5,0.1E-9/
DATA CC,C1,C2,D1,D2,D3/2.515517,0.802853,0.010328,1.432788,
* 0.189269,0.001308/
PR50 = PROB.LE.0.5+TOL50 .AND. PROB.GE.0.5-TOL50
QXP=1.0 - PROB
XINV= -3.09
IF(QXP .GE. 0.999) RETURN
XINV= 3.09
IF(PROB .GE. 0.999) RETURN
IF(QXP .GT. 0.5) GO TO 50
SIGNX= 1.0
40  T = SQRT(ALOG(1.0/(QXP*QXP)))
TT = T*T
TTT =T*TT
POLY2= CC + C1*T + C2*TT
POLY3= 1.0 + D1*T + D2*TT + D3*TTT
XINV = T - POLY2/POLY3
XINV = SIGNX* XINV
RETURN
C  THE INVERSE IS NEGATIVE < 0.0
50  QXP = PROB
SIGNX= -1.0
GO TO 40
RETURN
60  XINV= - C0
RETURN
70  XINV= C0
RETURN
END

```

```

C  ##### NORMAL INTEGRAL ( I.E. AREA UNDER CURVE) #####
C  THE NORMAL INTEGRAL.....DUE TO I.D.HILL...AS66.
C  FUNCTION ALNORM(X,UPPER)
C  EVALUATES TAIL AREA OF STAND. NORML CURVE FROM MINUS INF.TO

```

```

C      X IF UPPER IS .FALSE.
      REAL LTONE,UTZERO,HALF,ONE,CON,Z,Y,X
      LOGICAL UPPER,UP
      LTONE,UTZERO SET TO SUIT PARTIC. COMPUTER (SEE INTROD. TEXT)

      DATA LTONE,UTZERO/7.0,18.66/
      DATA ZERO,HALF,ONE,CON/0.0,0.5,1.0,1.28/
      UP=UPPER
      Z=X
      IF(Z.GE.ZERO) GO TO 10
      UP=.NOT.UP
      Z=-Z
10     IF(Z.LE.LTONE.OR.UP.AND.Z.LE.UTZERO) GO TO 20
      ALNORM=ZERO
      GO TO 40
20     Y=HALF*Z*Z
      IF(Z.GT.CON) GO TO 30

      ALNORM=HALF-Z*(0.398942280444-0.399903438504* Y/
1     (Y + 5.75885480458 - 29.8213557808 /
2     (Y + 2.62433121679 + 48.6959930692/
3     (Y + 5.92885724438 )))
      GO TO 40

30     ALNORM = 0.398942280385 * EXP(-Y)/
1     (Z - 3.8052E-8 + 1.00000615302/
2     (Z + 3.98064794E-4 + 1.98615381364/
3     (Z - 0.151679116635 + 5.29330324926/
4     (Z + 4.8385912808 - 15.1508972451/
5     (Z + 0.742380924027 + 30.789933034/
6     (Z + 3.99019417011 )))))

40     IF(.NOT.UP) ALNORM = ONE - ALNORM
      RETURN
      END

#####
DOUBLE PRECISION FUNCTION FLOG(IN)
      Intended to give ln(IN ! ) , i.e. "LOGe FACTORIAL" IN .
      Numerically recommendable for BI&TRINOMIALS.....

      DOUBLE PRECISION F(0:6),X,DLOG
      DATA F(1),F(2),F(3),F(4),F(5),F(6),F(0)/0.D0,0.D0,-.69314718D0,
1     1.7917595D0,3.1780538D0,4.7874917D0, 0.D0/
      IF (IN.GT.5) GO TO 10
      FLOG = F(IN+1)
      RETURN
10     X=IN
      FLOG = .91893854D0+(X+.5D0)*DLOG(X)-X+1.0D0/(12.0D0*X)
1     -1.0D0/(360*(X**3.0D0))+1.0D0/(1260*(X**5.0D0))
      RETURN
      END

.....
SUBROUTINE SINGLE(PO,P1,P2,NN,IO,I1,TRIN)
DOUBLE PRECISION COEFFT,PPPP,TERM,DPO,DP1,DP2
DOUBLE PRECISION FLOG
I2=NN-IO-I1
FN=FLOAT(NN)
FIO=FLOAT(IO)

F12=FLOAT(I2)
DP1=P1
DP2=P2
COEFFT=FLOG(NN)-FLOG(IO)-FLOG(I1)-FLOG(I2)
PPPP = FIO*ALOG(PO)+F11*ALOG(P1)+F12*ALOG(P2)
TERM=COEFFT+PPPP
TERM=EXP(TERM)
TRIN=TERM
RETURN
END

=====
SUBROUTINE UNRAMP(PO,B,NSIZ,T,PA)
      Assumes given :p0,B,nsiz,T ( &may be AMU95,AMU50 of B)
      DOUBLE PRECISION SUM2
      INTEGER RC,R1,R2
      DATA SQRT12/3.4641016/,A/0.0/
      ENSIZ = NSIZ
      NXT=NSIZ*T
      C1= - SQRT12 * PO
      C2=SQRT12+C1
      P1STAR=(B-A)/(C2-C1)
      UNSCAL=AMIN1(B,C2)
      SUM=0.0
      IF(UNSCAL .LT. B) GO TO 30
      P2STAR = 1. - PO - P1STAR
      P2SCAL=P2STAR/(PO+P2STAR)
      P0SCAL=1. - P2SCAL
      CALL BINOM(NSIZ,P0SCAL,NSIZ-NXT,BIN)
      SUM=( (PO+P2STAR)**ENSIZ ) * ( BIN )
      TN = NSIZ * T
      DO 10 RO=0,NSIZ-1
      LEFT=NSIZ-RO
      DO 10 R1=1,LEFT
      R2=LEFT-R1
      TEST= ( (TN - R2) ) / ( R1 ) * (B/UNSCAL)
      S=( R1 * TEST)
      SUM2=S
      IR0=RO
      IR1=R1
      IR2=R2
      CALL SINGLE(PO,P1STAR,P2STAR,NSIZ,IR0,IR1,TRINO)
      SNGTRI=TRINO
      UNFGT=1.0
      RR2 = R2
      IF ( RR2 .GE. TN) GO TO 7
      IF(IR1 .GT. 10) GO TO 8
      CALL UNFRMF(SUM2,IR1,UNF)
      UNFGT=1.0-UNF
17     SUM=SUM+UNFGT*SNGTRI
      GO TO 10
8     CALL RMPAPP(TEST,IR1,FNORM)
      UNFGT=1.0-FNORM
      GO TO 7
10     CONTINUE
30     PA=SUM
200    continue
      RETURN
      END

```

```

C =====
C SUBROUTINE UNFRMF( SN , NR1 , UNIFF )
C GIVEN 'NR1' , THE NUMBER OF UNIFORMS , 'UNFRMF' COMPUTES THE
C CUMULATIVE DISTN FOR THE SUM OF 'NR1' UNIFORMS IN ( 0 , 1 ) BEING
C .LE. 'SN'(GIVEN) . THE OUTPUT IS 'UNIFF'.....
C DOUBLE PRECISION SN,SUMK,TERM,FLOGD,CFNI,FINR1,AI, FN,FLOG,UN
C UNIFF=1.0
C FN = DFLOAT(NR1)
C IF( SN .GT. FN) RETURN
C UNIFF=0.0
C IF ( SN .LE. 0.000 ) RETURN
C K =INT(SN*0.500)
C SUMK = 0.000
C ISGN = -1
C UN=DEXP(-FLOG(NR1) + NR1 * DLOG(SN) )
C UNIFF = UN
C IF( K .EQ. 0) RETURN
C DO 100 I = 0,K
C II = I
C ISGN = - ISGN
C NR1II=NR1-II
C FLOGD= ( FLOG(NR1II)+FLOG(II) )
C CFNI = DEXP( FLOGD )
C TERM = 0.000
C FINR1=DFLOAT(II) / FN
C AI=DFLOAT(I) + 0.0500
C IF( AI .GT. SN) GO TO 100
C TERM = ISGN *CFNI *(SN - AI)**NR1
C SLMK = SUMK + TERM
100 CONTINUE
C UNIFF = SUMK
C IF(UNIFF .GT. 1.0) UNIFF=1.0
C IF (UNIFF .LT. 0.0) UNIFF=0.0
C RETURN
C
C 200 SN = SN/NR1
C XB = SN
C Z = (XB - 0.5 ) * SQRT(12.*NR1)
C APPRX = ALNORM( Z ,.FALSE. )
C UNIFF = APPRX
C RETURN
C
C END

```

```

C =====
C SUBROUTINE APPROX(TVALUE,IRR,UNFAPR)
C RT12R1=SQRT(IRR*12.0)
C XNORM=(TVALUE - 0.5) * RT12R1
C UNFAPR=ALNORM(XNORM,.TRUE.)
C RETURN
C END

```

```

C -----
C SUBROUTINE RMPAPP(TVAL,IR,UNFAPR)
C RT12R1 = SQRT(IR*12.0)
C Z = (TVAL - 0.5) * RT12R1
C UNFAPR = ALNORM(Z ,.FALSE.)
C RETURN
C END

```

```

C -----
C SUBROUTINE BINOM(NN,P,IX,BIN)

```

Definition: This Subroutine gives the Cumulative Binomial as:

BIN= "Sum over j=0 to IX" of $\frac{NN!}{(j! (NN-j)!)} P^j (1-P)^{NN-j}$
 So, the Subroutine should be used bearing this definition in mind !

```

C
C DOUBLE PRECISION PDB(0:1000),CDB(0:1000)
C DOUBLE PRECISION PDLOG, FNM , FM , Q ,PO,FLOG,BIND
C DATA IFL2/ 2 /
C PO = P
C Q=1.000 - PO
C M = IX
C N = NN
C M2=N-M-1
C IFLAG=0
C IF( Q .GT. 0.500 ) GO TO 200
200 CONTINUE
C FNM=DFLOAT(N-M)
C FM =DFLOAT(M)
C PDLOG=FLOG(N)-FLOG(M)-FLOG(N-M)+FM*DLOG(PO)+(FNM)*DLOG(Q)
C PDB(M)=DEXP( PDLOG )
C CDB(M)=PDB(M)
C IF ( M .EQ. 0 ) GO TO 100
C DO 100 J=M-1,0,-1
C JPLS1 = J + 1
C NMSJ = N - J
C PDB(J)=PDB(JPLS1)*( Q )/PO *DFLOAT(JPLS1)/DFLOAT(NMSJ)
C CDB(J) = CDB(JPLS1) + PDB(J)
100 CONTINUE
C BIN=CDB(0)
C IF ( IFLAG .EQ. IFL2 ) BIN=1. - BIN
C RETURN
200 IFLAG = 1
C PDLOG = Q ** N
C BIND = PDLOG
C IF ( M .GT. INT(N/2) ) GOTO 400
C DO 300 K=1,M
C PDLOG=PDLOG/Q *(N-K+1)/K *PO
C BIND=BIND + PDLOG
300 CONTINUE
C BIN = BIND
C RETURN
400 IFLAG=IFL2
C M = M2
C PO = Q
C Q = 1.000 -PO
C GO TO 200
C END

```

----- E n d -----

APPENDIX (B.6.)

```

C          ***** Simulation Program (1) *****
C          =====
C          Name of Program :      '  CONTAM.FOR  '
C          -----
C
C          Purpose :
C          ----- for study of robustness in "Contaminated" normal distribution
C          ( both the "Contaminant" and the "Contaminated" are Normals ).
C          Number of Simulations is NSIMUL=2000 so as to maintain a level of
C          precision at Alpha= 1% ; the Number of Normal r.v.'s
C          used in the simulation is about 800,000 r.v.'s . Details of the methods
C          implemented are imbedded as Comments inside the Program .
C
C          Input Data and Random Numbers Used :
C          -----
C          1.The Normal r.v.'s were prepared prior to the running of this program.
C          They were generated using Brent Algorithm and random uniform number
C          generator RAN together with other facilities of the University of Essex
C          Computer ( DEC-10 ) .These are then shuffled in blocks of 1000 at a time
C          and stored in a Data File named NORVS.DAT ( about 800000 r.v.'s in
C          about 6000 computer blocks ) .
C
C          2. The "equivalence" data are also used of course .
C
C          Routines and Sub-Programs CALLED :
C          -----
C          1. NEWRVS      :a routine to READ in the r.v.'s in blocks of a 1000 at
C                       a time once the 1000 in the buffer has been consumed .
C          2. GAMMA      : to READ in the required value of GAMMA , the fraction
C                       of "Contamination" . It is the proportion of the
C                       "contaminant" in the process .
C          3. STNORM     : Sub-program generator of Normal r.v.'s .
C
C          *****
C          -----
C
C          SUBROUTINE NEWRVS ( MORE , J )
C          COMMON / ANEW / XN(1000)
C          READ(21) XN
C          J = 1001
C          RETURN
C          END
C
C          DIMENSION NAT(4),ICA(4),NRA(4),TRA(4),NSG(4),AKG(4),NSP(4),QSP(4)
C          DIMENSION IEXIS(4)
C          DIMENSION X(450)
C          real xc(450),uu(450)
C          COMMON / ANEW / XN(1000)
C          DATA NSIMUL / 2000 /

```

```

DATA D / 2.0 /
      GAMMA is the contamination fraction
OPEN(UNIT=20,DEVICE='DSK',FILE='GAMMA.DAT',ACCESS='SEQINOUT')
READ(20,90) GAMMA
WRITE(5,90) GAMMA
90  FORMAT(2X,'Value of GAMMA as in OPENned GAMMA.DAT is =',F5.2)
CLOSE(UNIT=20,DEVICE='DSK')

DATA prop /0.0287 /
DATA (IEXIS(J),J=1,4) / 1,1,1,1 /
DATA (NAT(J),J=1,4) / 28,28,28,28 /
DATA (ICA(J),J=1,4) / 2,2,2,2 /
DATA (NRA(J),J=1,4) / 8,8,8,8 /
DATA (TRA(J),J=1,4) / .829,.7693,.7104,.6475 /
DATA (NSG(J),J=1,4) / 4,5,5,6 /
DATA (AKG(J),J=1,4) / 1.14248,1.18476,1.2229,1.26174 /
DATA (NSP(J),J=1,4) / 6,8,8,10 /
DATA (QSP(J),J=1,4) / 1.20261,1.22864,1.26756,1.29779 /

-----
PACCEP=C.95
WRITE(NOUT,99901) NSIMUL,PROP,D
99901  FORMAT(2X,'No. of Simulations=',I7,/,
*2X,' PD =',F7.4,' ( D =',F5.2,' where SIGC= D * SIGO )'
*,' For the Plans :',/,2X
*,' B Natt c Nramp Tramp Nsplan QS Nsigma Ksig'
*)
991  FORMAT(2X,'(',F4.1,')',I4,I4,I5,F7.4,I5,F7.4,I6,F7.4)
      B=0.1
      DO 25 J=1,4
      B=B + 0.4
      WRITE(NOUT,991) B,NAT(J),ICA(J),NRA(J),TRA(J),NSP(J),QSP(J)
* ,NSG(J),AKG(J)
85  CONTINUE
      WRITE(NOUT,99903)

Let EMUC and EMUO denote the means of the Contaminant dist. and
the Original dist. respectively. Let SIGC and SIGO be the respective
standard deviations for the component normals. Set EMUC = 0.0 and
solve for EMUO
and SIGC ( since SIGC = D * SIGO ) by using the facts that the overall
variance should equal 1, and that the overall proportion defective
is PROP ( given ). Hence,

( PROP :- GAMMA * PHI ( -O/SIGC ) ) / ( 1-GAMMA ) = PHI(-EMUO/SIGO)

EMUC = 0.0

The above discussion imply that

      EMUO = - SIGO * PHI-1 ( PROP - GAMMA/2 ) / ( 1-GAMMA )

which will only make sense if the argument is +ve and reasonably ( 0.001 )
away from 0. Strictly speaking if PROP < GAMMA/2 there is no solution.
So, we have 3 parameters and 2 equations which suggest we should
determine SIGO and EMUO in terms of GAMMA for agiven PROP

GAMMA = GAMMA * 0.9
10  WRITE(5,10) GAMMA
+  FORMAT(2X,' Negative probability argt , i.e., GAMMA
too large for PROP ,GAMMA is DESCALED into',F7.4,' *')
GO TO 5
20  ONEMG=1.0 - GAMMA
      GA=GAMMA
      PVALUE = ( PROP - GAMMA * 0.5 ) / ONEMG
      PHINVO = GAUINV ( PVALUE ,ifault)
      IF ( IFAULT .NE. 0 ) STOP ' PROP is not a Probability !!'
      RSIGMA = sqrt(GA*D*D + ONEMG + GA * ONEMG * ( PHINVO * PHINVO ) )
      SIG = 1.0 / RSIGMA
      EMUO = - PHINVO * SIG
      SIGO=SIG
      SIGC= D * SIGO

Now, having determined all the contamination and its components'
parameters ( i.e. EMUC, EMUO, SIGO, SIGC and GAMMA ), we use the
pseudo-random normal variates and do the contamination of the randomly
selected samples as in the following steps :

1.  READin the current set of parameters of the EQUIVALENT plans
to be compared (NATT,IC),(NRAMP,TRAMP,B,PD(2)),(NSIGMA,AKSGMA),
and (NSPLAN,QSPLAN) ,....,etc.

50  READ()

      B=0.1
      DO 9000 JB=1,4
      B = B + 0.4
      NATT = NAT(JB)
      IC = ICA(JB)
      NRAMP = NRA(JB)
      TRAMP = TRA(JB)
      NSIGMA = NSG(JB)
      AKSGMA = AKG(JB)
      NSPLAN = NSP(JB)
      QSPLAN = QSP(JB)

2.  Initialise the sums, sums of squares, the number of simulation
samplings, etc....

      SU1J=0.0
      SU1J2=0.0
      SD2J=0.0
      SD2J2=0.0
      SD4J=0.0
      SD4J2=0.0
      SD5J=0.0
      SD5J2=0.0
      IRAND=0
      ISIM = 0
      IF ( IEXIS(JB) .NE. 1 ) GO TO 8600

      J=1001
      OPEN(UNIT=21,DEVICE='DSK',FILE='NORVS.DAT',ACCESS='SEQINOUT',
1  MODE='BINARY')

```

```

C      Read-in the first block of a 1000 standard normal r.v.'s
C
C      READ(21) XN
C
C      Start of Simulation sampling
C      (( ISIM is the count of the Simulation samples made))
C
100  ISIM = ISIM + 1
      NMAX = NMAX
C
C      3. In the following we are assuming we have a block of 1000 r.v.'s
C      in the buffer array XN(1000) .Now, we select a sample for the
C      Attribute case sequentially relying on the randomization of the
C      shuffling done to the normal variates prior to storage on disc .
C      Note that if the supply of the
C      current 1000 r.v.s. is nearly exhausted MORE is supplied from storage
C      by a CALL NEWRVS( MORE , J) which reads more r.v.'s from the OPENED
C      disc file NORVS.DAT ...This happens whenever the remaining r.v.'s
C      are not exactly enough to make a new different sample . The Subroutine
C      NEWRVS provides MORE r.v.'s . That is , making a completely new different
C      set of 1000 uncycled r.v.'s from which further simulation samplings
C      are made ..
C
      DO 999 I = 1,NMAX
        J=J-1
        MORE=1000-J
        ITH = MORE
        X(I) = XN(ITH)
        IF ( J .LE. 1 ) CALL NEWRVS(MORE,J)
999  CONTINUE
C
C      Notice : A shuffling process is already done on the stored r.v.'s
C      prior to storing them . This is done by a randomisation procedure
C      and that is why we are reading and using the stored r.v.'s sequentially
C      Shuffling is meant to break down any pattern or sequence in the pseudo-
C      random variates used .
C
C      4. The random contamination procedure for the NMAX sample follows .
C      (NMAX is the sample size for the attribute case , the maximum n ).
C      NOTES on possible methods :
C      (a). The ALIAS METHOD is suggested here to speed up the operation
C      of random contamination .The Alias Table of Li and Fi is generated
C      by SUBROUTINE ALIAS .The Alias table is then used as follows:
C      - Generate ,independently, two r.v.'s U1 , U2 {~ Uniform(0,1) } .
C      - Select cell i=INT(nmax * U1) + 1 ; if U2 < Fi then IRC ,the
C      no. of contaminated r.v.'s in the sample , is IV(i) ; and otherwise
C      IRC=IV( L(i) ), where IV(i)=i-1 (for i=1,nmax+1 ) is the set of the
C      random number of contaminated r.v.'s .
C      (b). The DIRECT method is as follows :
C      -Generate NMAX uniform r.v.'s ,UU(),(independent of the shuffling
C      uniforms and of the normals creator ) .
C      -Compare each of the UU(j) uniforms with GAMMA and decide :
C      if UU(j) > GAMMA then XC(j)=X(j)*sigo + EMUO , otherwise
C      contamination takes place ,i.e., XC(j)=X(j)*sigc + EMUC
C      where XC and X are the contaminated and the pre-contamination
C      samples , respectively....
C
      UNIF = GOSCAF(UNIF)
      XI = X(I)
      XII= XI * SIGO + EMUO
      IF ( UNIF .LE. GAMMA ) XII = XI * SIGC + EMUC
      XC(I) = XII
1500 CONTINUE
C
C      This XC(I) sample is a GAMMA-contaminated normal sample from :
C      F = (1 - GAMMA) * PHI(EMUO ,SIG) + GAMMA * PHI(EMUC ,SIG)
C      which is a mixture of two normals
C      Generally , on simulating the robustness of the contaminated
C      normal we made use of the idea of 'CONTROL VARIATE ' by use of the
C      attribute plan whose variability is controlled and by re-use of the
C      same sample data to simulate the behaviour of each of the "Equivalent"
C      plans . Note also the economisation due to the intensive use and re-use
C      of r.v.'s of the attribute largest sample to create more than one smaller
C      samples of equivalent plans per each attribute sample.
C
C      5. Herebelow we evaluate the contamination effects on the attribute as
C      well as preparing for assessing the effects on other "equivalent"
C      plans :
C
      NO = 0
      U1J = 0.0
      A = 0.0
      DO 2500 I = 1, NMAX
        IF ( XC(I) .LE. A ) NO = NO + 1
2500 CONTINUE
      IF ( NO .LE. IC ) U1J = 1.0
      NSU1J = ISIM
      SU1J = SU1J + U1J
      SU1J2 = SU1J2 + U1J * U1J
C
C      Equivalent Ramp plan ( contamination ) [ given NRAMP, B, TRAMP]
C
      TOT = 0.0
      RAMPIN= 1.0/NRAMP
      IRATIO=0
      INTIAL = 1
      DO 4500 K=NRAMP,NMAX,NRAMP
        IRATIO = IRATIO + 1
        SBAR = 0.0
        DO 3500 I=INTIAL,INTIAL+NRAMP-1
          XIU = XC(I) / B
          IF ( XIU .GE. 1.0 ) SBAR = SBAR + 1.0
          IF ( XIU .LE. 0.0 .OR. XIU .GE. 1.0 ) GO TO 3500
          SBAR = SBAR + XIU
3500 CONTINUE
        QBAR = SBAR * RAMPIN
        UIJ = 0.0
        IF ( QBAR .GE. TRAMP ) UIJ = 1.0
        TOT = TOT + UIJ
        INTIAL = INTIAL + NRAMP
4500 CONTINUE

```

```

C      IF ( IRATIO .EQ. 0 ) IRATIO=1
C      DIJ = ( TOT / IRATIO ) - U1J
C      SD2J = SD2J + DIJ
C      SD2J2 = SD2J2 + DIJ * DIJ
C      NSD2J = ISIM
C
C      Similarly , we have scores for cases of other equivalent plans ; S-plan
C      and Sigma-plan .
C
C      Equivalent S-Plan (( under Contamination ))
C
C      TOT = 0.0
C      RSPLAN = 1.0 / NSPLAN
C      NRATIO = C
C      INIT = 1
C      DO 6500 L= NSPLAN, NMAX , NSPLAN
C      NRATIO=NRATIO+1
C      XBAR = 0.0
C      DO 5500 I = INIT , INIT + NSPLAN - 1
C      XBAR = XBAR + XC(I)
5500  CONTINUE
C      XBAR = XBAR * RSPLAN
C      UIJ = 0.0
C      IF ( XBAR .GE. QSPLAN ) UIJ = 1.0
C      TOT = TOT + UIJ
C      INIT = INIT + NSPLAN
6500  CONTINUE
C      DIJ = ( TOT / NRATIO ) - U1J
C      SD4J = SD4J + DIJ
C      SD4J2 = SD4J2 + DIJ * DIJ
C      NSD4J = ISIM
C
C      Equivalent Sigma-Plan (( under contaminated Noraml model ))
C
C      TOT = 0.0
C      RSIGMA= 1.0 / NSIGMA
C      IRATIO=C
C      INI = 1
C      DO 8500 L = NSIGMA,NMAX , NSIGMA
C      IRATIO=IRATIO + 1
C      XBARS = 0.0
C      DO 7500 I= INI , INI + NSIGMA-1
C      XBARS = XBARS + XC(I)
7500  CONTINUE
C      XBARS = XBARS * RSIGMA
C      UIJ = 0.0
C      IF ( XBARS .GE. AKSGMA ) UIJ = 1.0
C      TOT = TOT + UIJ
8500  CONTINUE
C      DIJ = ( TOT / IRATIO ) - U1J
C
C      SD5J = SD5J + DIJ
C      SD5J2 = SD5J2 + DIJ * DIJ
C      INI = INI + NSIGMA
C      NSD5J = ISIM
C
C      6. At the end of each simulation sample do the sums and check on whether
C      so as to use it in the final analysis when related to the "Controlled
C      variate" i.e. the attribute PA1J :
C
C      = 0 + Var(DIJ)
C
C      IF ( ISIM .LT. NSIMUL) GO TO 100
C      i.e. another round of simulation sampling ....
C
C      7. Keep track of the variability so as to use it in the final analysis
C      when related to the "Controlled Variate" i.e.the attribute PA1J:
C      Var( Pa1j) = Var ( pa1j) + Var( Dij)
C      = 0 + Var(Dij )
C
8600  CONTINUE
C
C      CLOSE ( UNIT=21,DEVICE='DSK' )
C
C      8 . Write-in the results in suitable FORMAT ....
C
C      PATTR=SU1J/NSIMUL
C      PARAMP=PACCEP + SD2J/NSIMUL
C      PASP=PACCEP + SD4J/NSIMUL
C      PASIG=PACCEP + SD5J/NSIMUL
C      SE1 = ( SU1J2 - SU1J * SU1J / NSIMUL )/(NSIMUL-1)
C      SE2 = ( SD2J2 - SD2J * SD2J / NSIMUL )/(NSIMUL-1)
C      SE4 = ( SD4J2 - SD4J * SD4J / NSIMUL)/(NSIMUL-1)
C      SE5 = ( SD5J2 - SD5J * SD5J / NSIMUL )/(NSIMUL-1)
C
C      write(NOUT,99910) B,PATTR,se1,PARAMP,se2,PASP,se4,PASIG,se5
99910  FORMAT(2X,'The "Acceptance Probability" Performances are :',/,/,
*2X,6X,' Attribu s.e. RAMP s.e. S-plan
* s.e. Sigma s.e.',/,/)
99910  FORMAT(2X,'( ',F4.1,' )',4(F8.2,F9.4))
C
9000  CONTINUE
C      WRITE(NOUT,99993) GAMMA,EMU0,SIG0,SIGC
99993  FORMAT(/,2X,' The Contamin. Fraction GAMMA = ',F7.3,' * .The
*Original process mean EMU0= ',F6.3,' * and s.d SIG0= ',F6.3,'
* ',/,2X,' ( NB :Under Different Variances, here SIGC=',F6.3,' )')
99999  WRITE(NOUT,99999)
99999  FORMAT('1')
C
C      END
C
C      -----
C
C      FUNCTION GAUINV( P , IFALT)
C      APP. STAT. (1974) VOL 23 NO. 1 PAGE 96
C
C      DATA ZERO,ONE,HALF,ALIMIT/0.0,1.0,0.5,1.0E-20/
C
C      DATA PD P1 P2 P3 /
* -.322232431088 , -1.0, -0.342242088547, -.204231210245E-1/
C      DATA P4 Q0 Q1 /
* -.453642210148E-4, 0.993484626060E-1, 0.588581570495/

```

DATA Q2 Q3 Q4 /
* 0.531103462366, 0.103537752850, 0.38560700634E-2 /

```
IF AULT=1
GAUINV=ZERO
PS=P
IF(PS .GT. HALF) PS=ONE - PS
IF(PS .LT. ALIMIT) RETURN
IF AULT=C
IF(PS .EQ. HALF) RETURN
YI=SQR(1/LOG(ONE/(PS * PS)))
GAUINV=YI + (((YI* P4 + P3)* YI + P2 ) *YI + P1)*YI + P0) /
* (((YI *Q4 + Q3)* YI + Q2)*YI+Q1)* YI + Q0)
IF ( P .LT. HALF) GAUINV= - GAUINV
RETURN
END
```

FUNCTION STNORM(N)

REAL D(32)
DATA(D(I), I=1, 32) /

1	0.67448975	0.47585963	0.383771164	0.328611323
2	0.29114283	0.26368432	0.242508450	0.225567440
3	0.21163417	0.19992427	0.189910760	0.181225180
4	0.17360140	0.16684191	0.160796730	0.15534972
5	0.15040938	0.14590258	0.141770030	0.13796317
6	0.13444176	0.13117215	0.128125970	0.12527909
7	0.12261088	0.12010356	0.117741710	0.11551189
8	0.11340235	0.11140272	0.109503850	0.10769762

DATA U/C.O /

```
A=0.0
I=0
10 U=U+U
IF(U.LT.1.0) GO TO 20
U= U - 1.0
I=I+1
A=A-D(I)
GO TO 10
20 W= D(I+1)*U
V= W*(0.5*W - A )
30 U=RAN(0)
IF (V.LE.U) GO TO 40
V = RAN(0)
IF(U.GT.V) GO TO 30
U= ( V - U) / (1.0-U)
GO TO 20
40 U=(U - V)/( 1.0 - V)
U= U + U
IF ( U.LT.1.0) GO TO 50
U = U - 1.0
STNORM= W - A
RETURN
50 STNORM = A - W
RETURN
END
```



```
C
C
C ***** Simulation Program (2) "Lognormal" *****
C
C
C Program Name : LOGNOR.FOR
C
C Purpose :
C ----- Same as in Program CONTAM.FOR except that this is one
C is for study of robustness in case of a Lognormal process .
C
C Input Data :
C ----- ( same as in the Program CONTAM.FOR )
C
C Routines and Sub-Programs :
C -----
C ( same as in CONTAM.FOR ) but also :
C
C 1. ZERO :to find the Zero of a transcendental function that
C satisfies the requirement that the overall variance
C of the Lognormal process should be 1 . ZERO relies
C on the subroutines FUN and DFUN that compute values
C of the function and its derivative , respectively .
C
C
C =====
C
C SUBROUTINE NEWRV(S(J,MORE)
C COMMON / ANEW / XN(1000)
C READ(21) XN
C J = 1001
C RETURN
C END
C
C -----
C
C ===== M A I N =====
C
C DIMENSION NAT(4),ICA(4),NRA(4),TRA(4),NSG(4),AKG(4),NSP(4),QSP(4)
C DIMENSION IEXIS(4)
C DIMENSION X(450)
C real xc(450),uu(450)
C COMMON / ANEW / XN(1000)
C DATA NSIMUL / 2000 /,PACCEP/0.95/
C
C Here , feed-in the DATA of PROP and Equivalence Parameters :
C
C DATA prop /0.0287 /
C DATA (IEXIS(J),J=1,4) / 1,1,1,1 /
C DATA ( NAT(J) ,J=1,4) /28,28,28,28 /
C DATA ( ICA(J) ,J=1,4) /2,2,2,2 /
C DATA ( NRA(J) ,J=1,4) / 8,8,8,8/
C DATA ( TRA(J) ,J=1,4) / .829, .7693, .7104, .6475 /
C DATA ( NSG(J) ,J=1,4) / 4,5,5,6/
```

```
DATA ( AKG(J) ,J=1,4)/1.14248,1.18476,1.222 .26174 /
DATA ( NSP(J) ,J=1,4)/ 6,8,8,10 /
DATA ( QSP(J) ,J=1,4)/1.20261,1.22864,1.26756,1.29779 /
```

```
=====
```

```
PACCEP=C.95
WRITE(NOUT,99901) NSIMUL,PROP
99901 FORMAT(2X,'No. of LOGNORMAL Simulations=',I7,/,
*2X,' PO =',F7.4,/,
*, ' For the Plans :',/,2X
*, ' B Natt c Nramp Tramp Nsplan QS Nsigma Ksig'
*)
991 FORMAT(2X,'( ',F4.1,')',I4,I4,I5,F7.4,I5,F7.4,I6,F7.4)
B=0.3
DO 25 J=1,4
B=B + 0.2
WRITE(NOUT,991) B,NAT(J),ICA(J),NRA(J),TRA(J),NSP(J),QSP(J)
*,NSG(J),AKG(J)
25 CONTINUE
WRITE(NOUT,99903)
```

```
DATA EPS / 0.001 /
```

```
XINV = GAUINV(PROP,IFAUULT)
IF(IFAUULT .NE. 0 ) STOP 'Inconsistent PROP '
```

```
MATCHING OF THE LOGNORMAL (or more proper to rename it "Exponormal")
such that it has p0 proportion defective and an overall variance = 1 .
```

```
Notes :
```

```
(a) If Y is N(Mstar , Sigstar) then X=EXP( Y ) is LOGNORMAL( M ,S2)
with mean M = EXP( MUstar + Sigstar**2) and variance
S2 = EXP(2.*MUstar + Sigstar*Sigstar) * ( EXP(Sigstar*Sigstar) - 1 )
(b) Suppose , for a +ve domain ,
ln Astar = MUstar + k * Sigstar
where k=PHI-1( p0 )
then we should look into transforming a N(MUstar+ln Astar ,Sigstar)
into a lognormal(M,S2)
```

```
AK = XINV
which is -ve for p0 < 0.5
```

```
(c) To match the lognormal variance S2 to 1 ( and since
MUstar=-k * Sigstar) we have to solve for Sigstar in :
exp(-2*k*Sigstar + Sigstar**2) * ( exp(Sigstar**2)-1)-1 = 0
( i.e. find the ZERO of this Transcendental function )
Sigstar will determine MUstar .The ZERO is found by the ROUTINE
```

```
CALL ZERO ( SIGO , EPS , AK ,IFAUULT)
IF (IFAUULT .NE. 0 ) STOP 'Derivat. DFUN is 0 for Newt.-Ral.'
SIGSTR = SIGO
AMUSTR = :- AK * SIGSTR
```

```
(d) Now , the Normal to be transformed into a Lognormal needs to
have a mean MUstar and standard deviation Sigstar , so
mu = Sigstar * XN(i) + MUstar
is a N( MUstar , Sigstar) , which is used in [4] below
as well as
```

```
ALNA = AMUSTR + AK * SIGSTR
ASTAR = EXP( ALNA )
```

```
Now , having matched the Lognormal and its parameters ( so as
to give a Variance = 1 and a prop. defective=p0 ) , we use the
pseudo-random normal variates and simulate the lognormal randomly
selected samples as in the following steps :
```

```
1. As done above READin current parameters the EQUIVALENT plans
to be compared (NATT,IC),(NRAMP,TRAMP,B,PO(2)),(NSIGMA,AKSGMA),
and (NSPLAN,QSPPLAN) ,...etc.
```

```
BB = 0.1
DO 9000 JB=1,4
BB = BB + 0.4
IF(IEXIS(JB) .NE. 0 ) GO TO 15
WRITE(0,19) BB
GO TO 9000
15 FORMAT(/,' At B =',F5.2,' there is a Non-Existence case ',/)
15 Natt= NAT(JB)
ic=ICA(JB)
nramp=NRA(JB)
tramp=TRA(JB)
nsigma=NSG(JB)
aksgma=AKG(JB)
nsplan=NSP(JB)
qsplan=QSP(JB)
```

```
2. Initialise the sums , sums of squares,the number of simulation
samplings, etc....
```

```
SU1J=0.0
SU1J2=0.0
SD2J=0.0
SD2J2=0.0
SD4J=0.0
SD4J2=0.0
SD5J=0.0
SD5J2=0.0
ISIM = 0
sumneg=C.0
```

```
J=1001
OPEN(UNIT=21,DEVICE='DSK',FILE='NORVS.DAT',ACCESS='SEQIN',
+ MODE='BINARY')
```

```
Read-in the Initial block of 1000 of standard normal r.v.'s :
```

```
READ(21) XN
```

```
100 ISIM = ISIM + 1
NMAX = NATT
```

```
3. In the following we are assuming we have a block of 1000 r.v.'s
```

C in the buffer array XN(1000) .Now, we select a sample for the
 C Attribute case sequentially relying on the randomization of the
 C shuffling done to the normal variates prior to storage on disc .
 C Note that if the supply of the
 C current 1000 r.v.s. is nearly exhausted MORE is supplied from storage
 C by a CALL NEWRVS(MORE , J) which reads more r.v.'s from the OPENED
 C disc file NORVS.DAT ...This happens whenever the remaining r.v.'s
 C are not exactly enough to make a new different sample . The Subroutine
 C NEWRVS provides MORE r.v.'s . THAT is , making a completely new different
 C set of 1000 uncycled r.v.'s from which further simulation samplings
 C are made ..
 C

```

DO 999 I = 1, NMAX
J=J-1
MORE=1001-J
ITH = MORE
XNORM = XN(ITH)
  
```

C 4. This XNORM is a N(0,1) to be transformed into a N(MUstar, Sigstar)
 C which is in turn "lognormalised" as Lognormal(M, S2=1) as follows :
 C

```

YNORM = SIGSTR * XNORM + AMUSTR
YEXP = EXP ( YNORM )
  
```

C YEXP comes from a Lognormal with p0 below Astar(>0) .. and for this
 C to mimick our process we require the displacement :
 C

```

XEXP = YEXP - ASTAR
X(I) = XEXP
if(xexp .le. 0.0) sumneg=sumneg+1.
IF ( J .LE. 1 ) CALL NEWRVS(MORE,J)
CONTINUE
  
```

999

C Now , we have an ATTRIBUTE complete sample from a lognormal process ...
 C

C Notice : A shuffling process is already done on the stored r.v.'s
 C prior to storing them . This is done by a randomisation procedure
 C and that is why we are reading and using the stored r.v.'s sequentially
 C Shuffling is meant to break down any pattern or sequence in the pseudo-
 C random variates used .
 C

C (NMAX is the sample size for the attribute case , the maximum n).
 C

C This X(1) is a Lognormal sample from a population with variance=1
 C Generally , on simulating the robustness of the Lognormal
 C we made use of the idea of 'CONTROL VARIATE ' by use of the
 C attribute plan whose variability is controlled and by re-use of the
 C same sample data to simulate the behaviour of each of the "Equivalent"
 C plans . Note also the economisation due to the intensive use and re-use
 C of r.v.'s of the attribute largest sample to create more than one smaller
 C samples of equivalent plans per each attribute sample.
 C

C 5. Herebelow we evaluate the Lognormal effects on the attribute as
 C well as preparing for assessing the effects on other "equivalent"
 C plans :
 C

```

NQ = 0
U1J = 0.0
A = 0.0
DO 2500 I = 1, NMAX
CONTINUE
IF ( NQ .LE. IC ) U1J = 1.0
SU1J = SU1J + U1J
SU1J2 = SU1J2 + U1J * U1J
  
```

2500

C Equivalent Ramp plan (contamination) [given NRAMP, B, TRAMP]
 C

```

TOT = 0.0
RAMPIN = 1.0/NRAMP
NRATIO = C
INITIAL = 1
DO 4500 K=NRAMP, NMAX, NRAMP
NRATIO=NRATIO+1
QBAR = 0.0
DO 3500 I=INITIAL, INITIAL+NRAMP-1
XIU = X(I) / BB
IF ( XIU .GE. 1.0 ) QBAR = QBAR + 1.0
IF ( XIU .LE. 0.0 .OR. XIU .GE. 1.0 ) GO TO 3500
QBAR = QBAR + XIU
3500 CONTINUE
QBAR = QBAR * RAMPIN
UIJ = 0.0
IF ( QBAR .GE. TRAMP ) UIJ = 1.0
TOT = TOT + UIJ
INITIAL = INITIAL + NRAMP
4500 CONTINUE
DIJ = ( TOT / NRATIO ) - U1J
SD2J = SD2J + DIJ
SD2J2 = SD2J2 + DIJ * DIJ
NSD2J = ISIM
  
```

3500

4500

C Similarly , we have scores for cases of other equivalent plans ; S-plan
 C and Sigma-plan .
 C

C Equivalent S-Plan ((under Lognormal))
 C

```

TOT = 0.0
RSPLAN = 1.0 / NSPLAN
NRATIO = C
INIT = 1
DO 6500 L= NSPLAN, NMAX , NSPLAN
NRATIO=NRATIO+1
XBAR = 0.0
DO 5500 I = INIT , INIT + NSPLAN - 1
XBAR = XBAR + X(I)
5500 CONTINUE
XBAR = XBAR * RSPLAN
UIJ = 0.0
IF ( XBAR .GE. QSPLAN ) UIJ = 1.0
TOT = TOT + UIJ
INIT = INIT + NSPLAN
6500 CONTINUE
DIJ = ( TOT / NRATIO ) - U1J
SD4J = SD4J + DIJ
SD4J2 = SD4J2 + DIJ * DIJ
NSD4J = ISIM
  
```

5500

6500

```

C      Equivalent Sigma-Plan (( under Lognormal model ))
C
C      TOT = 0.0
C      RSIGMA= 1.0 / NSIGMA
C      NRATIO = C
C      INI = 1
C      DO 8500 L = NSIGMA, NMAX , NSIGMA
C      NRATIO=NRATIO + 1
C      XBARS = 0.0
C      DO 7500 I= INI , INI + NSIGMA-1
C      XBARS = XBARS + X(I)
7500  CONTINUE
C      XBARS = XBARS * RSIGMA
C      UIJ = 0.0
C      IF ( XBARS .GE. AKSGMA ) UIJ = 1.0
C      TOT = TOT + UIJ
8500  CONTINUE
C      DIJ = ( TOT / NRATIO ) - U1J
C      SD5J = SD5J + DIJ
C      SD5J2 = SD5J2 + DIJ * DIJ
C      INI = INI + NSIGMA
C      NSD5J = ISIM
C
C
C      6. At the end of each simulation sample do the sums and check on whether
C      the number of simulations are enough (fixed). Keep track of the variability
C      so as to use it in the final analysis when related to the "Controlled
C      variate" i.e. the attribute PA1J :
C      Var(PAIJ) = Var(PA1J)+Var(mean of DIJ)
C      = 0 + Var(mean DIJ)
C
C      IF ( ISIM .LT. NSIMUL) GO TO 100
C      i.e. another round of simulation sampling ....
C
C      7. Keep track of the variability so as to use it in the final analysis
C      when related to the "Controlled Variate" i.e.the attribute PA1J:
C      Var( PAij) = Var ( Pa1j) + Var(mean Dij)
C      = 0 + Var(mean Dij )
C      which should be reported in the final analysis ...
C
C      CLOSE ( UNIT=21,DEVICE='DSK')
C
C      8 . Write-in the results in suitable FORMAT ....
C
C      PATTR=SU1J/ISIM
C      PARAMP=PACCEP + SD2J/ISIM
C      PASP=PACCEP + SD4J/ISIM
C      PASIG=PACCEP + SD5J/ISIM
C      SE1=(SU1J2 - SU1J*SU1J/ISIM)/(ISIM-1)
C      SE2=(SD2J2 - SD2J*SD2J/ISIM)/(ISIM-1)
C      SE4=(SD4J2 - SD4J*SD4J/ISIM)/ISIM
C      SE5=(SD5J2 - SD5J*SD5J/ISIM)/ISIM
C
C      write(0,99910) BB,PATTR,SE1,PARAMP,SE2,PASP,SE4,PASIG,SE5
99903  FORMAT(2X,'THE PERFORMANCES ARE :',/,2X,6X,
C      + ' PA of ATTR s.e. PA of RAMP s.e. PA of S-Plan
C      + s.e. PA of SIGMA s.e.',/)
99910  FORMAT(2X,'( ',F4.1,')',4(F8.2,F9.4))
C
9000  CONTINUE
C      WRITE(0,99999)
99999  FORMAT('1')
C
C      END
C
C      -----
C
C      SUBROUTINE ZERO( X0 ,EPS ,AK ,IFAUULT)
C
C      Choice of initial seed of the iteration by using simple
C      search and a bisection methods so as to be in the neighbourhood of
C      the ZERO .This speeds up the convergence process when using the
C      Newton-Ralphson iterative method used later below .
C      Try the lowest possible following lower and upper arbitrary
C      values :
C
110  XA = 0.1
C      XB = 1.0
20  FA = FUN( XA ,AK)
C      FB = FUN( XB , AK)
C
C      where FUN is the function to be solved for the zer .(( DFUN used later
C      is the derivative of FUN )) . Check that (XA,XB) is the right interval
C      for the solution (and possibly that XA or XB is the solution ) :
C
C      X0 = XA
C      IF ( ABS(FA) .LE. EPS) RETURN
C      X0 = XB
C      IF ( ABS(FB) .LE. EPS) RETURN
C      ADD = 1.0
C      FAFB = FA * FB
C      IF ( FAFB ) 70,70,35
35  XA = XB
C      XB = XB + ADD
C      GO TO 20
70  X0 = ( XA + XB )/2
C
C      End of Bisection and search .... X0 is the seed for the Newton-Ralphson
C      iterations ..... Possibly X0 is the ZERO of FUN :
C
75  XI = X0
C      FI = FUN ( XI , AK )
C      IF ( ABS(FI) .LE. EPS) RETURN
C      DFI = DFUN ( XI , AK)
C
C      We should not worry that the derivative DFI is 0 (or "zero-prone")
C      but a check is advisable ; thus
C
C      IFAULT = 1
C      IF ( ABS( DFI-0.0001) .LE. 0.0 ) RETURN
C      IFAULT = C
C      XI = XI - FI / DFI
C      X0 = XI
C      GO TO 75
C      RETURN

```

END

```
-----  
FUNCTION FUN ( X , AK )  
This function is the expression for Lognormal variance - 1  
REAL K  
K = - AK  
TERMK = 2.*K * X + X * X  
EXPK = EXP( TERMK )  
EXP2 = EXP( X * X )  
  
FUN = EXPK * ( EXP2 - 1.0 ) - 1.0  
RETURN  
END  
-----
```

```
FUNCTION DFUN ( X , AK )  
This is the Derivative of FUN  
REAL K  
K = - AK  
TERMK = 2. *K * X + X * X  
EXPK = EXP ( TERMK )  
EXP2 = EXP ( X * X )  
DFUN = EXPK * ( 2.*(K+X)*( EXP2 - 1.0 ) + 2.*X * EXP2 )  
RETURN  
END
```

```
-----  
FUNCTION GAUINV( P , IFAULT )  
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```

```
DATA ZERO,ONE,HALF,ALIMIT/0.0,1.0,0.5,1.0E-20/
```

```
DATA P0 P1 P2 P3 /  
* -.322232431088 -1.0 -0.342242088547 -.204231210245E-1/  
DATA P4 Q0 Q1 /  
* -.453642210148E-4 0.993484626060E-1 0.588581570495/  
DATA Q2 Q3 Q4 /  
* 0.531103462366 0.103537752850 0.38560700634E-2/
```

```
IF AULT=1  
GAUINV=ZERO  
PS=P  
IF(PS .GT. HALF) PS=ONE - PS  
IF(PS .LT. ALIMIT) RETURN  
IF AULT=0  
IF(PS .EQ. HALF) RETURN  
YI=SQRT(ALOG(ONE/(PS * PS)))  
GAUINV=YI + ((( YI* P4 + P3)* YI + P2 ) *YI + P1)*YI + P0)/  
* ((( YI *Q4 + Q3)* YI + Q2)*YI+Q1)* YI + Q0)  
IF ( P .LT. HALF ) GAUINV= - GAUINV  
RETURN  
END
```

```
=====
```

```
FUNCTION STNORM(N)
```

```
REAL D(32)  
DATA(D(I),I=1,32)/
```

1	0.67448975	0.47585963	0.383771164	0.328611323
2	0.29114283	0.26368432	0.242508450	0.225567440
3	0.21163417	0.19992427	0.189910760	0.181225180
4	0.17360140	0.16684191	0.160796730	0.15534972
5	0.15040938	0.14590258	0.141770030	0.13796317
6	0.13444176	0.13117215	0.128125970	0.12527909
7	0.12261088	0.12010356	0.117741710	0.11551189
8	0.11340235	0.11140272	0.109503850	0.10769762

```
DATA U/C.0/
```

```
A=0.0  
I=0  
10 U=U+U  
IF(U.LT.1.0) GO TO 20  
U= U - 1.0  
I=I+1  
A=A-D(I)  
GO TO 10  
20 W= D(I+1)*U  
V= W*(0.5*W - A )  
30 U=RAN(0)  
IF (V.LE.U) GO TO 40  
V = RAN(0)  
IF(U.GT.V) GO TO 30  
U= ( V - U ) / ( 1.0-U )  
GO TO 20  
40 U=(U - V)/( 1.0 - V )  
U= U + U  
IF ( U.LT.1.0 ) GO TO 50  
U = U - 1.0  
STNORM= W - A  
RETURN  
50 STNORM = A - W  
RETURN  
END
```

```
----- E n d -----
```

A	A	PPPP	PPPP	EEEEEE	N	N	DDDDD	D	I	I	X	X	X	CCCCC	1
A	A	P	P	E	N	N	D	D	I		X	X		C	111
AAAAA		PPPP	PPPP	EEEEEE	N	N	D	D	I		X	X		C	11
A	A	P	P	E	N	N	D	D	I		X	X		C	11
A	A	P	P	EEEEEE	N	N	DDDDD	D	I	I	X	X	X	CCCCC	:: IIII ::

SOME TABLES OF THE DISTRIBUTION OF average Q(X)

(the " RAMP " case)

Sample size = 4

B = 0.5 (0.2) 1.9

AMU = 0.8 (PO = 0.2119)

P1 0.1702 0.2483 0.3280 0.4061 0.4796 0.5462 0.6041 0.6525

Table with 9 columns and 47 rows of numerical data. Includes labels QMIN, SCAL, QMAX, and B = (0.5) to (1.9).

Table with 9 columns and 101 rows of numerical data. Includes labels B = (0.5) to (1.9) and values ranging from 0.1133 to 1.0000.

continued on the right

B = 0.5 (0.2) 1.9

AMU = 0.9 (PO = 0.1841)

P1 0.1605 0.2367 0.3159 0.3952 0.4714 0.5417 0.6041 0.6525

Table with 9 columns and 47 rows of numerical data. Includes labels QMIN, SCAL, QMAX, and B = (0.5) to (1.9).

Table with 9 columns and 101 rows of numerical data. Includes labels B = (0.5) to (1.9) and values ranging from 0.0830 to 1.0000.

continued on the right

Sample size = 4
P1 0.1033 0.1612 0.2278 0.3013 0.3794 0.4591 0.5372 0.6107

B = 0.5(0.2)1.9

AMU = 1.4 (PO = 0.0808)

***** continued on the right

* B =**(0.5)**(0.7)**(0.9)**(1.1)**(1.3)**(1.5)**(1.7)**(1.9)**

Sample size = 4
P1 0.0918 0.1450 0.2074 0.2778 0.3539 0.4332 0.5125 0.5886

B = 0.5(0.2)1.9

AMU = 1.5 (PO = 0.0668)

***** continued on the right

* B =**(0.5)**(0.7)**(0.9)**(1.1)**(1.3)**(1.5)**(1.7)**(1.9)**

Table with columns for P1, QMIN, SCAL, QMAX, and B values for various sample sizes from 0 to 47. Includes a note 'continued on the right' at the bottom.

Table with columns for B values corresponding to the first table, with values ranging from 0.0015 to 1.0000 for sample sizes 48 to 101. Includes a note 'continued on the right' at the bottom.

Table with columns for P1, QMIN, SCAL, QMAX, and B values for various sample sizes from 0 to 47. Includes a note 'continued on the right' at the bottom.

Table with columns for B values corresponding to the first table, with values ranging from 0.0248 to 1.0000 for sample sizes 48 to 101. Includes a note 'continued on the right' at the bottom.

Sample size = 4, B = 0.5(0.2)1.9, AMU = 2.0 (PO = 0.0228). Table with columns for sample size, B, and AMU. Rows labeled 100 QMIN, 100 SCAL, 100 QMAX, and * B, with sub-rows for samples 01 through 47. Data points are numerical values for each parameter.

Sample size = 4, B = 0.5(0.2)1.9, AMU = 2.1 (PO = 0.0179). Table with columns for sample size, B, and AMU. Rows labeled 100 QMIN, 100 SCAL, 100 QMAX, and * B, with sub-rows for samples 01 through 47. Data points are numerical values for each parameter.

Sample size = 4

B = 0.5(0.2)1.9

AMU = 2.2 (P0 = 0.0139)

P1 0.0307 0.0529 0.0829 0.1218 0.1702 0.2281 0.2946 0.3682

Table with 8 columns and 101 rows. Row 1: 100 QMIN 50.00 50.000 50.000 50.000 50.000 0.000 0.000 0.000. Row 2: 100 SCAL 0.50 0.500 0.500 0.500 0.500 1.000 1.000 1.000. Row 3: QMAX 1.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000. Subsequent rows are labeled 0-47 with values ranging from 0.0000 to 0.0326.

Table with 8 columns and 101 rows. Row 1: [48] 0.0073 0.0129 0.0215 0.0342 0.0514 0.0694 0.0879 0.1063. Row 2: [49] 0.0076 0.0135 0.0225 0.0358 0.0531 0.0712 0.0892 0.1071. Row 3: [51] 0.0577 0.0611 0.0670 0.0767 0.0931 0.1102 0.1273 0.1444. Subsequent rows are labeled 52-101 with values ranging from 0.0000 to 1.0000.

***** continued on the right *****

Sample size = 4

B = 0.5(0.2)1.9

AMU = 2.3 (P0 = 0.0107)

P1 0.0252 0.0441 0.0700 0.1043 0.1479 0.2011 0.2635 0.3339

Table with 8 columns and 101 rows. Row 1: 100 QMIN 50.00 50.000 50.000 50.000 50.000 0.000 0.000 0.000. Row 2: 100 SCAL 0.50 0.500 0.500 0.500 0.500 1.000 1.000 1.000. Row 3: QMAX 1.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000. Subsequent rows are labeled 0-47 with values ranging from 0.0000 to 0.0348.

Table with 8 columns and 101 rows. Row 1: [48] 0.0032 0.0085 0.0144 0.0235 0.0366 0.0539 0.0712 0.0879. Row 2: [49] 0.0033 0.0088 0.0151 0.0246 0.0386 0.0559 0.0732 0.0899. Row 3: [51] 0.0445 0.0470 0.0512 0.0582 0.0695 0.0835 0.1008 0.1181. Subsequent rows are labeled 52-101 with values ranging from 0.0000 to 1.0000.

***** continued on the right *****

Sample size = 8

B = 0.5 (0.2)1.9

AMU = 0.5 (P0 = 0.3085)

P1 0.1915 0.2707 0.3469 0.4172 0.4796 0.5328 0.5764 0.6107

*****	* B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **	
100 QMIN 0.00 0.000 0.000 0.000 0.000 0.000 0.000 0.000 *	[48] 0.2225 0.3050 0.3979 0.4980 0.6000 0.6975 0.7839 0.8549	
100 SCAL 1.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000 *	[49] 0.2371 0.3248 0.4215 0.5236 0.6258 0.7215 0.8046 0.8715	
QMAX 1.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000 *	[51] 0.3094 0.3866 0.4786 0.5780 0.6767 0.7668 0.8424 0.9007	
* B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **	[52] 0.3274 0.4086 0.5029 0.6029 0.7004 0.7876 0.8593 0.9133	
[0] 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 *	[53] 0.3458 0.4308 0.5272 0.6275 0.7232 0.8073 0.8749 0.9246	
[1] 0.0001 0.0001 0.0001 0.0002 0.0002 0.0002 0.0002 0.0002 *	[54] 0.3644 0.4533 0.5515 0.6515 0.7452 0.8258 0.8892 0.9348	
[2] 0.0002 0.0002 0.0002 0.0003 0.0003 0.0004 0.0004 0.0005 *	[55] 0.3834 0.4759 0.5756 0.6750 0.7663 0.8432 0.9024 0.9439	
[3] 0.0002 0.0003 0.0003 0.0004 0.0005 0.0007 0.0008 0.0010 *	[56] 0.4026 0.4986 0.5995 0.6979 0.7864 0.8594 0.9143 0.9519	
[4] 0.0003 0.0004 0.0005 0.0006 0.0008 0.0010 0.0013 0.0016 *	[57] 0.4220 0.5213 0.6230 0.7201 0.8055 0.8745 0.9252 0.9590	
[5] 0.0003 0.0005 0.0007 0.0009 0.0012 0.0016 0.0020 0.0025 *	[58] 0.4417 0.5441 0.6462 0.7415 0.8236 0.8884 0.9349 0.9653	
[6] 0.0004 0.0006 0.0009 0.0012 0.0017 0.0023 0.0030 0.0038 *	[59] 0.4615 0.5668 0.6689 0.7620 0.8405 0.9012 0.9437 0.9707	
[7] 0.0005 0.0007 0.0011 0.0016 0.0023 0.0032 0.0042 0.0055 *	[60] 0.4815 0.5893 0.6911 0.7817 0.8565 0.9129 0.9515 0.9754	
[8] 0.0006 0.0009 0.0014 0.0022 0.0031 0.0043 0.0058 0.0078 *	[61] 0.5016 0.6116 0.7127 0.8005 0.8713 0.9235 0.9584 0.9795	
[9] 0.0007 0.0011 0.0018 0.0028 0.0041 0.0057 0.0079 0.0106 *	[62] 0.5272 0.6360 0.7346 0.8186 0.8851 0.9332 0.9646 0.9830	
[10] 0.0008 0.0014 0.0023 0.0035 0.0052 0.0075 0.0104 0.0141 *	[63] 0.5572 0.6741 0.7606 0.8372 0.8983 0.9420 0.9699 0.9859	
[11] 0.0009 0.0016 0.0028 0.0044 0.0066 0.0096 0.0135 0.0185 *	[64] 0.5872 0.7116 0.7964 0.8667 0.9159 0.9509 0.9746 0.9885	
[12] 0.0010 0.0020 0.0034 0.0054 0.0083 0.0122 0.0173 0.0238 *	[65] 0.6172 0.7459 0.8296 0.8937 0.9372 0.9657 0.9787 0.9906	
[13] 0.0012 0.0024 0.0040 0.0068 0.0109 0.0157 0.0221 0.0303 *	[66] 0.6472 0.7749 0.8586 0.9187 0.9591 0.9822 0.9924 0.9994	
[14] 0.0015 0.0030 0.0050 0.0083 0.0136 0.0206 0.0287 0.0391 *	[67] 0.6772 0.8053 0.8890 0.9451 0.9815 0.9952 0.9998 1.0000	
[15] 0.0018 0.0036 0.0060 0.0102 0.0168 0.0253 0.0356 0.0486 *	[68] 0.7072 0.8353 0.9190 0.9711 0.9991 0.9999 1.0000 1.0000	
[16] 0.0022 0.0044 0.0074 0.0124 0.0200 0.0296 0.0416 0.0571 *	[69] 0.7372 0.8653 0.9490 0.9961 0.9999 1.0000 1.0000 1.0000	
[17] 0.0027 0.0054 0.0094 0.0156 0.0249 0.0369 0.0520 0.0714 *	[70] 0.7672 0.8953 0.9790 0.9999 1.0000 1.0000 1.0000 1.0000	
[18] 0.0033 0.0066 0.0114 0.0186 0.0291 0.0438 0.0627 0.0871 *	[71] 0.7972 0.9253 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[19] 0.0040 0.0080 0.0144 0.0232 0.0357 0.0524 0.0769 0.1094 *	[72] 0.8272 0.9533 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[20] 0.0048 0.0096 0.0174 0.0282 0.0438 0.0658 0.0960 0.1376 *	[73] 0.8572 0.9833 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[21] 0.0057 0.0114 0.0200 0.0320 0.0486 0.0714 0.1044 0.1494 *	[74] 0.8872 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[22] 0.0067 0.0136 0.0240 0.0384 0.0564 0.0800 0.1140 0.1604 *	[75] 0.9172 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[23] 0.0078 0.0156 0.0270 0.0426 0.0624 0.0882 0.1242 0.1736 *	[76] 0.9472 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[24] 0.0090 0.0176 0.0300 0.0468 0.0684 0.0972 0.1386 0.1936 *	[77] 0.9772 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[25] 0.0103 0.0196 0.0336 0.0516 0.0744 0.1056 0.1484 0.2064 *	[78] 0.9972 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[26] 0.0118 0.0216 0.0372 0.0564 0.0816 0.1164 0.1608 0.2184 *	[79] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[27] 0.0133 0.0240 0.0408 0.0600 0.0864 0.1224 0.1680 0.2296 *	[80] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[28] 0.0150 0.0264 0.0432 0.0636 0.0912 0.1296 0.1776 0.2448 *	[81] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[29] 0.0168 0.0288 0.0468 0.0684 0.1008 0.1416 0.1920 0.2616 *	[82] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[30] 0.0187 0.0312 0.0504 0.0720 0.1032 0.1440 0.1956 0.2688 *	[83] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[31] 0.0207 0.0336 0.0540 0.0768 0.1096 0.1512 0.2040 0.2784 *	[84] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[32] 0.0228 0.0360 0.0576 0.0816 0.1152 0.1584 0.2124 0.2880 *	[85] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[33] 0.0250 0.0384 0.0600 0.0840 0.1184 0.1632 0.2184 0.2976 *	[86] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[34] 0.0273 0.0408 0.0636 0.0888 0.1248 0.1704 0.2272 0.3072 *	[87] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[35] 0.0298 0.0432 0.0672 0.0936 0.1308 0.1776 0.2364 0.3168 *	[88] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[36] 0.0323 0.0456 0.0708 0.0972 0.1344 0.1824 0.2424 0.3264 *	[89] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[37] 0.0350 0.0480 0.0744 0.1008 0.1416 0.1904 0.2504 0.3360 *	[90] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[38] 0.0378 0.0504 0.0768 0.1032 0.1440 0.1936 0.2544 0.3456 *	[91] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[39] 0.0407 0.0528 0.0792 0.1064 0.1488 0.2000 0.2640 0.3552 *	[92] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[40] 0.0437 0.0552 0.0816 0.1104 0.1536 0.2064 0.2712 0.3648 *	[93] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[41] 0.0468 0.0576 0.0840 0.1144 0.1584 0.2136 0.2792 0.3744 *	[94] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[42] 0.0499 0.0600 0.0876 0.1184 0.1632 0.2208 0.2864 0.3840 *	[95] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[43] 0.0531 0.0624 0.0912 0.1232 0.1680 0.2280 0.2944 0.3936 *	[96] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[44] 0.0564 0.0648 0.0948 0.1284 0.1736 0.2352 0.3024 0.4032 *	[97] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[45] 0.0598 0.0672 0.0984 0.1336 0.1792 0.2424 0.3120 0.4128 *	[98] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[46] 0.0633 0.0696 0.1020 0.1392 0.1848 0.2496 0.3192 0.4224 *	[99] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[47] 0.0669 0.0720 0.1056 0.1440 0.1904 0.2568 0.3264 0.4320 *	[100] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
***** continued on the right *****	[101] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	

Sample size = 8

B = 0.5 (0.2)1.9

AMU = 0.6 (P0 = 0.2743)

P1 0.1859 0.2656 0.3437 0.4172 0.4838 0.5417 0.5901 0.6289

*****	* B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **	
100 QMIN 0.00 0.000 0.000 0.000 0.000 0.000 0.000 0.000 *	[48] 0.1571 0.2244 0.3048 0.3971 0.4976 0.6004 0.6984 0.7851	
100 SCAL 1.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000 *	[49] 0.1688 0.2414 0.3263 0.4220 0.5244 0.6271 0.7233 0.8065	
QMAX 1.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000 *	[51] 0.2300 0.2963 0.3800 0.4764 0.5787 0.6791 0.7698 0.8454	
* B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **	[52] 0.2458 0.3165 0.4036 0.5020 0.6048 0.7037 0.7913 0.8627	
[0] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *	[53] 0.2620 0.3371 0.4275 0.5277 0.6304 0.7273 0.8115 0.8786	
[1] 0.0000 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 0.0001 *	[54] 0.2787 0.3582 0.4516 0.5533 0.6554 0.7501 0.8305 0.8932	
[2] 0.0001 0.0001 0.0001 0.0001 0.0001 0.0002 0.0003 0.0004 *	[55] 0.2958 0.3798 0.4760 0.5786 0.6798 0.7717 0.8482 0.9064	
[3] 0.0001 0.0001 0.0001 0.0002 0.0003 0.0004 0.0005 0.0007 *	[56] 0.3134 0.4017 0.5005 0.6037 0.7035 0.7923 0.8647 0.9185	
[4] 0.0001 0.0001 0.0002 0.0003 0.0004 0.0005 0.0006 0.0007 *	[57] 0.3313 0.4240 0.5251 0.6285 0.7264 0.8118 0.8799 0.9293	
[5] 0.0001 0.0002 0.0003 0.0004 0.0005 0.0007 0.0009 0.0012 *	[58] 0.3496 0.4465 0.5496 0.6527 0.7485 0.8302 0.8939 0.9390	
[6] 0.0002 0.0003 0.0004 0.0006 0.0008 0.0010 0.0014 0.0018 *	[59] 0.3683 0.4693 0.5740 0.6764 0.7696 0.8474 0.9067 0.9476	
[7] 0.0002 0.0003 0.0005 0.0008 0.0011 0.0015 0.0020 0.0027 *	[60] 0.3873 0.4922 0.5982 0.6995 0.7897 0.8634 0.9183 0.9553	
[8] 0.0002 0.0004 0.0007 0.0010 0.0015 0.0021 0.0029 0.0039 *	[61] 0.4066 0.5152 0.6221 0.7219 0.8088 0.8782 0.9288 0.9620	
[9] 0.0003 0.0005 0.0008 0.0013 0.0019 0.0028 0.0040 0.0054 *	[62] 0.4318 0.5408 0.6467 0.7439 0.8269 0.8920 0.9382 0.9679	
[10] 0.0003 0.0006 0.0010 0.0017 0.0026 0.0038 0.0053 0.0074 *	[63] 0.4531 0.5621 0.6667 0.7669 0.8445 0.9047 0.9467 0.9730	
[11] 0.0004 0.0007 0.0013 0.0021 0.0033 0.0049 0.0071 0.0099 *	[64] 0.4766 0.5856 0.6895 0.7895 0.8630 0.9162 0.9543 0.9774	
[12] 0.0005 0.0009 0.0016 0.0027 0.0042 0.0063 0.0092 0.0130 *	[65] 0.5016 0.6106 0.7145 0.8145 0.8879 0.9266 0.9609 0.9813	
[13] 0.0011 0.0016 0.0024 0.0037 0.0056 0.0083 0.0119 0.0168 *	[66] 0.5283 0.6373 0.7411 0.8411 0.9145 0.9532 0.9868 0.9845	
[14] 0.0014 0.0020 0.0031 0.0047 0.0071 0.0105 0.0152 0.0215 *	[67] 0.5571 0.6661 0.7699 0.8699 0.9433 0.9820 0.9983 0.9953	
[15] 0.0017 0.0025 0.0038 0.0059 0.0089 0.0132 0.0191 0.0270 *	[68] 0.5878 0.6968 0.7968 0.8968 0.9702 0.9885 0.9966 0.9946	
[16] 0.0020 0.0031 0.0048 0.0073 0.0111 0.0164 0.0238 0.0336 *	[69] 0.6194 0.7284 0.8284 0.9284 0.9918 0.9999 0.9999 0.9999	
[17] 0.0024 0.0038 0.0058 0.0090 0.0136 0.0202 0.0292 0.0412 *	[70] 0.6539 0.7629 0.8629 0.9629 1.0000 1.0000 1.0000 1.0000	
[18] 0.0028 0.0045 0.0071 0.0110 0.0166 0.0246 0.0356 0.0501 *	[71] 0.6914 0.8004 0.9004 0.9964 1.0000 1.0000 1.0000 1.0000	
[19] 0.0033 0.0054 0.0086 0.0133 0.0201 0.0298 0.0429 0.0603 *	[72] 0.7319 0.8409 0.9409 0.9999 1.0000 1.0000 1.0000 1.0000	
[20] 0.0039 0.0064 0.0102 0.0159 0.0241 0.0357 0.0513 0.0718 *	[73] 0.7744 0.8834 0.9834 0.9999 1.0000 1.0000 1.0000 1.0000	
[21] 0.0044 0.0075 0.0121 0.0189 0.0287 0.0424 0.0608 0.0848 *	[74] 0.8189 0.9279 0.9999 1.0000 1.0000 1.0000 1.0000 1.0000	
[22] 0.0051 0.0088 0.0143 0.0224 0.0340 0.0500 0.0715 0.0992 *	[75] 0.8654 0.9744 0.9999 1.0000 1.0000 1.0000 1.0000 1.0000	
[23] 0.0058 0.0102 0.0167 0.0263 0.0399 0.0586 0.0834 0.1152 *	[76] 0.9139 0.9884 0.9999 1.0000 1.0000 1.0000 1.0000 1.0000	
[24] 0.0066 0.0117 0.0194 0.0307 0.0465 0.0682 0.0966 0.1328 *	[77] 0.9634 0.9999 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[25] 0.0073 0.0148 0.0235 0.0362 0.0543 0.0790 0.1113 0.1519 *	[78] 0.9999 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	
[26] 0.0127 0.0188 0.0284 0.0427 0.0632 0.0911 0.1274 0.1726 *	[79] 0.8364 0.8922 0.9361 0.9663 0.9843 0.9936 0.9977 0.9993	
[27] 0.0147 0.0218 0.0330 0.0495 0.0728 0.1042 0.1447 0.1948 *	[80] 0.8847 0.9030 0.9441 0.9713 0.9870 0.9948 0.9982 0.9995	
[28] 0.0169 0.0253 0.0381 0.0569 0.0833 0.1185 0.1635 0.2185 *	[81] 0.8607 0.9131 0.9513 0.9757 0.9893 0.9959 0.9986 0.9996	
[29] 0.01		

Sample size = 8	B = 0.5(0.2)1.9								AMU = 0.7 (PO = 0.2420)
P1	0.1788	0.2580	0.3373	0.4135	0.4838	0.5462	0.5994	0.6430	
100 QMIN	0.00	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
100 SCAL	1.00	1.000	1.000	1.000	1.000	1.000	1.000	1.000	
QMAX	1.00	1.000	1.000	1.000	1.000	1.000	1.000	1.000	
* B = ** (0.5)** (0.7)** (0.9)** (1.1)** (1.3)** (1.5)** (1.7)** (1.9)** *									
[0]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	[48] 0.1058 0.1575 0.2229 0.3026 0.3952 0.4965 0.6002 0.6988
[1]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	[49] 0.1147 0.1712 0.2414 0.3254 0.4213 0.5244 0.6280 0.7246
[2]	0.0000	0.0000	0.0000	0.0000	0.0001	0.0001	0.0001	0.0001	[51] 0.1636 0.2173 0.2888 0.3764 0.4756 0.5800 0.6816 0.7728
[3]	0.0000	0.0000	0.0001	0.0001	0.0001	0.0001	0.0001	0.0002	[52] 0.1767 0.2347 0.3102 0.4011 0.5024 0.6071 0.7070 0.7949
[4]	0.0000	0.0001	0.0001	0.0001	0.0001	0.0002	0.0002	0.0003	[53] 0.1903 0.2527 0.3323 0.4262 0.5292 0.6337 0.7315 0.8157
[5]	0.0001	0.0001	0.0001	0.0002	0.0002	0.0003	0.0004	0.0005	[54] 0.2044 0.2715 0.3549 0.4517 0.5559 0.6597 0.7549 0.8351
[6]	0.0001	0.0001	0.0002	0.0002	0.0003	0.0005	0.0006	0.0008	[55] 0.2190 0.2908 0.3781 0.4774 0.5823 0.6849 0.7772 0.8532
[7]	0.0001	0.0001	0.0002	0.0003	0.0005	0.0007	0.0009	0.0013	[56] 0.2341 0.3108 0.4018 0.5032 0.6085 0.7094 0.7983 0.8699
[8]	0.0001	0.0002	0.0003	0.0004	0.0007	0.0009	0.0013	0.0018	[57] 0.2497 0.3313 0.4258 0.5291 0.6342 0.7329 0.8181 0.8852
[9]	0.0001	0.0002	0.0004	0.0006	0.0009	0.0013	0.0019	0.0026	[58] 0.2659 0.3523 0.4502 0.5549 0.6593 0.7555 0.8368 0.8993
[10]	0.0001	0.0003	0.0005	0.0008	0.0012	0.0018	0.0026	0.0037	[59] 0.2825 0.3739 0.4748 0.5805 0.6838 0.7771 0.8541 0.9120
[11]	0.0002	0.0003	0.0006	0.0010	0.0015	0.0024	0.0035	0.0050	[60] 0.2995 0.3958 0.4996 0.6059 0.7076 0.7976 0.8702 0.9235
[12]	0.0002	0.0004	0.0007	0.0012	0.0020	0.0031	0.0046	0.0066	[61] 0.3170 0.4182 0.5245 0.6309 0.7306 0.8169 0.8851 0.9339
[13]	0.0005	0.0007	0.0011	0.0017	0.0027	0.0041	0.0061	0.0088	[62] 0.3345 0.4435 0.5504 0.6558 0.7529 0.8352 0.8988 0.9432
[14]	0.0006	0.0009	0.0014	0.0022	0.0035	0.0053	0.0079	0.0115	[63] 0.3499 0.4658 0.5831 0.6826 0.7749 0.8524 0.9113 0.9514
[15]	0.0008	0.0012	0.0018	0.0028	0.0044	0.0068	0.0101	0.0147	[64] 0.3651 0.4858 0.6052 0.7009 0.7829 0.8520 0.9025 0.9356
[16]	0.0009	0.0014	0.0023	0.0036	0.0056	0.0086	0.0128	0.0186	[65] 0.3800 0.5055 0.6280 0.7167 0.7887 0.8484 0.8927 0.9227
[17]	0.0011	0.0018	0.0028	0.0045	0.0070	0.0107	0.0160	0.0233	[66] 0.3945 0.5256 0.6500 0.7320 0.7959 0.8464 0.8831 0.9081
[18]	0.0013	0.0022	0.0035	0.0056	0.0087	0.0133	0.0198	0.0288	[67] 0.4086 0.5458 0.6720 0.7480 0.8009 0.8420 0.8702 0.8887
[19]	0.0016	0.0026	0.0043	0.0068	0.0107	0.0163	0.0243	0.0353	[68] 0.4223 0.5655 0.6940 0.7640 0.8079 0.8380 0.8552 0.8632
[20]	0.0018	0.0031	0.0052	0.0083	0.0130	0.0199	0.0296	0.0428	[69] 0.4356 0.5852 0.7160 0.7800 0.8159 0.8370 0.8440 0.8470
[21]	0.0021	0.0037	0.0062	0.0100	0.0157	0.0240	0.0357	0.0515	[70] 0.4485 0.6045 0.7370 0.7960 0.8239 0.8360 0.8340 0.8290
[22]	0.0025	0.0044	0.0074	0.0120	0.0189	0.0288	0.0427	0.0614	[71] 0.4610 0.6230 0.7570 0.8100 0.8299 0.8300 0.8190 0.8080
[23]	0.0029	0.0052	0.0088	0.0143	0.0225	0.0343	0.0506	0.0725	[72] 0.4732 0.6430 0.7780 0.8260 0.8379 0.8310 0.8110 0.7880
[24]	0.0033	0.0060	0.0104	0.0169	0.0266	0.0405	0.0596	0.0850	[73] 0.4841 0.6600 0.7960 0.8380 0.8419 0.8300 0.8010 0.7690
[25]	0.0047	0.0078	0.0127	0.0203	0.0316	0.0477	0.0698	0.0989	[74] 0.4936 0.6750 0.8120 0.8480 0.8439 0.8280 0.7910 0.7510
[26]	0.0066	0.0100	0.0156	0.0243	0.0373	0.0558	0.0811	0.1143	[75] 0.5017 0.6880 0.8260 0.8560 0.8439 0.8240 0.7790 0.7310
[27]	0.0078	0.0118	0.0184	0.0286	0.0436	0.0649	0.0937	0.1311	[76] 0.5084 0.7000 0.8380 0.8620 0.8419 0.8170 0.7640 0.7170
[28]	0.0090	0.0138	0.0216	0.0333	0.0506	0.0749	0.1075	0.1494	[77] 0.5137 0.7110 0.8430 0.8620 0.8339 0.8040 0.7430 0.6970
[29]	0.0104	0.0161	0.0251	0.0387	0.0585	0.0860	0.1226	0.1692	[78] 0.5176 0.7200 0.8480 0.8620 0.8299 0.7960 0.7270 0.6820
[30]	0.0119	0.0187	0.0291	0.0447	0.0672	0.0982	0.1391	0.1905	[79] 0.5200 0.7270 0.8520 0.8620 0.8259 0.7870 0.7110 0.6670
[31]	0.0136	0.0215	0.0336	0.0514	0.0768	0.1116	0.1568	0.2131	[80] 0.5210 0.7320 0.8550 0.8600 0.8209 0.7780 0.6950 0.6520
[32]	0.0154	0.0247	0.0385	0.0588	0.0874	0.1261	0.1759	0.2371	[81] 0.5206 0.7350 0.8570 0.8580 0.8159 0.7690 0.6790 0.6370
[33]	0.0173	0.0281	0.0440	0.0670	0.0990	0.1417	0.1963	0.2624	[82] 0.5189 0.7370 0.8580 0.8560 0.8119 0.7610 0.6630 0.6220
[34]	0.0195	0.0319	0.0500	0.0759	0.1115	0.1586	0.2179	0.2888	[83] 0.5158 0.7380 0.8580 0.8530 0.8079 0.7530 0.6470 0.6070
[35]	0.0218	0.0360	0.0566	0.0856	0.1251	0.1766	0.2407	0.3163	[84] 0.5113 0.7380 0.8570 0.8500 0.8039 0.7450 0.6310 0.5920
[36]	0.0243	0.0406	0.0638	0.0962	0.1397	0.1958	0.2646	0.3447	[85] 0.5054 0.7370 0.8550 0.8460 0.7979 0.7350 0.6130 0.5750
[37]	0.0280	0.0461	0.0720	0.1078	0.1555	0.2162	0.2896	0.3738	[86] 0.4981 0.7340 0.8520 0.8410 0.7909 0.7240 0.5930 0.5570
[38]	0.0388	0.0567	0.0837	0.1219	0.1731	0.2380	0.3157	0.4037	[87] 0.4894 0.7290 0.8480 0.8350 0.7829 0.7120 0.5730 0.5390
[39]	0.0447	0.0645	0.0942	0.1359	0.1912	0.2606	0.3425	0.4339	[88] 0.4793 0.7220 0.8430 0.8280 0.7729 0.7000 0.5530 0.5200
[40]	0.0499	0.0723	0.1051	0.1507	0.2103	0.2841	0.3701	0.4644	[89] 0.4678 0.7130 0.8360 0.8190 0.7609 0.6840 0.5300 0.4980
[41]	0.0555	0.0807	0.1169	0.1664	0.2304	0.3085	0.3982	0.4951	[90] 0.4549 0.7020 0.8230 0.8050 0.7429 0.6620 0.5000 0.4690
[42]	0.0614	0.0897	0.1295	0.1832	0.2515	0.3338	0.4269	0.5256	[91] 0.4406 0.6890 0.8080 0.7890 0.7229 0.6380 0.4700 0.4400
[43]	0.0678	0.0993	0.1430	0.2008	0.2736	0.3598	0.4558	0.5560	[92] 0.4250 0.6740 0.7910 0.7700 0.7009 0.6120 0.4400 0.4110
[44]	0.0746	0.1096	0.1573	0.2195	0.2965	0.3864	0.4849	0.5859	[93] 0.4081 0.6570 0.7720 0.7490 0.6759 0.5820 0.4100 0.3820
[45]	0.0817	0.1206	0.1725	0.2390	0.3202	0.4135	0.5141	0.6153	[94] 0.3898 0.6380 0.7510 0.7260 0.6489 0.5500 0.3700 0.3430
[46]	0.0893	0.1322	0.1885	0.2594	0.3446	0.4410	0.5431	0.6440	[95] 0.3702 0.6170 0.7280 0.7010 0.6199 0.5160 0.3400 0.3140
[47]	0.0974	0.1446	0.2053	0.2806	0.3696	0.4687	0.5718	0.6719	[96] 0.3493 0.5940 0.7030 0.6740 0.5879 0.4780 0.3000 0.2750
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Sample size = 8	B = 0.5(0.2)1.9								AMU = 0.8 (PO = 0.2119)
P1	0.1702	0.2483	0.3280	0.4061	0.4796	0.5462	0.6041	0.6525	
100 QMIN	0.00	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
100 SCAL	1.00	1.000	1.000	1.000	1.000	1.000	1.000	1.000	
QMAX	1.00	1.000	1.000	1.000	1.000	1.000	1.000	1.000	
* B = ** (0.5)** (0.7)** (0.9)** (1.1)** (1.3)** (1.5)** (1.7)** (1.9)** *									
[0]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	[48] 0.0679 0.1053 0.1553 0.2199 0.2996 0.3929 0.4951 0.5996
[1]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	[49] 0.0743 0.1157 0.1701 0.2393 0.3233 0.4200 0.5241 0.6285
[2]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	[51] 0.1113 0.1521 0.2095 0.2841 0.3742 0.4756 0.5816 0.6840
[3]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0001	0.0001	[52] 0.1215 0.1663 0.2278 0.3064 0.4000 0.5035 0.6097 0.7104
[4]	0.0000	0.0000	0.0000	0.0000	0.0001	0.0001	0.0001	0.0001	[53] 0.1322 0.1812 0.2470 0.3295 0.4262 0.5313 0.6373 0.7357
[5]	0.0000	0.0000	0.0000	0.0001	0.0001	0.0001	0.0002	0.0002	[54] 0.1435 0.1968 0.2669 0.3533 0.4527 0.5590 0.6641 0.7598
[6]	0.0000	0.0000	0.0001	0.0001	0.0001	0.0002	0.0003	0.0004	[55] 0.1553 0.2132 0.2876 0.3777 0.4796 0.5865 0.6902 0.7827
[7]	0.0000	0.0001	0.0001	0.0001	0.0002	0.0003	0.0004	0.0005	[56] 0.1676 0.2304 0.3091 0.4026 0.5065 0.6136 0.7154 0.8042
[8]	0.0000	0.0001	0.0001	0.0002	0.0003	0.0004	0.0006	0.0008	[57] 0.1805 0.2482 0.3313 0.4280 0.5335 0.6402 0.7397 0.8245
[9]	0.0000	0.0001	0.0001	0.0002	0.0004	0.0006	0.0008	0.0012	[58] 0.1939 0.2667 0.3540 0.4537 0.5604 0.6662 0.7628 0.8434
[10]	0.0001	0.0001	0.0002	0.0003	0.0005	0.0008	0.0012	0.0017	[59] 0.2079 0.2859 0.3774 0.4797 0.5870 0.6915 0.7848 0.8609
[11]	0.0001	0.0001	0.0002	0.0004	0.0007	0.0011	0.0016	0.0024	[60] 0.2224 0.3057 0.4013 0.5058 0.6134 0.7159 0.8056 0.8771
[12]	0.0001	0.0002	0.0003	0.0005	0.0009	0.0014	0.0022	0.0032	[61] 0.2374 0.3262 0.4256 0.5320 0.6393 0.7394 0.8252 0.8919
[13]	0.0002	0.0003	0.0005	0.0008	0.0012	0.0019	0.0029	0.0043	[62] 0.2580 0.3498 0.4514 0.5586 0.6648 0.7620 0.8435 0.9055

Sample size = 8	B = 0.5(0.2)1.9								AMU = 0.9 (PO = 0.1841)
P1	0.1605	0.2367	0.3159	0.3952	0.4714	0.5417	0.6041	0.6573	
100 QMIN	0.00	0.000	0.000	0.000	0.000	0.000	0.000	0.000	*
100 SCAL	1.00	1.000	1.000	1.000	1.000	1.000	1.000	1.000	*
QMAX	1.00	1.000	1.000	1.000	1.000	1.000	1.000	1.000	*
* B =** (0.5)** (0.7)** (0.9)** (1.1)** (1.3)** (1.5)** (1.7)** (1.9)****									
[0]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*
[1]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*
[2]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*
[3]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*
[4]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*
[5]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0001	0.0001	0.0001	*
[6]	0.0000	0.0000	0.0000	0.0000	0.0001	0.0001	0.0001	0.0001	*
[7]	0.0000	0.0000	0.0000	0.0000	0.0001	0.0001	0.0002	0.0002	*
[8]	0.0000	0.0000	0.0000	0.0001	0.0001	0.0002	0.0002	0.0003	*
[9]	0.0000	0.0000	0.0001	0.0001	0.0002	0.0002	0.0003	0.0005	*
[10]	0.0000	0.0000	0.0001	0.0001	0.0002	0.0003	0.0005	0.0007	*
[11]	0.0000	0.0000	0.0001	0.0002	0.0003	0.0004	0.0007	0.0010	*
[12]	0.0000	0.0001	0.0001	0.0002	0.0004	0.0006	0.0010	0.0015	*
[13]	0.0001	0.0001	0.0002	0.0003	0.0005	0.0008	0.0013	0.0020	*
[14]	0.0001	0.0002	0.0003	0.0004	0.0007	0.0011	0.0018	0.0027	*
[15]	0.0001	0.0002	0.0003	0.0006	0.0009	0.0015	0.0023	0.0036	*
[16]	0.0002	0.0003	0.0004	0.0007	0.0012	0.0019	0.0031	0.0048	*
[17]	0.0002	0.0003	0.0006	0.0009	0.0015	0.0025	0.0040	0.0062	*
[18]	0.0002	0.0004	0.0007	0.0012	0.0020	0.0032	0.0051	0.0079	*
[19]	0.0003	0.0005	0.0009	0.0015	0.0025	0.0041	0.0065	0.0101	*
[20]	0.0004	0.0006	0.0011	0.0019	0.0032	0.0052	0.0082	0.0127	*
[21]	0.0004	0.0008	0.0014	0.0024	0.0039	0.0064	0.0102	0.0159	*
[22]	0.0005	0.0009	0.0017	0.0029	0.0049	0.0080	0.0127	0.0196	*
[23]	0.0006	0.0011	0.0020	0.0036	0.0060	0.0098	0.0156	0.0240	*
[24]	0.0007	0.0013	0.0025	0.0043	0.0073	0.0119	0.0189	0.0291	*
[25]	0.0010	0.0018	0.0031	0.0053	0.0089	0.0145	0.0229	0.0351	*
[26]	0.0015	0.0024	0.0039	0.0066	0.0109	0.0176	0.0276	0.0420	*
[27]	0.0018	0.0029	0.0048	0.0080	0.0131	0.0211	0.0329	0.0499	*
[28]	0.0022	0.0035	0.0058	0.0096	0.0157	0.0251	0.0390	0.0588	*
[29]	0.0026	0.0042	0.0070	0.0115	0.0187	0.0297	0.0460	0.0689	*
[30]	0.0030	0.0050	0.0083	0.0137	0.0221	0.0350	0.0539	0.0801	*
[31]	0.0035	0.0059	0.0098	0.0162	0.0261	0.0411	0.0627	0.0927	*
[32]	0.0041	0.0069	0.0116	0.0190	0.0306	0.0478	0.0726	0.1065	*
[33]	0.0047	0.0081	0.0136	0.0223	0.0357	0.0555	0.0836	0.1217	*
[34]	0.0054	0.0094	0.0159	0.0260	0.0414	0.0640	0.0957	0.1383	*
[35]	0.0061	0.0109	0.0184	0.0301	0.0478	0.0734	0.1090	0.1562	*
[36]	0.0069	0.0125	0.0213	0.0348	0.0549	0.0838	0.1235	0.1756	*
[37]	0.0082	0.0146	0.0247	0.0401	0.0629	0.0953	0.1393	0.1963	*
[38]	0.0122	0.0188	0.0297	0.0467	0.0721	0.1080	0.1565	0.2184	*
[39]	0.0145	0.0220	0.0344	0.0536	0.0820	0.1218	0.1748	0.2417	*
[40]	0.0166	0.0254	0.0395	0.0611	0.0927	0.1366	0.1944	0.2663	*
[41]	0.0189	0.0291	0.0451	0.0694	0.1045	0.1526	0.2152	0.2919	*
[42]	0.0214	0.0332	0.0514	0.0785	0.1173	0.1698	0.2372	0.3187	*
[43]	0.0241	0.0376	0.0582	0.0885	0.1311	0.1882	0.2603	0.3463	*
[44]	0.0271	0.0426	0.0657	0.0993	0.1460	0.2077	0.2846	0.3747	*
[45]	0.0303	0.0479	0.0739	0.1110	0.1620	0.2283	0.3098	0.4038	*
[46]	0.0337	0.0538	0.0828	0.1237	0.1790	0.2499	0.3359	0.4334	*
[47]	0.0375	0.0601	0.0925	0.1373	0.1971	0.2727	0.3627	0.4633	*

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* B =** (0.5)** (0.7)** (0.9)** (1.1)** (1.3)** (1.5)** (1.7)** (1.9)****	[48]	0.0415	0.0670	0.1029	0.1519	0.2162	0.2963	0.3903	0.4934
[49]	0.0458	0.0744	0.1141	0.1674	0.2364	0.3209	0.4184	0.5235	
[51]	0.0723	0.1016	0.1449	0.2044	0.2809	0.3729	0.4759	0.5832	
[52]	0.0799	0.1124	0.1596	0.2233	0.3041	0.3996	0.5049	0.6124	
[53]	0.0879	0.1240	0.1752	0.2432	0.3281	0.4269	0.5339	0.6410	
[54]	0.0964	0.1364	0.1917	0.2641	0.3528	0.4545	0.5627	0.6688	
[55]	0.1054	0.1495	0.2091	0.2858	0.3783	0.4824	0.5912	0.6958	
[56]	0.1149	0.1633	0.2275	0.3083	0.4043	0.5105	0.6192	0.7217	
[57]	0.1250	0.1780	0.2466	0.3317	0.4308	0.5385	0.6467	0.7466	
[58]	0.1355	0.1933	0.2667	0.3558	0.4577	0.5664	0.6735	0.7703	
[59]	0.1466	0.2095	0.2875	0.3805	0.4848	0.5941	0.6995	0.7927	
[60]	0.1582	0.2264	0.3092	0.4057	0.5121	0.6213	0.7246	0.8139	
[61]	0.1704	0.2440	0.3315	0.4315	0.5394	0.6480	0.7486	0.8337	
[62]	0.1876	0.2648	0.3557	0.4581	0.5668	0.6742	0.7716	0.8521	
[63]	0.2353	0.3023	0.3880	0.4880	0.5951	0.6999	0.7935	0.8692	
[64]	0.2562	0.3257	0.4136	0.5150	0.6218	0.7244	0.8141	0.8848	
[65]	0.2731	0.3472	0.4385	0.5415	0.6478	0.7479	0.8334	0.8992	
[66]	0.2905	0.3693	0.4637	0.5679	0.6733	0.7704	0.8514	0.9122	
[67]	0.3084	0.3919	0.4892	0.5942	0.6982	0.7919	0.8682	0.9240	
[68]	0.3268	0.4149	0.5149	0.6203	0.7223	0.8122	0.8837	0.9346	
[69]	0.3456	0.4384	0.5407	0.6460	0.7456	0.8313	0.8979	0.9441	
[70]	0.3649	0.4622	0.5665	0.6711	0.7679	0.8493	0.9109	0.9525	
[71]	0.3847	0.4863	0.5922	0.6958	0.7893	0.8660	0.9226	0.9599	
[72]	0.4048	0.5106	0.6177	0.7197	0.8096	0.8815	0.9333	0.9663	
[73]	0.4252	0.5351	0.6430	0.7429	0.8288	0.8958	0.9428	0.9719	
[74]	0.4460	0.5597	0.6678	0.7653	0.8468	0.9089	0.9513	0.9768	
[75]	0.5042	0.6017	0.6993	0.7892	0.8644	0.9210	0.9588	0.9809	
[76]	0.5622	0.6423	0.7290	0.8113	0.8805	0.9318	0.9654	0.9845	
[77]	0.5821	0.6643	0.7503	0.8296	0.8945	0.9414	0.9711	0.9874	
[78]	0.6020	0.6861	0.7709	0.8470	0.9075	0.9500	0.9760	0.9899	
[79]	0.6218	0.7074	0.7908	0.8634	0.9195	0.9576	0.9803	0.9920	
[80]	0.6416	0.7284	0.8100	0.8788	0.9303	0.9643	0.9839	0.9937	
[81]	0.6613	0.7490	0.8284	0.8931	0.9402	0.9702	0.9870	0.9951	
[82]	0.6809	0.7690	0.8458	0.9064	0.9490	0.9754	0.9896	0.9962	
[83]	0.7003	0.7885	0.8624	0.9186	0.9569	0.9798	0.9918	0.9971	
[84]	0.7195	0.8074	0.8780	0.9298	0.9639	0.9836	0.9935	0.9978	
[85]	0.7385	0.8257	0.8927	0.9400	0.9700	0.9868	0.9950	0.9984	
[86]	0.7572	0.8432	0.9064	0.9492	0.9753	0.9895	0.9961	0.9988	
[87]	0.7756	0.8600	0.9191	0.9574	0.9799	0.9917	0.9971	0.9991	
[88]	0.8663	0.9054	0.9406	0.9674	0.9845	0.9937	0.9978	0.9994	
[89]	0.8765	0.9150	0.9483	0.9725	0.9874	0.9951	0.9984	0.9996	
[90]	0.8863	0.9241	0.9553	0.9771	0.9899	0.9962	0.9988	0.9997	
[91]	0.8958	0.9327	0.9618	0.9812	0.9921	0.9972	0.9992	0.9998	
[92]	0.9050	0.9409	0.9677	0.9847	0.9938	0.9979	0.9994	0.9999	
[93]	0.9139	0.9484	0.9730	0.9878	0.9953	0.9985	0.9996	0.9999	
[94]	0.9224	0.9555	0.9777	0.9904	0.9965	0.9990	0.9997	0.9999	
[95]	0.9306	0.9621	0.9820	0.9927	0.9975	0.9993	0.9998	1.0000	
[96]	0.9384	0.9681	0.9857	0.9945	0.9982	0.9995	0.9999	1.0000	
[97]	0.9459	0.9737	0.9899	0.9961	0.9988	0.9997	0.9999	1.0000	
[98]	0.9529	0.9787	0.9917	0.9973	0.9993	0.9998	1.0000	1.0000	
[99]	0.9596	0.9833							

Sample size = 8

B = 0.5(0.2)1.9

AMU = 1.1 (P0 = 0.1357)

Table with 10 columns for P1 values (0.1386 to 0.6525) and 10 columns for B values (0.5 to 1.9). Rows include QMIN, SCAL, QMAX, and individual data points from [0] to [101].

Sample size = 8

B = 0.5(0.2)1.9

AMU = 1.2 (P0 = 0.1131)

Table with 10 columns for P1 values (0.1269 to 0.6430) and 10 columns for B values (0.5 to 1.9). Rows include QMIN, SCAL, QMAX, and individual data points from [0] to [101].

Sample size = 8

B = 0.5(0.2)1.9

AMU = 1.3 (PO = 0.0968)

P1 0.1151 0.1775 0.2478 0.3239 0.4032 0.4825 0.5586 0.6289

100 QMIN 0.00 0.000 0.000 0.000 0.000 0.000 0.000 0.000 *

100 SCAL 1.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000 *

QMAX 1.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000 *

* B =**(0.5)**(0.7)**(0.9)**(1.1)**(1.3)**(1.5)**(1.7)**(1.9)***

[0] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[1] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[2] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[3] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[4] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[5] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[6] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[7] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[8] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[9] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[10] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[11] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[12] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[13] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[14] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 *

[15] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 0.0001 *

[16] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 0.0001 *

[17] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 0.0001 0.0002 *

[18] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 0.0002 0.0003 *

[19] 0.0000 0.0000 0.0000 0.0000 0.0001 0.0001 0.0002 0.0004 *

[20] 0.0000 0.0000 0.0000 0.0000 0.0001 0.0002 0.0003 0.0005 *

[21] 0.0000 0.0000 0.0000 0.0001 0.0001 0.0002 0.0004 0.0007 *

[22] 0.0000 0.0000 0.0000 0.0001 0.0002 0.0003 0.0005 0.0009 *

[23] 0.0000 0.0000 0.0001 0.0001 0.0002 0.0004 0.0007 0.0012 *

[24] 0.0000 0.0000 0.0001 0.0001 0.0003 0.0005 0.0009 0.0016 *

[25] 0.0000 0.0000 0.0001 0.0002 0.0003 0.0006 0.0012 0.0021 *

[26] 0.0000 0.0001 0.0001 0.0002 0.0004 0.0008 0.0015 0.0027 *

[27] 0.0001 0.0001 0.0002 0.0003 0.0006 0.0010 0.0019 0.0034 *

[28] 0.0001 0.0001 0.0002 0.0004 0.0007 0.0013 0.0024 0.0043 *

[29] 0.0001 0.0001 0.0003 0.0005 0.0009 0.0017 0.0031 0.0054 *

[30] 0.0001 0.0002 0.0003 0.0006 0.0012 0.0021 0.0038 0.0068 *

[31] 0.0001 0.0002 0.0004 0.0008 0.0014 0.0027 0.0048 0.0084 *

[32] 0.0001 0.0003 0.0005 0.0010 0.0018 0.0033 0.0059 0.0104 *

[33] 0.0002 0.0003 0.0006 0.0012 0.0022 0.0041 0.0073 0.0127 *

[34] 0.0002 0.0004 0.0008 0.0015 0.0028 0.0050 0.0090 0.0155 *

[35] 0.0002 0.0005 0.0010 0.0018 0.0034 0.0062 0.0109 0.0187 *

[36] 0.0003 0.0006 0.0012 0.0023 0.0042 0.0075 0.0132 0.0226 *

[37] 0.0004 0.0007 0.0015 0.0028 0.0051 0.0091 0.0159 0.0270 *

[38] 0.0006 0.0011 0.0019 0.0034 0.0062 0.0110 0.0191 0.0321 *

[39] 0.0008 0.0013 0.0023 0.0042 0.0075 0.0132 0.0228 0.0380 *

[40] 0.0010 0.0016 0.0029 0.0051 0.0090 0.0158 0.0270 0.0447 *

[41] 0.0012 0.0020 0.0035 0.0061 0.0109 0.0189 0.0319 0.0524 *

[42] 0.0014 0.0024 0.0042 0.0074 0.0130 0.0223 0.0375 0.0610 *

[43] 0.0017 0.0029 0.0050 0.0088 0.0154 0.0264 0.0439 0.0707 *

[44] 0.0019 0.0034 0.0060 0.0105 0.0182 0.0309 0.0511 0.0815 *

[45] 0.0023 0.0041 0.0072 0.0125 0.0215 0.0362 0.0592 0.0936 *

[46] 0.0026 0.0048 0.0085 0.0147 0.0252 0.0421 0.0683 0.1068 *

[47] 0.0030 0.0056 0.0100 0.0173 0.0294 0.0488 0.0784 0.1214 *

***** continued on the right *****

* B =**(0.5)**(0.7)**(0.9)**(1.1)**(1.3)**(1.5)**(1.7)**(1.9)***

[48] 0.0035 0.0065 0.0117 0.0203 0.0343 0.0563 0.0896 0.1373 *

[49] 0.0040 0.0076 0.0137 0.0236 0.0397 0.0647 0.1020 0.1546 *

[51] 0.0081 0.0124 0.0200 0.0327 0.0532 0.0847 0.1305 0.1935 *

[52] 0.0094 0.0145 0.0233 0.0379 0.0611 0.0962 0.1467 0.2149 *

[53] 0.0109 0.0169 0.0271 0.0437 0.0698 0.1089 0.1642 0.2378 *

[54] 0.0125 0.0196 0.0314 0.0503 0.0795 0.1227 0.1830 0.2619 *

[55] 0.0143 0.0226 0.0361 0.0575 0.0902 0.1378 0.2032 0.2873 *

[56] 0.0162 0.0260 0.0415 0.0656 0.1020 0.1541 0.2246 0.3139 *

[57] 0.0184 0.0298 0.0474 0.0746 0.1148 0.1717 0.2474 0.3415 *

[58] 0.0208 0.0339 0.0540 0.0845 0.1288 0.1906 0.2714 0.3701 *

[59] 0.0233 0.0385 0.0613 0.0953 0.1440 0.2107 0.2966 0.3995 *

[60] 0.0261 0.0435 0.0694 0.1071 0.1604 0.2321 0.3229 0.4296 *

[61] 0.0292 0.0490 0.0782 0.1200 0.1780 0.2548 0.3502 0.4602 *

[62] 0.0341 0.0561 0.0884 0.1343 0.1971 0.2787 0.3784 0.4912 *

[63] 0.0509 0.0716 0.1043 0.1522 0.2185 0.3043 0.4076 0.5224 *

[64] 0.0587 0.0818 0.1175 0.1694 0.2402 0.3305 0.4373 0.5535 *

[65] 0.0654 0.0916 0.1311 0.1874 0.2630 0.3576 0.4674 0.5844 *

[66] 0.0725 0.1022 0.1457 0.2067 0.2869 0.3856 0.4979 0.6150 *

[67] 0.0801 0.1136 0.1615 0.2271 0.3120 0.4144 0.5286 0.6450 *

[68] 0.0882 0.1258 0.1783 0.2488 0.3382 0.4439 0.5593 0.6744 *

[69] 0.0969 0.1390 0.1963 0.2716 0.3653 0.4738 0.5898 0.7028 *

[70] 0.1061 0.1530 0.2154 0.2956 0.3933 0.5041 0.6200 0.7303 *

[71] 0.1159 0.1680 0.2357 0.3207 0.4220 0.5346 0.6497 0.7565 *

[72] 0.1263 0.1839 0.2570 0.3468 0.4514 0.5652 0.6787 0.7815 *

[73] 0.1373 0.2007 0.2795 0.3738 0.4813 0.5955 0.7069 0.8052 *

[74] 0.1489 0.2185 0.3030 0.4018 0.5116 0.6256 0.7341 0.8274 *

[75] 0.1927 0.2563 0.3377 0.4352 0.5440 0.6558 0.7604 0.8481 *

[76] 0.2403 0.2969 0.3740 0.4692 0.5762 0.6852 0.7853 0.8672 *

[77] 0.2572 0.3191 0.4005 0.4985 0.6061 0.7131 0.8087 0.8848 *

[78] 0.2748 0.3422 0.4278 0.5282 0.6357 0.7400 0.8307 0.9008 *

[79] 0.2930 0.3660 0.4558 0.5581 0.6649 0.7659 0.8512 0.9152 *

[80] 0.3118 0.3907 0.4843 0.5881 0.6936 0.7906 0.8703 0.9282 *

[81] 0.3313 0.4160 0.5133 0.6180 0.7215 0.8140 0.8878 0.9397 *

[82] 0.3514 0.4420 0.5427 0.6477 0.7485 0.8360 0.9038 0.9499 *

[83] 0.3722 0.4686 0.5723 0.6770 0.7745 0.8566 0.9182 0.9588 *

[84] 0.3935 0.4958 0.6020 0.7058 0.7993 0.8756 0.9311 0.9664 *

[85] 0.4153 0.5234 0.6317 0.7338 0.8228 0.8931 0.9426 0.9730 *

[86] 0.4378 0.5514 0.6613 0.7610 0.8449 0.9091 0.9527 0.9785 *

[87] 0.4607 0.5798 0.6905 0.7872 0.8656 0.9235 0.9615 0.9832 *

[88] 0.6280 0.6871 0.7564 0.8270 0.8896 0.9377 0.9693 0.9870 *

[89] 0.6468 0.7089 0.7785 0.8467 0.9051 0.9483 0.9755 0.9901 *

[90] 0.6657 0.7305 0.8000 0.8655 0.9194 0.9576 0.9808 0.9926 *

[91] 0.6846 0.7520 0.8208 0.8831 0.9324 0.9658 0.9852 0.9946 *

[92] 0.7036 0.7731 0.8409 0.8996 0.9441 0.9729 0.9888 0.9961 *

[93] 0.7225 0.7938 0.8601 0.9150 0.9546 0.9790 0.9918 0.9973 *

[94] 0.7414 0.8141 0.8785 0.9291 0.9638 0.9841 0.9941 0.9982 *

[95] 0.7602 0.8340 0.8958 0.9420 0.9718 0.9883 0.9959 0.9988 *

[96] 0.7788 0.8532 0.9122 0.9535 0.9787 0.9917 0.9973 0.9993 *

[97] 0.7972 0.8718 0.9274 0.9639 0.9845 0.9944 0.9983 0.9996 *

[98] 0.8155 0.8897 0.9414 0.9729 0.9893 0.9964 0.9990 0.9998 *

[99] 0.8334 0.9068 0.9543 0.9807 0.9931 0.9979 0.9995 0.9999 *

[100] 0.8511 0.9230 0.9659 0.9873 0.9961 0.9990 0.9998 1.0000 *

[101] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *

Sample size = 8

P1 0.1033 0.1612 0.2278 0.3013 0.3794 0.4591 0.5372 0.6107

100 QMIN 0.00 0.000 0.000 0.000 0.000 0.000 0.000 0.000 *

100 SCAL 1.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000 *

QMAX 1.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000 *

* B =**(0.5)**(0.7)**(0.9)**(1.1)**(1.3)**(1.5)**(1.7)**(1.9)***

[0] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[1] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[2] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[3] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[4] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[5] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[6] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[7] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[8] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[9] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[10] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[11] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[12] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[13] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[14] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[15] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *

[16] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 *

[17] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 *

[18] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 0.0001 *

[19] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 0.0001 *

[20] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 0.0002 *

[21] 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 0.0001 0.0003 *

[22] 0.0000 0.0000 0.0000 0.0000 0.0001 0.0001 0.0002 0.0004 *

[23] 0.0000 0.0000 0.0000 0.0000 0.0001 0.0001 0.0003 0.0005 *

[24] 0.0000 0.0000 0.0000 0.0000 0.0001 0.0002 0.0004 0.0007 *

[25] 0.0000 0.0000 0.0000 0.0001 0.0001 0.0002 0.0005 0.0009 *

[26] 0.0000 0.0000 0.0000 0.0001 0.0002 0.0003 0.0006 0.0011 *

[27] 0.0000 0.0000 0.0001 0.0001 0.0002 0.0004 0.0008 0.0015 *

[28] 0.0000 0.0000 0.0001 0.0001 0.0003 0.0005 0.0010 0.0019 *

[29] 0.0000 0.0001 0.0001 0.0002 0.0004 0.0007 0.0013 0.0024 *

[30] 0.0000 0.0001 0.0001 0.0002 0.0005 0.0009 0.0017 0.0031 *

[31] 0.0000 0.0001 0.0002 0.0003 0.0006 0.0011 0.0021 0.0039 *

[32] 0.0001 0.0001 0.0002 0.0004 0.0008 0.0014 0.0027 0.0049 *

[33] 0.0001 0.0001 0.0003 0.0005 0.0010 0.0018 0.0034 0.0062 *

[34] 0.0001 0.0002 0.0003 0.0006 0.0012 0.0023 0.0042 0.0076 *

[35] 0.0001 0.0002 0.0004 0.0008 0.0015 0.0028 0.0052 0.0094 *

[36] 0.0001 0.0002 0.0005 0.0010 0.0019 0.0035 0.0065 0.0115 *

[37] 0.0001 0.0003 0.0006 0.0012 0.0023 0.0043 0.0079 0.0141 *

[38] 0.0003 0.0005 0.0008 0.0015 0.0029 0.0053 0.0097 0.0170 *

[39] 0.0003 0.0006 0.0010 0.0019 0.0036 0.0065 0.0117 0.0205 *

[40] 0.0004 0.0007 0.0013 0.0024 0.0044 0.0079 0.0142 0.0246 *

[41] 0.0005 0.0009 0.0016 0.0029 0.0053 0.0096 0.0170 0.0293 *

[42] 0.0006 0.0011 0.0019 0.0035 0.0064 0.0116 0.0204 0.0347 *

[43] 0.0007 0.0013 0.0024 0.0043 0.0078 0.0139 0.0242 0.0410 *

[44] 0.0009 0.0016 0.0029 0.0052 0.0094 0.0166 0.0287 0.0481 *

[45] 0.0010 0.0019 0.0035 0.0063 0.0112 0.0197 0.0338 0.0561 *

[46] 0.0012 0.0023 0.0042 0.0075 0.0134 0.0233 0.0397 0.0652 *

[47] 0.0014 0.0027 0.0050 0.0090 0.0159 0.0275 0.0463 0.0754 *

***** continued on the right *****

* B =**(0.5)**(0.7)**(0.9)**(1.1)**(1.3)**(1.5)**(1.7)**(1.9)***

[48] 0.0017 0.0032 0.0059 0.0107 0.0188 0.0323 0.0538 0.0867 *

[49] 0.0019 0.0038 0.0070 0.0126 0.0221 0.0377 0.0623 0.0993 *

[51] 0.0042 0.0065 0.0107 0.0181 0.0306 0.0510 0.0824 0.1285 *

[52] 0.0049 0.0077 0.0127 0.0213 0.0357 0.0589 0.0942 0.1451 *

[53] 0.0058 0.0091 0.0150 0.0250 0.0415 0.0677 0.1071 0.1632 *

[54] 0.0067 0.0107 0.0176 0.0292 0.0480 0.0775 0.1213 0.1827 *

[55] 0.0077 0.0126 0.0206 0.0339 0.0554 0.0884 0.1369 0.2036 *

[56] 0.0089 0.0146 0.0240 0.0393 0.0636 0.1005 0.1538 0.2260 *

[57] 0.0102 0.0169 0.0278 0.0454 0.0727 0.1137 0.1720 0.2498 *

[58] 0.0116 0.0195 0.0322 0.0521 0.0829 0.1282 0.1917 0.2748 *

[59] 0.0132 0.0224 0.0370 0.0597 0.0941 0.1440 0.2127 0.3012 *

[60] 0.0149 0.0257 0.0424 0.0681 0.1064 0.1611 0.2351 0.3287 *

[61] 0.0168 0.0293 0.0485 0.0774 0.1198 0.1795 0.2589 0.3573 *

[62] 0.0200 0.0340 0.0556 0.0879 0.1347 0.1994 0.2839 0.3869 *

[63] 0.0315 0.0450 0.0672 0.1015 0.1518 0.2210 0.3103 0.4173 *

[64] 0.0369 0.0522 0.0769 0.1148 0.1694 0.2436 0.3378 0.4482 *

[65] 0.0416 0.0593 0.0871 0.1289 0.1882 0.2675 0.3662 0.4797 *

[66] 0.0466 0.0670 0.0983 0.1442 0.2084 0.2927 0.3956 0.5115 *

[67] 0.0521 0.0755 0.1104 0.1608 0.2299 0.3190 0.4257 0.5433 *

[68] 0.0579 0.0847 0.1237 0.1787 0.2528 0.3465 0.4565 0.5751 *

[69] 0.0643 0.0947 0.1380 0.1979 0.2769 0.3750 0.4877 0.6066 *

[70] 0.0711 0.1055 0.1534 0.2183 0.3023 0.4043 0.5192 0.6376 *

[71] 0.0784 0.1172 0.1701 0.2401 0.3289 0.4345 0.5509 0.6679 *

[72] 0.0862 0.1298 0.1879 0.2632 0.3565 0.4653 0.5824 0.6974 *

[73] 0.0945 0.1432 0.2069 0.2875 0.3852 0.4965 0.6137 0.7259 *

[74] 0.1034 0.1576 0.2271 0.3130 0.

Sample size = 8

B = 0.5(0.2)1.9

AMU = 1.5 (P0 = 0.0668)

P1 0.0918 0.1450 0.2074 0.2778 0.3539 0.4332 0.5125 0.5886

*****									* B =**(0.5)**(0.7)**(0.9)**(1.1)**(1.3)**(1.5)**(1.7)**(1.9)**									
100	QMIN	50.00	0.000	0.000	0.000	0.000	0.000	0.000	*	[48]	0.0691	0.0015	0.0029	0.0053	0.0097	0.0174	0.0305	0.0516
100	SCAL	0.50	1.000	1.000	1.000	1.000	1.000	1.000	*	[49]	0.0757	0.0018	0.0034	0.0064	0.0116	0.0207	0.0359	0.0601
QMAX 1.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000									[51]	0.1228	0.0032	0.0054	0.0095	0.0167	0.0290	0.0491	0.0805	
* B =**(0.5)**(0.7)**(0.9)**(1.1)**(1.3)**(1.5)**(1.7)**(1.9)**									[52]	0.1318	0.0039	0.0066	0.0114	0.0198	0.0340	0.0571	0.0925	
[0]	0.0014	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[53]	0.1377	0.0047	0.0079	0.0135	0.0234	0.0398	0.0660	0.1058
[1]	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[54]	0.1438	0.0056	0.0094	0.0161	0.0275	0.0463	0.0761	0.1205
[2]	0.0021	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[55]	0.1501	0.0066	0.0112	0.0190	0.0322	0.0537	0.0872	0.1366
[3]	0.0023	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[56]	0.1565	0.0078	0.0132	0.0224	0.0376	0.0621	0.0996	0.1541
[4]	0.0025	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[57]	0.1632	0.0092	0.0156	0.0262	0.0437	0.0714	0.1133	0.1732
[5]	0.0027	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[58]	0.1700	0.0108	0.0182	0.0306	0.0506	0.0818	0.1284	0.1937
[6]	0.0029	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[59]	0.1770	0.0125	0.0213	0.0356	0.0584	0.0934	0.1448	0.2157
[7]	0.0032	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[60]	0.1842	0.0145	0.0248	0.0412	0.0670	0.1062	0.1626	0.2392
[8]	0.0034	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[61]	0.1915	0.0167	0.0287	0.0475	0.0767	0.1202	0.1819	0.2641
[9]	0.0037	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[62]	0.1991	0.0197	0.0334	0.0548	0.0876	0.1356	0.2027	0.2904
[10]	0.0040	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[63]	0.2068	0.0271	0.0414	0.0646	0.1004	0.1528	0.2251	0.3181
[11]	0.0043	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[64]	0.2148	0.0320	0.0482	0.0742	0.1139	0.1712	0.2488	0.3469
[12]	0.0047	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[65]	0.2229	0.0369	0.0555	0.0847	0.1286	0.1909	0.2739	0.3767
[13]	0.0050	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[66]	0.2312	0.0423	0.0635	0.0963	0.1446	0.2121	0.3004	0.4075
[14]	0.0054	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[67]	0.2397	0.0482	0.0724	0.1090	0.1620	0.2347	0.3281	0.4390
[15]	0.0058	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[68]	0.2484	0.0548	0.0823	0.1229	0.1808	0.2587	0.3569	0.4711
[16]	0.0062	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[69]	0.2573	0.0621	0.0931	0.1381	0.2010	0.2842	0.3868	0.5037
[17]	0.0067	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[70]	0.2664	0.0700	0.1050	0.1547	0.2227	0.3110	0.4177	0.5364
[18]	0.0071	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[71]	0.2757	0.0787	0.1179	0.1726	0.2459	0.3390	0.4492	0.5691
[19]	0.0076	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[72]	0.2852	0.0881	0.1320	0.1918	0.2704	0.3682	0.4814	0.6017
[20]	0.0081	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0001	*	[73]	0.2949	0.0984	0.1473	0.2125	0.2963	0.3984	0.5139	0.6337
[21]	0.0087	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0001	*	[74]	0.3048	0.1095	0.1637	0.2346	0.3236	0.4295	0.5466	0.6652
[22]	0.0092	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0001	*	[75]	0.3135	0.1366	0.1906	0.2629	0.3543	0.4622	0.5797	0.6959
[23]	0.0098	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0002	*	[76]	0.3243	0.1672	0.2202	0.2932	0.3863	0.4955	0.6124	0.7255
[24]	0.0112	0.0000	0.0000	0.0000	0.0000	0.0001	0.0001	0.0003	*	[77]	0.3364	0.1840	0.2419	0.3198	0.4168	0.5281	0.6443	0.7538
[25]	0.0148	0.0000	0.0000	0.0000	0.0000	0.0001	0.0002	0.0003	*	[78]	0.3507	0.2019	0.2650	0.3476	0.4482	0.5609	0.6757	0.7808
[26]	0.0187	0.0000	0.0000	0.0000	0.0001	0.0001	0.0002	0.0005	*	[79]	0.5150	0.2209	0.2894	0.3766	0.4804	0.5937	0.7062	0.8063
[27]	0.0209	0.0000	0.0000	0.0000	0.0001	0.0002	0.0003	0.0006	*	[80]	0.5254	0.2410	0.3150	0.4068	0.5131	0.6263	0.7356	0.8302
[28]	0.0223	0.0000	0.0000	0.0001	0.0001	0.0002	0.0004	0.0008	*	[81]	0.5359	0.2622	0.3418	0.4379	0.5462	0.6585	0.7639	0.8524
[29]	0.0239	0.0000	0.0000	0.0001	0.0001	0.0003	0.0005	0.0010	*	[82]	0.5465	0.2845	0.3699	0.4698	0.5794	0.6900	0.7908	0.8728
[30]	0.0255	0.0000	0.0000	0.0001	0.0002	0.0004	0.0007	0.0013	*	[83]	0.5572	0.3079	0.3990	0.5025	0.6127	0.7207	0.8162	0.8915
[31]	0.0271	0.0000	0.0001	0.0001	0.0002	0.0005	0.0009	0.0017	*	[84]	0.5680	0.3324	0.4292	0.5357	0.6457	0.7503	0.8400	0.9084
[32]	0.0289	0.0000	0.0001	0.0002	0.0003	0.0006	0.0012	0.0022	*	[85]	0.5789	0.3580	0.4603	0.5693	0.6783	0.7786	0.8621	0.9235
[33]	0.0307	0.0000	0.0001	0.0002	0.0004	0.0008	0.0015	0.0028	*	[86]	0.5898	0.3845	0.4922	0.6030	0.7101	0.8055	0.8823	0.9368
[34]	0.0326	0.0001	0.0001	0.0002	0.0005	0.0010	0.0019	0.0035	*	[87]	0.6009	0.4121	0.5248	0.6367	0.7411	0.8309	0.9007	0.9485
[35]	0.0346	0.0001	0.0002	0.0003	0.0006	0.0012	0.0024	0.0044	*	[88]	0.6120	0.5396	0.6120	0.6955	0.7810	0.8578	0.9181	0.9588
[36]	0.0367	0.0001	0.0002	0.0004	0.0008	0.0015	0.0030	0.0055	*	[89]	0.6231	0.5650	0.6401	0.7238	0.8064	0.8782	0.9323	0.9673
[37]	0.0388	0.0001	0.0002	0.0005	0.0010	0.0019	0.0037	0.0069	*	[90]	0.6344	0.5907	0.6683	0.7515	0.8307	0.8969	0.9449	0.9745
[38]	0.0411	0.0002	0.0003	0.0006	0.0013	0.0024	0.0046	0.0085	*	[91]	0.6457	0.6167	0.6965	0.7785	0.8537	0.9140	0.9558	0.9805
[39]	0.0434	0.0002	0.0004	0.0008	0.0016	0.0030	0.0057	0.0104	*	[92]	0.6570	0.6430	0.7244	0.8047	0.8752	0.9295	0.9653	0.9854
[40]	0.0459	0.0003	0.0005	0.0010	0.0020	0.0037	0.0070	0.0127	*	[93]	0.6684	0.6695	0.7520	0.8298	0.8952	0.9432	0.9734	0.9894
[41]	0.0484	0.0004	0.0007	0.0013	0.0024	0.0046	0.0085	0.0154	*	[94]	0.6798	0.6960	0.7790	0.8538	0.9136	0.9553	0.9801	0.9925
[42]	0.0511	0.0005	0.0009	0.0016	0.0030	0.0056	0.0104	0.0186	*	[95]	0.6913	0.7225	0.8055	0.8765	0.9303	0.9657	0.9856	0.9949
[43]	0.0538	0.0006	0.0011	0.0020	0.0037	0.0069	0.0126	0.0223	*	[96]	0.7028	0.7489	0.8312	0.8977	0.9452	0.9746	0.9900	0.9967
[44]	0.0566	0.0007	0.0013	0.0024	0.0045	0.0084	0.0151	0.0266	*	[97]	0.7143	0.7751	0.8559	0.9174	0.9584	0.9820	0.9934	0.9980
[45]	0.0596	0.0009	0.0016	0.0030	0.0055	0.0101	0.0182	0.0317	*	[98]	0.7258	0.8009	0.8795	0.9353	0.9698	0.9879	0.9959	0.9989
[46]	0.0627	0.0010	0.0020	0.0036	0.0067	0.0122	0.0217	0.0374	*	[99]	0.7374	0.8263	0.9020	0.9515	0.9794	0.9926	0.9978	0.9994
[47]	0.0659	0.0012	0.0024	0.0044	0.0081	0.0146	0.0258	0.0441	*	[100]	0.7489	0.8511	0.9230	0.9659	0.9873	0.9961	0.9990	0.9998
***** continued on the right									[101]	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	

Sample size = 8

B = 0.5(0.2)1.9

AMU = 1.5 (P0 = 0.0548)

P1 0.0809 0.1293 0.1872 0.2537 0.3273 0.4054 0.4850 0.5631

*****									* B =**(0.5)**(0.7)**(0.9)**(1.1)**(1.3)**(1.5)**(1.7)**(1.9)**									
100	QMIN	50.00	50.000	0.000	0.000	0.000	0.000	0.000	*	[48]	0.0446	0.0732	0.0013	0.0025	0.0047	0.0089	0.0162	0.0289
100	SCAL	0.50	0.500	1.000	1.000	1.000	1.000	1.000	*	[49]	0.0495	0.0794	0.0016	0.0031	0.0058	0.0107	0.0194	0.0342
QMAX 1.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000									[51]	0.0864	0.1114	0.0026	0.0047	0.0086	0.0155	0.0276	0.0475	
* B =**(0.5)**(0.7)**(0.9)**(1.1)**(1.3)**(1.5)**(1.7)**(1.9)**									[52]	0.0935	0.1197	0.0032	0.0057	0.0103	0.0186	0.0326	0.0556	
[0]	0.0006	0.0011	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[53]	0.0982	0.1264	0.0039	0.0070	0.0124	0.0221	0.0384	0.0648
[1]	0.0008	0.0013	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[54]	0.1031	0.1334						

Table with 10 columns and 100 rows. Columns include P1, QMIN, Q50, QMAX, and B values. Rows are labeled from [0] to [100]. Includes header information like 'continued on the right'.

Table with 10 columns and 100 rows. Columns include P1, QMIN, Q50, QMAX, and B values. Rows are labeled from [0] to [100]. Includes header information like 'continued on the right'.

Table with 100 columns and 100 rows of numerical data. The first row is labeled 'Sample size = 8'. The first column is labeled 'p1'. The table contains a grid of values ranging from 0.0000 to 0.9999. The bottom right corner contains the text 'continued on the right'.

Table with 100 columns and 100 rows of numerical data. The first row is labeled 'p1'. The first column is labeled 'p1'. The table contains a grid of values ranging from 0.0000 to 0.9999. The bottom right corner contains the text 'continued on the right'.

Sample size = 8 B = 0.5(0.2)1.9 AMU = 2.3 (P0 = 0.0107)

Table with 10 columns and 100 rows of numerical data. Includes header information like 'Sample size = 8', 'B = 0.5(0.2)1.9', and 'AMU = 2.3 (P0 = 0.0107)'. The data is organized into two main sections, each with a header row starting with '* B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **'. The first section contains 100 rows of data, and the second section contains 100 rows of data. The values range from 0.0000 to 1.0000.

RAMP case version of the distribution where the DISCRETE contribution is NOT removed yet

Sample size = 16 B = 0.5(0.2)1.9 AMU = 0.4 (P0 = 0.3446)

Table with 10 columns and 100 rows of numerical data. Includes header information like 'Sample size = 16', 'B = 0.5(0.2)1.9', and 'AMU = 0.4 (P0 = 0.3446)'. The data is organized into two main sections, each with a header row starting with '* B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **'. The first section contains 100 rows of data, and the second section contains 100 rows of data. The values range from 0.0000 to 1.0000.

Sample size = 16

B = 0.5(0.2)1.9

AMU = 0.5 (PC = 0.3085)

P1	0.1915	0.2707	0.3469	0.4172	0.4796	0.5328	0.5764	0.6107	*	[48]	0.1533	0.2431	0.3604	0.4974	0.6388	0.7660	0.8651	0.9315
100 QMIN	0.00	0.000	0.000	0.000	0.000	0.000	0.000	0.000	*	[49]	0.1734	0.2711	0.3946	0.5346	0.6743	0.7956	0.8865	0.9447
100 SCAL	1.00	1.000	1.000	1.000	1.000	1.000	1.000	1.000	*	[51]	0.2233	0.3325	0.4654	0.6077	0.7406	0.8477	0.9217	0.9651
QMAX	1.00	1.000	1.000	1.000	1.000	1.000	1.000	1.000	*	[52]	0.2488	0.3647	0.5013	0.6430	0.7709	0.8701	0.9358	0.9726
* B = ** (0.5)** (0.7)** (0.9)** (1.1)** (1.3)** (1.5)** (1.7)** (1.9)**									*	[53]	0.2758	0.3978	0.5372	0.6772	0.7991	0.8901	0.9479	0.9788
[0]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[54]	0.3041	0.4318	0.5729	0.7099	0.8251	0.9078	0.9581	0.9837
[1]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[55]	0.3335	0.4663	0.6080	0.7410	0.8489	0.9233	0.9666	0.9876
[2]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[56]	0.3657	0.5014	0.6423	0.7704	0.8704	0.9367	0.9736	0.9907
[3]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[57]	0.4016	0.5371	0.6757	0.7978	0.8898	0.9483	0.9794	0.9931
[4]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	*	[58]	0.4343	0.5717	0.7076	0.8231	0.9069	0.9581	0.9840	0.9949
[5]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0001	*	[59]	0.4673	0.6059	0.7380	0.8464	0.9221	0.9663	0.9878	0.9963
[6]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0001	*	[60]	0.5006	0.6393	0.7668	0.8677	0.9353	0.9732	0.9907	0.9973
[7]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0001	0.0001	*	[61]	0.5340	0.6718	0.7938	0.8868	0.9467	0.9789	0.9930	0.9981
[8]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0001	0.0001	0.0002	*	[62]	0.5681	0.7033	0.8189	0.9039	0.9565	0.9835	0.9948	0.9987
[9]	0.0000	0.0000	0.0000	0.0000	0.0001	0.0001	0.0002	0.0004	*	[63]	0.6061	0.7342	0.8422	0.9191	0.9648	0.9873	0.9962	0.9991
[10]	0.0000	0.0000	0.0000	0.0001	0.0001	0.0002	0.0004	0.0007	*	[64]	0.6387	0.7626	0.8634	0.9324	0.9718	0.9902	0.9972	0.9994
[11]	0.0000	0.0000	0.0000	0.0001	0.0002	0.0004	0.0007	0.0012	*	[65]	0.6698	0.7892	0.8826	0.9440	0.9776	0.9926	0.9980	0.9996
[12]	0.0000	0.0000	0.0001	0.0001	0.0003	0.0006	0.0011	0.0020	*	[66]	0.7000	0.8142	0.8998	0.9540	0.9824	0.9945	0.9986	0.9997
[13]	0.0000	0.0000	0.0001	0.0002	0.0005	0.0009	0.0018	0.0032	*	[67]	0.7291	0.8373	0.9153	0.9626	0.9863	0.9959	0.9990	0.9998
[14]	0.0000	0.0001	0.0002	0.0003	0.0007	0.0014	0.0027	0.0050	*	[68]	0.7571	0.8587	0.9289	0.9698	0.9894	0.9970	0.9993	0.9999
[15]	0.0000	0.0001	0.0002	0.0005	0.0011	0.0022	0.0041	0.0075	*	[69]	0.7875	0.8787	0.9409	0.9759	0.9919	0.9978	0.9995	0.9999
[16]	0.0001	0.0002	0.0003	0.0008	0.0016	0.0032	0.0061	0.0109	*	[70]	0.8128	0.8962	0.9512	0.9809	0.9939	0.9984	0.9997	0.9999
[17]	0.0001	0.0002	0.0005	0.0011	0.0023	0.0046	0.0087	0.0155	*	[71]	0.8350	0.9118	0.9601	0.9850	0.9954	0.9989	0.9998	1.0000
[18]	0.0001	0.0003	0.0007	0.0016	0.0033	0.0065	0.0122	0.0216	*	[72]	0.8557	0.9256	0.9676	0.9884	0.9966	0.9992	0.9999	1.0000
[19]	0.0002	0.0005	0.0010	0.0022	0.0046	0.0091	0.0168	0.0295	*	[73]	0.8748	0.9378	0.9740	0.9911	0.9975	0.9995	0.9999	1.0000
[20]	0.0003	0.0006	0.0014	0.0031	0.0064	0.0124	0.0227	0.0394	*	[74]	0.8924	0.9486	0.9793	0.9932	0.9982	0.9996	0.9999	1.0000
[21]	0.0004	0.0009	0.0020	0.0043	0.0087	0.0167	0.0302	0.0517	*	[75]	0.9101	0.9580	0.9837	0.9949	0.9987	0.9998	1.0000	1.0000
[22]	0.0005	0.0012	0.0027	0.0058	0.0116	0.0221	0.0395	0.0666	*	[76]	0.9253	0.9660	0.9873	0.9962	0.9991	0.9998	1.0000	1.0000
[23]	0.0007	0.0017	0.0037	0.0077	0.0154	0.0288	0.0509	0.0845	*	[77]	0.9369	0.9725	0.9902	0.9972	0.9994	0.9999	1.0000	1.0000
[24]	0.0010	0.0022	0.0049	0.0102	0.0201	0.0371	0.0645	0.1054	*	[78]	0.9472	0.9781	0.9925	0.9980	0.9996	0.9999	1.0000	1.0000
[25]	0.0013	0.0030	0.0065	0.0133	0.0258	0.0471	0.0807	0.1296	*	[79]	0.9564	0.9827	0.9944	0.9985	0.9997	1.0000	1.0000	1.0000
[26]	0.0018	0.0040	0.0085	0.0172	0.0329	0.0591	0.0995	0.1571	*	[80]	0.9644	0.9865	0.9958	0.9990	0.9998	1.0000	1.0000	1.0000
[27]	0.0024	0.0052	0.0110	0.0220	0.0414	0.0732	0.1212	0.1879	*	[81]	0.9718	0.9897	0.9969	0.9993	0.9999	1.0000	1.0000	1.0000
[28]	0.0031	0.0068	0.0141	0.0278	0.0515	0.0896	0.1458	0.2219	*	[82]	0.9786	0.9922	0.9978	0.9995	0.9999	1.0000	1.0000	1.0000
[29]	0.0040	0.0087	0.0179	0.0347	0.0634	0.1084	0.1732	0.2588	*	[83]	0.9828	0.9941	0.9984	0.9997	0.9999	1.0000	1.0000	1.0000
[30]	0.0052	0.0111	0.0224	0.0430	0.0772	0.1297	0.2036	0.2983	*	[84]	0.9864	0.9956	0.9989	0.9998	1.0000	1.0000	1.0000	1.0000
[31]	0.0066	0.0140	0.0280	0.0527	0.0931	0.1537	0.2366	0.3400	*	[85]	0.9894	0.9968	0.9992	0.9999	1.0000	1.0000	1.0000	1.0000
[32]	0.0086	0.0176	0.0346	0.0640	0.1112	0.1802	0.2722	0.3835	*	[86]	0.9919	0.9977	0.9995	0.9999	1.0000	1.0000	1.0000	1.0000
[33]	0.0109	0.0219	0.0423	0.0771	0.1315	0.2092	0.3100	0.4282	*	[87]	0.9940	0.9984	0.9996	0.9999	1.0000	1.0000	1.0000	1.0000
[34]	0.0135	0.0270	0.0514	0.0920	0.1542	0.2407	0.3497	0.4735	*	[88]	0.9961	0.9989	0.9998	1.0000	1.0000	1.0000	1.0000	1.0000
[35]	0.0167	0.0330	0.0619	0.1089	0.1792	0.2744	0.3908	0.5190	*	[89]	0.9970	0.9992	0.9998	1.0000	1.0000	1.0000	1.0000	1.0000
[36]	0.0204	0.0401	0.0739	0.1279	0.2065	0.3101	0.4331	0.5639	*	[90]	0.9978	0.9995	0.9999	1.0000	1.0000	1.0000	1.0000	1.0000
[37]	0.0249	0.0483	0.0876	0.1489	0.2359	0.3475	0.4758	0.6079	*	[91]	0.9984	0.9996	0.9999	1.0000	1.0000	1.0000	1.0000	1.0000
[38]	0.0310	0.0580	0.1032	0.1721	0.2675	0.3863	0.5187	0.6503	*	[92]	0.9989	0.9998	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[39]	0.0375	0.0690	0.1206	0.1974	0.3009	0.4261	0.5612	0.6907	*	[93]	0.9993	0.9999	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[40]	0.0449	0.0814	0.1398	0.2247	0.3360	0.4666	0.6029	0.7288	*	[94]	0.9997	0.9999	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[41]	0.0533	0.0954	0.1610	0.2539	0.3724	0.5072	0.6432	0.7642	*	[95]	0.9998	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[42]	0.0628	0.1111	0.1842	0.2850	0.4099	0.5477	0.6819	0.7969	*	[96]	0.9998	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[43]	0.0735	0.1284	0.2092	0.3177	0.4482	0.5876	0.7186	0.8266	*	[97]	0.9999	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[44]	0.0873	0.1480	0.2363	0.3519	0.4869	0.6265	0.7531	0.8533	*	[98]	0.9999	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[45]	0.1020	0.1693	0.2650	0.3872	0.5257	0.6641	0.7850	0.8770	*	[99]	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[46]	0.1176	0.1921	0.2954	0.4234	0.5641	0.7000	0.8144	0.8978	*	[100]	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[47]	0.1346	0.2168	0.3273	0.4603	0.6019	0.7341	0.8411	0.9160	*	[101]	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000

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Sample size = 16

B = 0.5(0.2)1.9

AMU = 0.6 (PC = 0.2743)

P1	0.1859	0.2656	0.3437	0.4172	0.4838	0.5417	0.5901	0.6289	*	[48]	0.0865	0.1483	0.2384	0.3570	0.4959	0.6389	0.7671	0.8664
100 QMIN	0.00	0.000	0.000	0.000	0.000													

Sample size = 16										B = 0.5(0.2)1.9										AMU = 0.7 (P0 = 0.2420)																																																																																																																																																																																																																																																																																																																																																																																																																																																																																												
P1 0.1788 0.2580 0.3373 0.4135 0.4838 0.5462 0.5994 0.6430																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																
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100 QMIN	0.00	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	[48]	0.0443	0.0821	0.1433	0.2337	0.3535	0.4940	0.6386	0.7676	[49]	0.0525	0.0961	0.1647	0.2632	0.3900	0.5340	0.6768	0.7994	[50]	0.0607	0.1199	0.2025	0.3119	0.4500	0.6014	0.7576	0.8823	0.9447	[51]	0.0750	0.1299	0.2135	0.3275	0.4656	0.6123	0.7475	0.8544	[52]	0.0876	0.1494	0.2407	0.3619	0.5041	0.6501	0.7795	0.8777	[53]	0.1017	0.1707	0.2698	0.3974	0.5426	0.6864	0.8091	0.8982	[54]	0.1172	0.1938	0.3005	0.4339	0.5807	0.7210	0.8361	0.9162	[55]	0.1343	0.2188	0.3328	0.4710	0.6181	0.7537	0.8605	0.9316	[56]	0.1542	0.2458	0.3665	0.5084	0.6545	0.7843	0.8823	0.9447	[57]	0.1780	0.2752	0.4014	0.5458	0.6896	0.8125	0.9016	0.9558	[58]	0.2010	0.3055	0.4371	0.5829	0.7231	0.8384	0.9185	0.9650	[59]	0.2255	0.3372	0.4734	0.6193	0.7547	0.8619	0.9332	0.9726	[60]	0.2516	0.3702	0.5100	0.6548	0.7844	0.8830	0.9457	0.9788	[61]	0.2793	0.4043	0.5466	0.6891	0.8120	0.9017	0.9563	0.9838	[62]	0.3091	0.4394	0.5829	0.7219	0.8373	0.9182	0.9652	0.9877	[63]	0.3451	0.4762	0.6189	0.7530	0.8604	0.9325	0.9726	0.9908	[64]	0.3779	0.5122	0.6538	0.7822	0.8812	0.9449	0.9786	0.9932	[65]	0.4109	0.5481	0.6876	0.8095	0.8998	0.9554	0.9835	0.9950	[66]	0.4446	0.5838	0.7200	0.8346	0.9162	0.9643	0.9874	0.9964	[67]	0.4790	0.6190	0.7508	0.8576	0.9306	0.9717	0.9905	0.9974	[68]	0.5138	0.6535	0.7799	0.8784	0.9430	0.9778	0.9929	0.9982	[69]	0.5549	0.6881	0.8072	0.8971	0.9537	0.9828	0.9948	0.9987	[70]	0.5913	0.7204	0.8323	0.9137	0.9627	0.9868	0.9962	0.9991	[71]	0.6249	0.7508	0.8553	0.9283	0.9703	0.9900	0.9973	0.9994	[72]	0.6579	0.7795	0.8762	0.9409	0.9766	0.9925	0.9981	0.9996	[73]	0.6901	0.8065	0.8950	0.9519	0.9818	0.9944	0.9987	0.9997	[74]	0.7213	0.8316	0.9118	0.9612	0.9860	0.9959	0.9991	0.9998	[75]	0.7554	0.8554	0.9267	0.9690	0.9893	0.9971	0.9994	0.9999	[76]	0.7868	0.8767	0.9397	0.9755	0.9920	0.9979	0.9996	0.9999	[77]	0.8119	0.8953	0.9508	0.9809	0.9940	0.9985	0.9997	1.0000	[78]	0.8355	0.9119	0.9603	0.9853	0.9956	0.9990	0.9998	1.0000	[79]	0.8576	0.9267	0.9683	0.9888	0.9968	0.9993	0.9999	1.0000	[80]	0.8779	0.9398	0.9750	0.9916	0.9977	0.9995	0.9999	1.0000	[81]	0.8979	0.9513	0.9806	0.9938	0.9984	0.9997	1.0000	1.0000	[82]	0.9183	0.9613	0.9851	0.9954	0.9989	0.9998	1.0000	1.0000	[83]	0.9313	0.9691	0.9887	0.9967	0.9993	0.9999	1.0000	1.0000	[84]	0.9430	0.9756	0.9915	0.9977	0.9995	0.9999	1.0000	1.0000	[85]	0.9534	0.9811	0.9938	0.9984	0.9997	1.0000	1.0000	1.0000	[86]	0.9625	0.9856	0.9955	0.9989	0.9998	1.0000	1.0000	1.0000	[87]	0.9704	0.9892	0.9968	0.9993	0.9999	1.0000	1.0000	1.0000	[88]	0.9797	0.9924	0.9978	0.9995	0.9999	1.0000	1.0000	1.0000	[89]	0.9839	0.9944	0.9985	0.9997	1.0000	1.0000	1.0000	1.0000	[90]	0.9875	0.9959	0.9990	0.9998	1.0000	1.0000	1.0000	1.0000	[91]	0.9905	0.9971	0.9993	0.9999	1.0000	1.0000	1.0000	1.0000	[92]	0.9930	0.9981	0.9996	0.9999	1.0000	1.0000	1.0000	1.0000	[93]	0.9951	0.9987	0.9997	1.0000	1.0000	1.0000	1.0000	1.0000	[94]	0.9976	0.9993	0.9999	1.0000	1.0000	1.0000	1.0000	1.0000	[95]	0.9982	0.9995	0.9999	1.0000	1.0000	1.0000	1.0000	1.0000	[96]	0.9987	0.9997	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	[97]	0.9991	0.9998	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	[98]	0.9994	0.9999	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	[99]	0.9997	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	[100]	0.9998	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	[101]	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000

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Sample size = 16										B = 0.5(0.2)1.9										AMU = 0.8 (P0 = 0.2119)																																																																																																																																																																																																																																																																																																																																																																																																																																																																																											
P1 0.1702 0.2483 0.3280 0.4061 0.4796 0.5462 0.6041 0.6525																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
*****										* B =**(0.5)***(0.7)***(0.9)***(1.1)***(1.3)***(1.5)***(1.7)***(1.9)***										* B =**(0.5)***(0.7)***(0.9)***(1.1)***(1.3)***(1.5)***(1.7)***(1.9)***																																																																																																																																																																																																																																																																																																																																																																																																																																																																																											
100 QMIN	0.00	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	[48]	0.0206	0.0411	0.0779	0.1385	0.2291	0.3499	0.4919	0.6377	[49]	0.0250	0.0494	0.0919	0.1602	0.2594	0.3877	0.5333	0.6774	[50]	0.0307	0.0604	0.1126	0.2099	0.3257	0.4660	0.6147	0.7507	[51]	0.0377	0.0704	0.1256	0.2299	0.3525	0.4960	0.6377	0.7836	[52]	0.0452	0.0831	0.1453	0.2379	0.3612	0.5060	0.6537	0.7836	[53]	0.0538	0.0974	0.1670	0.2678	0.3981	0.5458	0.6912	0.8139	[54]	0.0635	0.1134	0.1907	0.2996	0.4359	0.5853	0.7269	0.8415	[55]	0.0745	0.1312	0.2164	0.3330	0.4743	0.6240	0.7604	0.8662	[56]	0.0877	0.1511	0.2442	0.3678	0.5131	0.6615	0.7915	0.8882	[57]	0.1042	0.1734	0.2739	0.4039	0.5518	0.6975	0.8202	0.9074	[58]	0.1205	0.1972	0.3053	0.4409	0.5901	0.7317	0.8463	0.9242	[59]	0.1384	0.2229	0.3382	0.4785	0.6276	0.7640	0.8698	0.9385	[60]	0.1580	0.2504	0.3726	0.5164	0.6640	0.7940	0.8907	0.9507	[61]	0.1793	0.2797	0.4080	0.5542	0.6991	0.8218	0.9092	0.9608	[62]	0.2029	0.3108	0.4445	0.5917	0.7325	0.8471	0.9252	0.9692	[63]	0.2328	0.3446	0.4817	0.6285	0.7641	0.8700	0.9391	0.9761	[64]	0.2607	0.3787	0.5190	0.6643	0.7935	0.8905	0.9509	0.9817	[65]	0.2895	0.4138	0.5563	0.6988	0.8208	0.9086	0.9608	0.9861	[66]	0.3198	0.4497	0.5933	0.7318	0.8458	0.9244	0.9690	0.9896	[67]	0.3515	0.4862	0.6296	0.7630	0.8685	0.9381	0.9758	0.9923	[68]	0.3846	0.5231	0.6650	0.7922	0.8888	0.9499	0.9813	0.9944	[69]	0.4252	0.5614	0.6995	0.8193	0.9069	0.9598	0.9858	0.9959	[70]	0.4625	0.5983	0.7322	0.8442	0.9228	0.9681	0.9893	0.9971	[71]	0.4977	0.6341	0.7631	0.8669	0.9366	0.9750	0.9920	0.9980	[72]	0.5332	0.6690	0.7922	0.8873	0.9485	0.9806	0.9941	0.9986	[73]	0.5688	0.7028	0.8192	0.9055	0.9586	0.9852	0.9957	0.9990	[74]	0.6042	0.7352	0.8441	0.9215	0.9671	0.9888	0.9970	0.9994	[75]	0.6446	0.7671	0.8670	0.9355	0.9742	0.9916	0.9979	0.9996	[76]	0.6832	0.7966	0.8875	0.9476	0.9799	0.9938	0.9985	0.9997	[77]	0.7148	0.8230	0.9057	0.9579	0.9846	0.9955	0.9990	0.9998	[78]	0.7453	0.8475	0.9218	0.9665	0.9884	0.9968	0.9993	0.9999	[79]	0.7745	0.8699	0.9358	0.9737	0.9913	0.9977	0.9995	0.9999	[80]	0.8022	0.8902	0.9480	0.9797	0.9936	0.9984	0.9997	1.0000	[81]	0.8304	0.9088	0.9584	0.9845	0.9954	0.9989	0.9998	1.0000	[82]	0.8606	0.9257	0.9672	0.9883	0.9967	0.9993	0.9999	1.0000	[83]	0.8803	0.9390	0.9743	0.9913	0.9977	0.9995	0.9999	1.0000	[84]	0.8985	0.9507	0.9802	0.9936	0.9984	0.9997	1.0000	1.0000	[85]	0.9150	0.9607	0.9850	0.9954	0.9989	0.9998	1.0000	1.0000	[86]	0.9298	0.9692	0.9888	0.9968	0.9993	0.9999	1.0000	1.0000	[87]	0.9431	0.9763	0.9918	0.9978	0.9995	0.9999	1.0000	1.0000	[88]	0.9598	0.9828	0.9942	0.9985	0.9997	1.0000	1.0000	1.0000	[89]	0.9674	0.9869	0.9959	0.9990	0.9998	1.0000	1.0000	1.0000	[90]	0.9741	0.9903	0.9971	0.9994	0.9999	1.0000	1.0000	1.0000	[91]	0.9799	0.9930	0.9981	0.9996	0.9999	1.0000	1.0000	1.0000	[92]	0.9848	0.9951	0.9987	0.9998	1.0000	1.0000	1.0000	1.0000	[93]	0.9889	0.9967	0.9992	0.9999	1.0000	1.0000	1.0000	1.0000	[94]	0.9943	0.9981	0.9995	0.9999	1.0000	1.0000	1.0000	1.0000	[95]	0.9957	0.9987	0.9997	1.0000	1.0000	1.0000	1.0000	1.0000	[96]	0.9969	0.9992	0.9998	1.0000	1.0000	1.0000	1.0000	1.0000	[97]	0.9978	0.9995	0.9999	1.0000	1.0000	1.0000	1.0000	1.0000	[98]	0.9986	0.9997	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	[99]	0.9991	0.9999	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	[100]	0.9995	0.9999	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	[101]	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000

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Sample size = 16

B = 0.5(0.2)1.9

AMU = 0.9 (PC = 0.1841)

P1 0.1605 0.2367 0.3159 0.3952 0.4714 0.5417 0.6041 0.6573

Table with 10 columns: 100 QMIN, 100 SCAL, QMAX, and 10 columns for B values from 0.5 to 1.9. Rows 0-47 show values increasing from 0.0000 to 1.0000. Row 48 shows values around 0.0087. Row 49 shows values around 0.0108. Row 50 shows values around 0.0172. Row 51 shows values around 0.0212. Row 52 shows values around 0.0259. Row 53 shows values around 0.0314. Row 54 shows values around 0.0377. Row 55 shows values around 0.0455. Row 56 shows values around 0.0557. Row 57 shows values around 0.0661. Row 58 shows values around 0.0779. Row 59 shows values around 0.0911. Row 60 shows values around 0.1058. Row 61 shows values around 0.1226. Row 62 shows values around 0.1448. Row 63 shows values around 0.1661. Row 64 shows values around 0.1888. Row 65 shows values around 0.2134. Row 66 shows values around 0.2397. Row 67 shows values around 0.2679. Row 68 shows values around 0.3041. Row 69 shows values around 0.3384. Row 70 shows values around 0.3717. Row 71 shows values around 0.4062. Row 72 shows values around 0.4417. Row 73 shows values around 0.4780. Row 74 shows values around 0.5211. Row 75 shows values around 0.5640. Row 76 shows values around 0.5999. Row 77 shows values around 0.6355. Row 78 shows values around 0.6704. Row 79 shows values around 0.7046. Row 80 shows values around 0.7406. Row 81 shows values around 0.7813. Row 82 shows values around 0.8082. Row 83 shows values around 0.8337. Row 84 shows values around 0.8575. Row 85 shows values around 0.8795. Row 86 shows values around 0.8997. Row 87 shows values around 0.9270. Row 88 shows values around 0.9396. Row 89 shows values around 0.9509. Row 90 shows values around 0.9609. Row 91 shows values around 0.9696. Row 92 shows values around 0.9771. Row 93 shows values around 0.9879. Row 94 shows values around 0.9907. Row 95 shows values around 0.9931. Row 96 shows values around 0.9950. Row 97 shows values around 0.9966. Row 98 shows values around 0.9979. Row 99 shows values around 0.9988. Row 100 shows values around 1.0000.

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Sample size = 16

B = 0.5(0.2)1.9

AMU = 0.9 (PC = 0.1841)

P1 0.1499 0.2234 0.3015 0.3812 0.4593 0.5328 0.5994 0.6573

Table with 10 columns: 100 QMIN, 100 SCAL, QMAX, and 10 columns for B values from 0.5 to 1.9. Rows 0-47 show values increasing from 0.0000 to 1.0000. Row 48 shows values around 0.0033. Row 49 shows values around 0.0042. Row 50 shows values around 0.0071. Row 51 shows values around 0.0090. Row 52 shows values around 0.0113. Row 53 shows values around 0.0141. Row 54 shows values around 0.0173. Row 55 shows values around 0.0215. Row 56 shows values around 0.0272. Row 57 shows values around 0.0332. Row 58 shows values around 0.0401. Row 59 shows values around 0.0481. Row 60 shows values around 0.0572. Row 61 shows values around 0.0680. Row 62 shows values around 0.0828. Row 63 shows values around 0.0828. Row 64 shows values around 0.0976. Row 65 shows values around 0.1137. Row 66 shows values around 0.1315. Row 67 shows values around 0.1512. Row 68 shows values around 0.1729. Row 69 shows values around 0.2021. Row 70 shows values around 0.2307. Row 71 shows values around 0.2592. Row 72 shows values around 0.2894. Row 73 shows values around 0.3214. Row 74 shows values around 0.3550. Row 75 shows values around 0.3968. Row 76 shows values around 0.4400. Row 77 shows values around 0.4770. Row 78 shows values around 0.5146. Row 79 shows values around 0.5526. Row 80 shows values around 0.5907. Row 81 shows values around 0.6325. Row 82 shows values around 0.6822. Row 83 shows values around 0.7158. Row 84 shows values around 0.7482. Row 85 shows values around 0.7794. Row 86 shows values around 0.8091. Row 87 shows values around 0.8370. Row 88 shows values around 0.8777. Row 89 shows values around 0.8967. Row 90 shows values around 0.9141. Row 91 shows values around 0.9299. Row 92 shows values around 0.9441. Row 93 shows values around 0.9566. Row 94 shows values around 0.9764. Row 95 shows values around 0.9815. Row 96 shows values around 0.9858. Row 97 shows values around 0.9896. Row 98 shows values around 0.9927. Row 99 shows values around 0.9952. Row 100 shows values around 0.9973.

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Sample size = 16
 P1 0.1151 0.1775 0.2478 0.3239 0.4032 0.4825 0.5586 0.6289 B = 0.5 (0.2)1.9 AMU = 1.3 (P0 = 0.0968)

 100 QMIN50.00 50.000 0.000 0.000 0.000 0.000 0.000 0.000 * [48] 0.0963 0.1617 0.0007 0.0020 0.0051 0.0126 0.0290 0.0615
 100 SCAL 0.50 0.500 1.000 1.000 1.000 1.000 1.000 1.000 * [49] 0.1052 0.1747 0.0010 0.0027 0.0068 0.0163 0.0367 0.0757
 QMAX 1.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000 * [51] 0.1318 0.2054 0.0019 0.0047 0.0115 0.0265 0.0568 0.1117
 * B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **
 [0] 0.0002 0.0005 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [52] 0.1433 0.2207 0.0025 0.0062 0.0148 0.0334 0.0698 0.1336
 [1] 0.0002 0.0006 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [53] 0.1546 0.2364 0.0033 0.0081 0.0189 0.0417 0.0850 0.1585
 [2] 0.0003 0.0007 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [54] 0.1665 0.2528 0.0044 0.0105 0.0240 0.0516 0.1025 0.1862
 [3] 0.0003 0.0008 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [55] 0.1790 0.2699 0.0057 0.0135 0.0301 0.0632 0.1226 0.2168
 [4] 0.0004 0.0010 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [56] 0.1921 0.2876 0.0075 0.0172 0.0376 0.0770 0.1453 0.2502
 [5] 0.0005 0.0011 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [57] 0.2058 0.3059 0.0097 0.0217 0.0465 0.0928 0.1708 0.2862
 [6] 0.0005 0.0013 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [58] 0.2201 0.3248 0.0124 0.0273 0.0570 0.1111 0.1991 0.3247
 [7] 0.0006 0.0015 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [59] 0.2349 0.3443 0.0158 0.0340 0.0694 0.1319 0.2302 0.3652
 [8] 0.0007 0.0018 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [60] 0.2504 0.3644 0.0200 0.0421 0.0839 0.1553 0.2639 0.4074
 [9] 0.0008 0.0021 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [61] 0.2665 0.3850 0.0252 0.0517 0.1005 0.1814 0.3001 0.4509
 [10] 0.0010 0.0024 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [62] 0.2828 0.4077 0.0314 0.0631 0.1196 0.2102 0.3385 0.4952
 [11] 0.0011 0.0027 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [63] 0.3184 0.4335 0.0389 0.0764 0.1412 0.2417 0.3789 0.5397
 [12] 0.0013 0.0031 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [64] 0.3418 0.4569 0.0479 0.0918 0.1654 0.2758 0.4208 0.5839
 [13] 0.0015 0.0036 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [65] 0.3606 0.4788 0.0585 0.1094 0.1922 0.3123 0.4639 0.6272
 [14] 0.0018 0.0042 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [66] 0.3797 0.5009 0.0710 0.1295 0.2218 0.3509 0.5076 0.6693
 [15] 0.0021 0.0048 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [67] 0.3993 0.5232 0.0854 0.1522 0.2540 0.3914 0.5515 0.7095
 [16] 0.0024 0.0055 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [68] 0.4193 0.5456 0.1021 0.1776 0.2888 0.4333 0.5950 0.7474
 [17] 0.0028 0.0063 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [69] 0.4397 0.5682 0.1214 0.2057 0.3259 0.4763 0.6377 0.7828
 [18] 0.0032 0.0071 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [70] 0.4604 0.5907 0.1432 0.2365 0.3650 0.5198 0.6789 0.8154
 [19] 0.0036 0.0081 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [71] 0.4814 0.6132 0.1675 0.2699 0.4060 0.5635 0.7184 0.8449
 [20] 0.0041 0.0092 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [72] 0.5028 0.6356 0.1946 0.3058 0.4483 0.6067 0.7556 0.8713
 [21] 0.0047 0.0104 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [73] 0.5243 0.6579 0.2244 0.3440 0.4916 0.6490 0.7903 0.8946
 [22] 0.0053 0.0117 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [74] 0.5461 0.6799 0.2569 0.3843 0.5354 0.6899 0.8221 0.9149
 [23] 0.0060 0.0132 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [75] 0.5683 0.7073 0.2926 0.4263 0.5792 0.7288 0.8510 0.9322
 [24] 0.0068 0.0149 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [76] 0.6277 0.7335 0.3307 0.4696 0.6224 0.7656 0.8768 0.9468
 [25] 0.0080 0.0169 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [77] 0.6471 0.7525 0.3706 0.5136 0.6646 0.7997 0.8995 0.9589
 [26] 0.0093 0.0191 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 * [78] 0.6664 0.7709 0.4124 0.5579 0.7052 0.8310 0.9192 0.9687
 [27] 0.0106 0.0215 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 * [79] 0.6856 0.7889 0.4557 0.6021 0.7439 0.8593 0.9360 0.9766
 [28] 0.0119 0.0241 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 * [80] 0.7046 0.8063 0.5002 0.6455 0.7801 0.8844 0.9501 0.9829
 [29] 0.0135 0.0269 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 * [81] 0.7235 0.8232 0.5457 0.6878 0.8137 0.9065 0.9618 0.9877
 [30] 0.0151 0.0300 0.0000 0.0000 0.0000 0.0000 0.0001 0.0002 * [82] 0.7421 0.8394 0.5921 0.7284 0.8443 0.9256 0.9712 0.9913
 [31] 0.0169 0.0334 0.0000 0.0000 0.0000 0.0000 0.0001 0.0003 * [83] 0.7604 0.8550 0.6362 0.7664 0.8717 0.9417 0.9788 0.9940
 [32] 0.0189 0.0371 0.0000 0.0000 0.0000 0.0001 0.0002 0.0005 * [84] 0.7784 0.8698 0.6794 0.8018 0.8960 0.9552 0.9846 0.9959
 [33] 0.0211 0.0412 0.0000 0.0000 0.0000 0.0001 0.0003 0.0007 * [85] 0.7961 0.8840 0.7211 0.8344 0.9171 0.9662 0.9891 0.9973
 [34] 0.0234 0.0456 0.0000 0.0000 0.0000 0.0001 0.0004 0.0011 * [86] 0.8134 0.8974 0.7607 0.8638 0.9351 0.9750 0.9925 0.9983
 [35] 0.0260 0.0504 0.0000 0.0000 0.0001 0.0002 0.0006 0.0016 * [87] 0.8303 0.9100 0.7979 0.8900 0.9502 0.9820 0.9949 0.9989
 [36] 0.0289 0.0556 0.0000 0.0000 0.0001 0.0003 0.0008 0.0022 * [88] 0.8870 0.9328 0.8344 0.9131 0.9626 0.9873 0.9967 0.9994
 [37] 0.0326 0.0615 0.0000 0.0000 0.0001 0.0004 0.0012 0.0031 * [89] 0.8966 0.9405 0.8640 0.9323 0.9726 0.9913 0.9979 0.9996
 [38] 0.0375 0.0682 0.0000 0.0001 0.0002 0.0006 0.0016 0.0043 * [90] 0.9059 0.9477 0.8906 0.9484 0.9804 0.9942 0.9987 0.9998
 [39] 0.0422 0.0753 0.0000 0.0001 0.0003 0.0008 0.0023 0.0059 * [91] 0.9148 0.9545 0.9141 0.9618 0.9864 0.9963 0.9992 0.9999
 [40] 0.0467 0.0826 0.0000 0.0001 0.0004 0.0012 0.0032 0.0080 * [92] 0.9233 0.9608 0.9343 0.9725 0.9909 0.9977 0.9996 0.9999
 [41] 0.0515 0.0904 0.0001 0.0002 0.0006 0.0016 0.0043 0.0107 * [93] 0.9315 0.9665 0.9513 0.9809 0.9941 0.9986 0.9998 1.0000
 [42] 0.0567 0.0988 0.0001 0.0003 0.0008 0.0022 0.0059 0.0142 * [94] 0.9393 0.9718 0.9674 0.9876 0.9964 0.9992 0.9999 1.0000
 [43] 0.0622 0.1077 0.0001 0.0004 0.0011 0.0031 0.0078 0.0186 * [95] 0.9467 0.9767 0.9766 0.9918 0.9978 0.9996 0.9999 1.0000
 [44] 0.0682 0.1173 0.0002 0.0006 0.0016 0.0041 0.0104 0.0241 * [96] 0.9537 0.9810 0.9839 0.9949 0.9988 0.9998 1.0000 1.0000
 [45] 0.0745 0.1274 0.0003 0.0008 0.0021 0.0056 0.0136 0.0310 * [97] 0.9604 0.9849 0.9896 0.9971 0.9994 0.9999 1.0000 1.0000
 [46] 0.0813 0.1382 0.0004 0.0011 0.0029 0.0074 0.0177 0.0393 * [98] 0.9666 0.9884 0.9939 0.9985 0.9997 1.0000 1.0000 1.0000
 [47] 0.0886 0.1496 0.0005 0.0015 0.0039 0.0097 0.0228 0.0494 * [99] 0.9724 0.9914 0.9969 0.9994 0.9999 1.0000 1.0000 1.0000
 ***** continued on the right *****
 [100] 0.9778 0.9941 0.9988 0.9998 1.0000 1.0000 1.0000 1.0000
 [101] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000

Sample size = 16
 P1 0.1033 0.1612 0.2278 0.3013 0.3794 0.4591 0.5372 0.6107 B = 0.5 (0.2)1.9 AMU = 1.4 (P0 = 0.0808)

 100 QMIN50.00 50.000 50.000 50.000 0.000 0.000 0.000 0.000 * [48] 0.0541 0.0966 0.1643 0.2649 0.0017 0.0046 0.0116 0.0274
 100 SCAL 0.50 0.500 0.500 0.500 1.000 1.000 1.000 1.000 * [49] 0.0599 0.1059 0.1779 0.2832 0.0023 0.0061 0.0152 0.0349
 QMAX 1.00 1.000 1.000 1.000 1.000 1.000 1.000 1.000 * [51] 0.0784 0.1286 0.2081 0.3217 0.0042 0.0107 0.0253 0.0553
 * B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **
 [0] 0.0001 0.0001 0.0004 0.0012 0.0000 0.0000 0.0000 0.0000 * [52] 0.0865 0.1402 0.2241 0.3419 0.0056 0.0139 0.0321 0.0685
 [1] 0.0001 0.0002 0.0005 0.0014 0.0000 0.0000 0.0000 0.0000 * [53] 0.0946 0.1524 0.2407 0.3626 0.0074 0.0179 0.0405 0.0840
 [2] 0.0001 0.0002 0.0006 0.0016 0.0000 0.0000 0.0000 0.0000 * [54] 0.1032 0.1652 0.2581 0.3838 0.0097 0.0229 0.0505 0.1022
 [3] 0.0001 0.0002 0.0007 0.0018 0.0000 0.0000 0.0000 0.0000 * [55] 0.1124 0.1788 0.2761 0.4055 0.0126 0.0291 0.0625 0.1230
 [4] 0.0001 0.0003 0.0008 0.0021 0.0000 0.0000 0.0000 0.0000 * [56] 0.1221 0.1931 0.2950 0.4277 0.0162 0.0366 0.0766 0.1467
 [5] 0.0001 0.0004 0.0009 0.0025 0.0000 0.0000 0.0000 0.0000 * [57] 0.1325 0.2081 0.3145 0.4502 0.0207 0.0456 0.0931 0.1734
 [6] 0.0002 0.0004 0.0011 0.0029 0.0000 0.0000 0.0000 0.0000 * [58] 0.1434 0.2239 0.3346 0.4730 0.0263 0.0564 0.1121 0.2031
 [7] 0.0002 0.0005 0.0013 0.0034 0.0000 0.0000 0.0000 0.0000 * [59] 0.1549 0.2405 0.3554 0.4960 0.0331 0.0692 0.1338 0.2358
 [8] 0.0002 0.0006 0.0015 0.0039 0.0000 0.0000 0.0000 0.0000 * [60] 0.1670 0.2578 0.3767 0.5192 0.0413 0.0842 0.1584 0.2712
 [9] 0.0003 0.0007 0.0017 0.0045 0.0000 0.0000 0.0000 0.0000 * [61] 0.1798 0.2758 0.3986 0.5426 0.0511 0.1015 0.1858 0.3093
 [10] 0.0003 0.0008 0.0020 0.0052 0.0000 0.0000 0.0000 0.0000 * [62] 0.1978 0.2963 0.4215 0.5660 0.0627 0.1215 0.2162 0.3497
 [11] 0.0004 0.0009 0.0024 0.0059 0.0000 0.0000 0.0000 0.0000 * [63] 0.2240 0.3203 0.4456 0.5895 0.0764 0.1441 0.2494 0.3921
 [12] 0.0004 0.0011 0.0027 0.0068 0.0000 0.0000 0.0000 0.0000 * [64] 0.2445 0.3423 0.4692 0.6127 0.0924 0.1695 0.2853 0.4361
 [13] 0.0005 0.0013 0.0032 0.0078 0.0000 0.0000 0.0000 0.0000 * [65] 0.2609 0.3631 0.4925 0.6356 0.1108 0.1978 0.3238 0.4810
 [14] 0.0006 0.0015 0.0037 0.0089 0.0000 0.0000 0.0000 0.0000 * [66] 0.2779 0.3844 0.5160 0.6581 0.1319 0.2290 0.3644 0.5265
 [15] 0.0007 0.0017 0.0042 0.0101 0.0000 0.0000 0.0000 0.0000 * [67] 0.2956 0.4063 0.5396 0.6803 0.1556 0.2630 0.4069 0.5718
 [16] 0.0008 0.0020 0.0049 0.0115 0.0000 0.0000 0.0000 0.0000 * [68] 0.3138 0.4287 0.5634 0.7020 0.1823 0.2997 0.4508 0.6165
 [17] 0.0010 0.0023 0.0056 0.0131 0.0000 0.0000 0.0000 0.0000 * [69] 0.3326 0.4515 0.5871 0.7233 0.2118 0.3387 0.4955 0.6600
 [18] 0.0011 0.0027 0.0064 0.0148 0.0000 0.0000 0.0000 0.0000 * [70] 0.3520 0.4748 0.6108 0.7440 0.2443 0.3799 0.5407 0.7017
 [19] 0.0013 0.0031 0.0073 0.0168 0.0000 0.0000 0.0000 0.0000 * [71] 0.3719 0.4983 0.6343 0.7640 0.2795 0.4228 0.5857 0.7412
 [20] 0.0015 0.0036 0.0083 0.0190 0.0000 0.0000 0.0000 0.0000 * [72] 0.3924 0.5221 0.6576 0.7834 0.3173 0.4670 0.6299 0.7781
 [21] 0.0018 0.0041 0.0095 0.0214 0.0000 0.0000 0.0000 0.0000 * [73] 0.4134 0.5462 0.6805 0.8020 0.3575 0.5120 0.6728 0.8121
 [22] 0.0020 0.0047 0.0108 0.0241 0.0000 0.0000 0.0000 0.0000 * [74] 0.4349 0.5704 0.7031 0.8198 0.3997 0.5573 0.7139 0.8429
 [23] 0.0023 0.0054 0.0123 0.0270 0.0000 0.0000 0.0000 0.0000 * [75] 0.4789 0.6022 0.7271 0.8371 0.4436 0.6022 0.7528 0.8704
 [24] 0.0027 0.0062 0.0139 0.0303 0.0000 0.0000 0.0000 0.0000 * [76] 0.5229 0.6332 0.7501 0.8534 0.4886 0.6463 0.7889 0.8946
 [25] 0.0032 0.0071 0.0158 0.0339 0.0000 0.0000 0.0000 0.0000 * [77] 0.5439 0.6555 0.7700 0.8682 0.5342 0.6889 0.8221 0.9155
 [26] 0.0038 0.0082 0.0178 0.0379 0.0000 0.0000 0.0000 0.0000 * [78] 0.5650 0.6775 0.7893 0.8822 0.5799 0.7296 0.8521 0.9334
 [27] 0.0044 0.0094 0.0201 0.0422 0.0000 0.0000 0.0000 0.0000 * [79] 0.5862 0.6994 0.8079 0.8953 0.6251 0.7679 0.8789 0.9483
 [28] 0.0050 0.0106 0.0227 0.0470 0.0000 0.0000 0.0000 0.0000 * [80] 0.6075 0.7208 0.8258 0.9075 0.6692 0.8034 0.9023 0.9606
 [29] 0.0057 0.0121 0.0255 0.0521 0.0000 0.0000 0.0000 0.0000 * [81] 0.6288 0.7420 0.8428 0.9188 0.7117 0.8358 0.9224 0.9705
 [30] 0.0065 0.0137 0.0286 0.0578 0.0000 0.0000 0.0000 0.0001 * [82] 0.6502 0.7626 0.8591 0.9292 0.7520 0.8649 0.9395 0.9784
 [31] 0.0074 0.0155 0.0320 0.0639 0.0000 0.0000 0.0000 0.0001 * [83] 0.6715 0.7828 0.8744 0.9387 0.7895 0.8907 0.9537 0.9845
 [32] 0.0084 0.0175 0.0357 0.0705 0.0000 0.0000 0.0000 0.0001 * [84] 0.6927 0.8024 0.8889 0.9474 0.8241 0.9130 0.9652 0.9891
 [33] 0.0095 0.0197 0.0398 0.0777 0.0000 0.0000 0.0001 0.0002 * [85] 0.7138 0.8213 0.9024 0.9552 0.8553 0.9321 0.9744 0.9925
 [34] 0.0107 0.0221 0.0443 0.0855 0.0000 0.0000 0.0001 0.0003 * [86] 0.7347 0.8396 0.9150 0.9622 0.8831 0.9481 0.9816 0.9950
 [35] 0.0120 0.0248 0.0493 0.0938 0.0000 0.0000 0.0001 0.0004 * [87] 0.7554 0.8571 0.9267 0.9684 0.9073 0.9611 0.9871 0.9968
 [36] 0.0135 0.0278 0.0546 0.1028 0.0000 0.0001 0.0002 0.0006 * [88] 0.8333 0.8917 0.9415 0.9745 0.9281 0.9716 0.9912 0.9980
 [37] 0.0156 0.0312 0.0605 0.1124 0.0000 0.0001 0.0003 0.0009 * [89] 0.8460 0.9030 0.9494 0.9789 0.9454 0.9798 0.9942 0.9988
 [38] 0.0183 0.0352 0.0670 0.1227 0.0000 0.0001 0.0005 0.0013 * [90] 0.8584 0.9138 0.9567 0.9827 0.9596 0.9860 0.9963 0.9993
 [39] 0.0210 0.0395 0.0740 0.1337 0.0001 0.0002 0.0007 0.0019 * [91] 0.8705 0.9239 0.9633 0.9860 0.9710

Sample size = 16 B = 0.5(0.2)1.9 AMU = 1.7 (PO = 0.0446)

Table with columns for sample size, P1, and various B values. Includes a header row for B values and a footer row indicating continuation on the right.

Table with columns for sample size, P1, and various B values. Includes a header row for B values and a footer row indicating continuation on the right.

Table with columns for sample size (100 QMIN, 50.000, 50.000, 50.000, 50.000, 50.000, 50.000, 50.000, 49.000), QMAX, and B values. Includes a list of 100 rows with values for B from 0.0001 to 1.0000. Ends with 'continued on the right'.

Table with columns for sample size (100 QMIN, 75.000, 50.000, 50.000, 50.000, 50.000, 50.000, 50.000, 50.000), QMAX, and B values. Includes a list of 100 rows with values for B from 0.0006 to 1.0000. Ends with 'continued on the right'.

Table with columns for P1, QMIN, QSCALE, QMAX, B, and a grid of values for different sample sizes and B values. Includes a header row: P1 0.0369 0.0629 0.0972 0.1408 0.1940 0.2564 0.3267 0.4029. Includes a footer row: continued on the right.

Table with columns for P1, QMIN, QSCALE, QMAX, B, and a grid of values for different sample sizes and B values. Includes a header row: P1 0.0307 0.0529 0.0829 0.1218 0.1704 0.2281 0.2944 0.3697. Includes a footer row: continued on the right.

"RAMP" case version of the distribution where the DISCRETE contribution is NOT removed yet

Table with 10 columns: Sample size = 32, P1, and 8 columns of values (0.1952, 0.2733, 0.3469, 0.4135, 0.4714, 0.5198, 0.5586, 0.5886). Includes parameters B = 0.5(0.2)1.9 and AMU = 0.4 (PO = 0.3446). Rows include QMIN, SCAL, QMAX, and a grid of values for B from 0.0 to 1.0.

Table with 10 columns: Sample size = 32, P1, and 8 columns of values (0.1915, 0.2707, 0.3469, 0.4172, 0.4796, 0.5328, 0.5764, 0.6107). Includes parameters B = 0.5(0.2)1.9 and AMU = 0.5 (PO = 0.3085). Rows include QMIN, SCAL, QMAX, and a grid of values for B from 0.0 to 1.0.

Sample size = 32

B = 0.5(0.2)1.9

AMU = 0.6 (P0 = 0.2743)

P1 0.1859 0.2656 0.3437 0.4172 0.4838 0.5417 0.5901 0.6289

Table with 10 columns and 48 rows of numerical data. Includes header 'QMIN 37.00 34.000 30.000 27.000 23.000 20.000 17.000 14.000' and 'QMAX 0.87 0.840 0.800 0.770 0.730 0.700 0.670 0.640'. Rows are labeled with indices from 0 to 47.

Table with 10 columns and 101 rows of numerical data. Header: '* B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **'. Rows are labeled with indices from 48 to 101.

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Sample size = 32

B = 0.5(0.2)1.9

AMU = 0.7 (P0 = 0.2420)

P1 0.1788 0.2580 0.3370 0.4100 0.4780 0.5360 0.5840 0.6220

Table with 10 columns and 48 rows of numerical data. Includes header 'QMIN 41.00 37.000 34.000 30.000 27.000 23.000 20.000 17.000' and 'QMAX 0.91 0.870 0.840 0.800 0.770 0.730 0.700 0.670'. Rows are labeled with indices from 0 to 47.

Table with 10 columns and 101 rows of numerical data. Header: '* B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **'. Rows are labeled with indices from 48 to 101.

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Sample size = 32

B = 0.5(0.2)1.9

AMU = 0.8 (P0 = 0.2119)

P1 0.1702 0.2483 0.3280 0.4061 0.4796 0.5462 0.6041 0.6525

Table with 8 columns and 47 rows of numerical data. Includes header '100 QMIN 4.00 40.000 37.000 34.000 30.000 27.000 23.000 20.000' and '100 SCAL 0.50 0.500 0.500 0.500 0.500 0.500 0.500 0.500'. Ends with '***** continued on the right'.

Table with 8 columns and 47 rows of numerical data. Starts with '* B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **'. Ends with '101] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000'.

Sample size = 32

B = 0.5(0.2)1.9

AMU = 0.9 (P0 = 0.1841)

P1 0.1005 0.2507 0.3157 0.3755 0.4353 0.4951 0.5549 0.6147

Table with 8 columns and 47 rows of numerical data. Includes header '100 QMIN 4.00 43.000 40.000 37.000 33.000 30.000 27.000 23.000' and '100 SCAL 0.50 0.500 0.500 0.500 0.500 0.500 0.500 0.500'. Ends with '***** continued on the right'.

Table with 8 columns and 47 rows of numerical data. Starts with '* B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **'. Ends with '101] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000'.

Sample size = 32

B = 0.5(0.2)1.9

AMU = 1.0 (P0 = 0.1587)

P1 0.1499 0.2234 0.3015 0.3812 0.4593 0.5328 0.5994 0.6573

Table with columns for sample index and values from 0.0000 to 0.2471, including labels like QMIN, SCAL, QMAX, and B.

Table with columns for sample index and values from 0.2693 to 1.0000, including labels like B and various numerical values.

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Sample size = 32

B = 0.5(0.2)1.9

AMU = 1.1 (P0 = 0.1357)

P1 0.1499 0.2234 0.3015 0.3812 0.4593 0.5328 0.5994 0.6573

Table with columns for sample index and values from 0.0000 to 0.2471, including labels like QMIN, SCAL, QMAX, and B.

Table with columns for sample index and values from 0.1796 to 1.0000, including labels like B and various numerical values.

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Sample size = 32

B = 0.5 (0.2) 1.9

AMU = 1.2 (P0 = 0.1151)

P1 0.1269 0.1935 0.2670 0.3451 0.4248 0.5028 0.5764 0.6430

Table with 8 columns and 47 rows of data. Header row: ***** continued on the right

Table with 8 columns and 47 rows of data. Header row: * B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **

Sample size = 32

B = 0.5 (0.2) 1.9

AMU = 1.3 (P0 = 0.0968)

P1 0.1269 0.1935 0.2670 0.3451 0.4248 0.5028 0.5764 0.6430

Table with 8 columns and 47 rows of data. Header row: ***** continued on the right

Table with 8 columns and 47 rows of data. Header row: * B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **

Sample size = 32 B = 0.5(0.2)1.9 AMU = 1.4 (PO = 0.0808)

Table with 10 columns: P1, QMIN, SCAL, QMAX, and 8 columns of B values. Rows range from 100 down to 477. Includes header information and a continuation note at the bottom.

Sample size = 32 B = 0.5(0.2)1.9 AMU = 1.5 (PO = 0.0668)

Table with 10 columns: P1, QMIN, SCAL, QMAX, and 8 columns of B values. Rows range from 100 down to 477. Includes header information and a continuation note at the bottom.

Sample size = 32

B = 0.5 (0.2) 1.9

AMU = 1.6 (P0 = 0.0548)

P1 0.0809 0.1293 0.1872 0.2537 0.3273 0.4054 0.4850 0.5631

Table with 10 columns and 47 rows of numerical data. Includes header row with B values and a footer row with 'continued on the right'.

Sample size = 32

B = 0.5 (0.2) 1.9

AMU = 1.7 (P0 = 0.0446)

P1 0.0809 0.1293 0.1872 0.2537 0.3273 0.4054 0.4850 0.5631

Table with 10 columns and 47 rows of numerical data. Includes header row with B values and a footer row with 'continued on the right'.

Sample size = 32

B = 0.5(0.2)1.9

AMU = 2.0 (PO = 0.0228)

P1 0.0441 0.0741 0.1129 0.1613 0.2192 0.2858 0.3593 0.4374

Table with 9 columns: 100 QMIN, 75.00, 75.000, 75.000, 75.000, 74.500, 50.000, 50.000, 50.000. Includes rows for QMAX and B values from 0 to 47.

Table with 9 columns: B values from 0.0104 to 1.0000. Includes rows for B values from 0.5 to 1.9.

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Sample size = 32

B = 0.5(0.2)1.9

AMU = 2.1 (PO = 0.0179)

Table with 9 columns: 100 QMIN, 75.00, 75.000, 75.000, 75.000, 74.500, 50.000, 50.000, 50.000. Includes rows for QMAX and B values from 0 to 47.

Table with 9 columns: B values from 0.0041 to 1.0000. Includes rows for B values from 0.5 to 1.9.

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"RAMP" case version of the distribution where the DISCRETE contribution is NOT removed yet

Table with 10 columns: Sample size = 64, P1, and values for 100 QMIN, 100 SCAL, QMAX, and B. Rows represent discrete values from 0 to 100. Includes parameters AMU = 0.4 (PO = 0.3446) and B = 0.5(0.2)1.9.

Table with 10 columns: Sample size = 64, P1, and values for 100 QMIN, 100 SCAL, QMAX, and B. Rows represent discrete values from 0 to 100. Includes parameters AMU = 0.5 (PO = 0.3085) and B = 0.5(0.2)1.9.

Sample size = 64

B = 0.5 (0.2) 1.9

AMU = 0.6 (PO = 0.2743)

P1 0.1859 0.2656 0.3437 0.4172 0.4838 0.5417 0.5901 0.6289
100 QMIN 37.00 34.000 30.000 27.000 23.000 20.000 17.000 14.000
100 SCAL 0.50 0.500 0.500 0.500 0.500 0.500 0.500 0.500
QMAX 0.87 0.840 0.800 0.770 0.730 0.700 0.670 0.640

Table with 8 columns of data for B values from 0.5 to 1.9. Rows are indexed from 0 to 473. Includes a 'continued on the right' note at the bottom.

Table with 8 columns of data for B values from 0.5 to 1.9. Rows are indexed from 48 to 511. Includes a 'continued on the right' note at the bottom.

Sample size = 64

B = 0.5 (0.2) 1.9

AMU = 0.7 (PO = 0.2420)

Table with 8 columns of data for B values from 0.5 to 1.9. Rows are indexed from 0 to 473. Includes a 'continued on the right' note at the bottom.

Table with 8 columns of data for B values from 0.5 to 1.9. Rows are indexed from 48 to 511. Includes a 'continued on the right' note at the bottom.

Table with columns for P1, QMIN, SCAL, QMAX, and B values. Rows range from 0 to 101. Includes header information like 'Sample size = 64' and 'B = 0.5(0.2)1.9'.

Table with columns for P1, QMIN, SCAL, QMAX, and B values. Rows range from 0 to 101. Includes header information like 'Sample size = 64' and 'B = 0.5(0.2)1.9'.

Sample size = 64

B = 0.5(0.2)1.9

AMU = 1.0 (PC = 0.1587)

P1 0.1499 0.2234 0.3015 0.3812 0.4593 0.5328 0.5994 0.6573

Table with 10 columns and 48 rows of numerical data. Headers include QMIN, SCAL, QMAX, and B values. The data shows a progression from 0.0000 to 1.0000 across the rows.

Table with 10 columns and 48 rows of numerical data. Headers include B values and various numerical entries. The data shows a progression from 0.1985 to 1.0000 across the rows.

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Sample size = 64

B = 0.5(0.2)1.9

AMU = 1.0 (PC = 0.1587)

P1 0.1386 0.2089 0.2851 0.3643 0.4436 0.5198 0.5901 0.6525

Table with 10 columns and 48 rows of numerical data. Headers include QMIN, SCAL, QMAX, and B values. The data shows a progression from 0.0000 to 1.0000 across the rows.

Table with 10 columns and 48 rows of numerical data. Headers include B values and various numerical entries. The data shows a progression from 0.1018 to 1.0000 across the rows.

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Sample size = 64

E = 0.5(0.2)1.9

AMU = 1.2 (PO = 0.1151)

P1 0.1269 0.1935 0.2670 0.3451 0.4248 0.5028 0.5764 0.6430

Table with 9 columns of numerical data for P1, QMIN, SCAL, QMAX, and B values from 0.0 to 0.9.

Table with 9 columns of numerical data for B values from 0.5 to 1.9.

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Sample size = 64

E = 0.5(0.2)1.9

AMU = 1.3 (PO = 0.0968)

P1 0.1151 0.1775 0.2478 0.3239 0.4032 0.4825 0.5586 0.6289

Table with 9 columns of numerical data for P1, QMIN, SCAL, QMAX, and B values from 0.0 to 0.9.

Table with 9 columns of numerical data for B values from 0.5 to 1.9.

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Sample size = 64

B = 0.5(0.2)1.9

AMU = 1.6 (PO = 0.0548)

P1 0.0809 0.1293 0.1872 0.2537 0.3273 0.4054 0.4850 0.5631

Table with 8 columns and 47 rows of numerical data. Includes labels like QMIN, SCAL, QMAX, and B values.

Table with 8 columns and 47 rows of numerical data, corresponding to the first table. Includes labels like B values and numerical values.

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Sample size = 64

B = 0.5(0.2)1.9

AMU = 1.7 (PO = 0.0446)

P1 0.0705 0.1141 0.1673 0.2297 0.3000 0.3762 0.4554 0.5347

Table with 8 columns and 47 rows of numerical data. Includes labels like QMIN, SCAL, QMAX, and B values.

Table with 8 columns and 47 rows of numerical data, corresponding to the second table. Includes labels like B values and numerical values.

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Sample size =128

B = 0.5(0.2)1.9

AMU = 0.5 (P0 = 0.3085)

P1 0.1915 0.2707 0.3469 0.4172 0.4796 0.5328 0.5764 0.6107

Table with 8 columns and 48 rows of numerical data. Includes header row with B values and a row for QMIN, SCAL, and QMAX. The data shows a progression of values from 0.0000 to 1.0000 across the rows.

Table with 8 columns and 17 rows of numerical data. Header row shows B values from 0.5 to 1.9. The data shows a progression of values from 0.3295 to 1.0000 across the rows.

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Sample size =128

B = 0.5(0.2)1.9

AMU = 0.6 (P0 = 0.2743)

P1 0.1859 0.2656 0.3437 0.4172 0.4838 0.5417 0.5901 0.6289

Table with 8 columns and 48 rows of numerical data. Includes header row with B values and a row for QMIN, SCAL, and QMAX. The data shows a progression of values from 0.0009 to 1.0000 across the rows.

Table with 8 columns and 17 rows of numerical data. Header row shows B values from 0.5 to 1.9. The data shows a progression of values from 0.4421 to 1.0000 across the rows.

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Sample size =128

B = 0.5(0.2)1.9

AMU = 0.7 (PC = 0.2420)

P1 0.1788 0.2580 0.3373 0.4135 0.4838 0.5462 0.5994 0.6430

Table with 9 columns and 48 rows of data. Header row: 100 QMIN 54.50 50.500 47.000 43.000 39.500 35.500 32.500 29.000. Header row 2: 100 SCAL 0.25 0.250 0.250 0.250 0.250 0.250 0.250 0.250. Header row 3: QMAX 0.80 0.755 0.720 0.680 0.645 0.605 0.575 0.540. Row 0: [0] 0.0007 0.0005 0.0005 0.0003 0.0003 0.0001 0.0001 0.0000. Row 47: [47] 0.3996 0.3780 0.4143 0.4007 0.4326 0.3957 0.4501 0.4200.

Table with 9 columns and 48 rows of data. Header row: * B =**(0.5)**(0.7)**(0.9)**(1.1)**(1.3)**(1.5)**(1.7)**(1.9)***. Row 48: [48] 0.4246 0.4028 0.4400 0.4268 0.4598 0.4235 0.4797 0.4509. Row 101: [101] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000.

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Sample size =128

B = 0.5(0.2)1.9

AMU = 0.8 (PC = 0.2119)

P1 0.1702 0.2483 0.3280 0.4061 0.4796 0.5462 0.6041 0.6525

Table with 9 columns and 48 rows of data. Header row: 100 QMIN 57.50 54.000 50.500 46.500 43.000 39.500 36.000 32.500. Header row 2: 100 SCAL 0.25 0.250 0.250 0.250 0.250 0.250 0.250 0.250. Header row 3: QMAX 0.83 0.790 0.755 0.715 0.680 0.645 0.610 0.575. Row 0: [0] 0.0003 0.0003 0.0004 0.0003 0.0003 0.0002 0.0001 0.0001. Row 47: [47] 0.3466 0.3624 0.3914 0.3752 0.4088 0.4347 0.4447 0.4310.

Table with 9 columns and 48 rows of data. Header row: * B =**(0.5)**(0.7)**(0.9)**(1.1)**(1.3)**(1.5)**(1.7)**(1.9)***. Row 48: [48] 0.3712 0.3874 0.4173 0.4011 0.4360 0.4630 0.4741 0.4616. Row 101: [101] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000.

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Sample size =128

B = 0.5(0.2)1.9

AMU = 0.9 (PO = 0.1841)

P1 0.1605 0.2367 0.3159 0.3952 0.4714 0.5417 0.6041 0.6573

Table with 8 columns and 47 rows of numerical data. Includes header row for P1 and a row for QMAX. The data represents cumulative distribution function values for various sample sizes.

Table with 8 columns and 101 rows of numerical data. Includes a header row for B and a row for QMAX. The data represents cumulative distribution function values for various sample sizes and AMU values.

***** continued on the right *****

Sample size =128

B = 0.5(0.2)1.9

AMU = 1.0 (PO = 0.1587)

P1 0.1499 0.2234 0.3015 0.3812 0.4593 0.5328 0.5994 0.6573

Table with 8 columns and 47 rows of numerical data. Includes header row for P1 and a row for QMAX. The data represents cumulative distribution function values for various sample sizes.

Table with 8 columns and 101 rows of numerical data. Includes a header row for B and a row for QMAX. The data represents cumulative distribution function values for various sample sizes and AMU values.

***** continued on the right *****

Sample size =128

B = 0.5(0.2)1.9

AMU = 1.1 (PC = 0.1357)

P1 0.1386 0.2089 0.2851 0.3643 0.4436 0.5198 0.5901 0.6525

Table with 100 rows and 10 columns of data. Includes header 'B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **' and values ranging from 0.0000 to 1.0000. The table is split into two columns of 50 columns each.

***** continued on the right *****

[101] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000

Sample size =128

B = 0.5(0.2)1.9

AMU = 1.2 (PC = 0.1151)

P1 0.1269 0.1935 0.2670 0.3451 0.4248 0.5028 0.5764 0.6430

Table with 100 rows and 10 columns of data. Includes header 'B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **' and values ranging from 0.0000 to 1.0000. The table is split into two columns of 50 columns each.

***** continued on the right *****

[101] 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000

Sample size =128

B = 0.5(0.2)1.9

AMU = 1.3 (P0 = 0.0968)

P1 0.1151 0.1775 0.2478 0.3239 0.4032 0.4825 0.5586 0.6289

Table with 10 columns and 101 rows. Header row: * B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **. Rows contain numerical data for various indices from 0 to 100.

***** continued on the right *****

Sample size =128

B = 0.5(0.2)1.9

AMU = 1.4 (P0 = 0.0808)

P1 0.1033 0.1612 0.2278 0.3013 0.3794 0.4591 0.5372 0.6107

Table with 10 columns and 101 rows. Header row: * B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **. Rows contain numerical data for various indices from 0 to 100.

***** continued on the right *****

Sample size =128

B = 0.5(0.2)1.9

AMU = 1.7 (P0 = 0.0446)

P1 0.0705 0.1141 0.1673 0.2297 0.3000 0.3762 0.4554 0.5347

	B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **																
100 QMIN	75.00	75.000	74.000	72.000	70.000	67.000	64.500	61.000	[48]	0.0093	0.0570	0.1328	0.1758	0.2555	0.2533	0.3385	0.3191
100 SCAL	0.25	0.250	0.250	0.250	0.250	0.250	0.250	0.250	[49]	0.0120	0.0692	0.1549	0.2014	0.2862	0.2830	0.3719	0.3512
QMAX	1.00	1.000	0.990	0.970	0.950	0.920	0.895	0.860	[51]	0.0199	0.0999	0.2066	0.2592	0.3529	0.3475	0.4415	0.4189
[0]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	[52]	0.0252	0.1187	0.2361	0.2914	0.3885	0.3818	0.4773	0.4539
[1]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	[53]	0.0318	0.1401	0.2680	0.3254	0.4252	0.4172	0.5135	0.4894
[2]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	[54]	0.0398	0.1641	0.3022	0.3612	0.4627	0.4535	0.5496	0.5251
[3]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	[55]	0.0494	0.1909	0.3385	0.3984	0.5008	0.4903	0.5855	0.5607
[4]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	[56]	0.0608	0.2203	0.3765	0.4368	0.5390	0.5273	0.6207	0.5958
[5]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	[57]	0.0744	0.2525	0.4161	0.4760	0.5771	0.5642	0.6551	0.6303
[6]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	[58]	0.0902	0.2872	0.4568	0.5157	0.6146	0.6007	0.6884	0.6639
[7]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	[59]	0.1085	0.3244	0.4983	0.5555	0.6513	0.6366	0.7204	0.6963
[8]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	[60]	0.1295	0.3637	0.5401	0.5950	0.6868	0.6714	0.7507	0.7274
[9]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0001	[61]	0.1534	0.4048	0.5818	0.6338	0.7208	0.7049	0.7793	0.7568
[10]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0001	[62]	0.1803	0.4474	0.6228	0.6715	0.7531	0.7369	0.8060	0.7845
[11]	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0001	[63]	0.2102	0.4909	0.6629	0.7077	0.7835	0.7671	0.8308	0.8104
[12]	0.0000	0.0000	0.0000	0.0000	0.0001	0.0001	0.0001	0.0002	[64]	0.2432	0.5350	0.7014	0.7423	0.8117	0.7955	0.8535	0.8343
[13]	0.0000	0.0000	0.0000	0.0000	0.0001	0.0001	0.0001	0.0003	[65]	0.2790	0.5790	0.7382	0.7747	0.8377	0.8217	0.8741	0.8563
[14]	0.0000	0.0000	0.0000	0.0000	0.0001	0.0001	0.0001	0.0004	[66]	0.3177	0.6225	0.7727	0.8050	0.8614	0.8459	0.8927	0.8763
[15]	0.0000	0.0000	0.0000	0.0001	0.0002	0.0002	0.0002	0.0005	[67]	0.3588	0.6648	0.8048	0.8328	0.8827	0.8679	0.9093	0.8943
[16]	0.0000	0.0000	0.0000	0.0001	0.0002	0.0003	0.0003	0.0006	[68]	0.4020	0.7056	0.8342	0.8581	0.9017	0.8877	0.9240	0.9103
[17]	0.0000	0.0000	0.0000	0.0001	0.0003	0.0004	0.0004	0.0008	[69]	0.4470	0.7443	0.8608	0.8808	0.9184	0.9054	0.9368	0.9246
[18]	0.0000	0.0000	0.0001	0.0001	0.0005	0.0005	0.0012	0.0011	[70]	0.4931	0.7805	0.8846	0.9010	0.9330	0.9210	0.9479	0.9371
[19]	0.0000	0.0000	0.0001	0.0002	0.0006	0.0007	0.0017	0.0015	[71]	0.5398	0.8139	0.9055	0.9187	0.9456	0.9347	0.9575	0.9479
[20]	0.0000	0.0000	0.0001	0.0003	0.0008	0.0009	0.0022	0.0019	[72]	0.5865	0.8443	0.9236	0.9340	0.9562	0.9465	0.9656	0.9572
[21]	0.0000	0.0000	0.0002	0.0004	0.0011	0.0013	0.0029	0.0025	[73]	0.6325	0.8716	0.9391	0.9471	0.9652	0.9566	0.9724	0.9652
[22]	0.0000	0.0000	0.0002	0.0005	0.0015	0.0017	0.0037	0.0033	[74]	0.6773	0.8956	0.9522	0.9581	0.9727	0.9651	0.9781	0.9719
[23]	0.0000	0.0000	0.0003	0.0007	0.0020	0.0022	0.0048	0.0043	[75]	0.7201	0.9164	0.9630	0.9672	0.9788	0.9723	0.9828	0.9776
[24]	0.0000	0.0001	0.0004	0.0010	0.0026	0.0029	0.0061	0.0055	[76]	0.7604	0.9342	0.9719	0.9747	0.9837	0.9782	0.9866	0.9823
[25]	0.0000	0.0001	0.0006	0.0013	0.0034	0.0037	0.0078	0.0070	[77]	0.7978	0.9490	0.9789	0.9808	0.9877	0.9831	0.9897	0.9861
[26]	0.0000	0.0001	0.0008	0.0018	0.0044	0.0048	0.0099	0.0088	[78]	0.8320	0.9612	0.9845	0.9856	0.9908	0.9870	0.9922	0.9892
[27]	0.0000	0.0002	0.0011	0.0023	0.0057	0.0062	0.0124	0.0111	[79]	0.8626	0.9711	0.9888	0.9894	0.9932	0.9901	0.9941	0.9917
[28]	0.0000	0.0003	0.0015	0.0030	0.0073	0.0078	0.0154	0.0139	[80]	0.8895	0.9789	0.9921	0.9923	0.9951	0.9926	0.9956	0.9937
[29]	0.0000	0.0004	0.0020	0.0040	0.0092	0.0099	0.0190	0.0172	[81]	0.9128	0.9849	0.9945	0.9945	0.9965	0.9945	0.9968	0.9952
[30]	0.0000	0.0005	0.0026	0.0051	0.0116	0.0124	0.0234	0.0212	[82]	0.9325	0.9894	0.9963	0.9961	0.9975	0.9960	0.9976	0.9965
[31]	0.0000	0.0007	0.0034	0.0066	0.0145	0.0154	0.0286	0.0259	[83]	0.9489	0.9928	0.9975	0.9973	0.9983	0.9971	0.9983	0.9974
[32]	0.0000	0.0010	0.0045	0.0084	0.0181	0.0191	0.0347	0.0315	[84]	0.9621	0.9952	0.9984	0.9982	0.9988	0.9979	0.9988	0.9981
[33]	0.0001	0.0013	0.0058	0.0106	0.0223	0.0235	0.0418	0.0381	[85]	0.9726	0.9969	0.9990	0.9988	0.9992	0.9985	0.9992	0.9986
[34]	0.0001	0.0018	0.0075	0.0134	0.0274	0.0287	0.0501	0.0458	[86]	0.9807	0.9981	0.9994	0.9992	0.9995	0.9990	0.9994	0.9990
[35]	0.0002	0.0024	0.0096	0.0168	0.0335	0.0349	0.0597	0.0547	[87]	0.9868	0.9988	0.9996	0.9995	0.9997	0.9993	0.9996	0.9993
[36]	0.0002	0.0032	0.0123	0.0209	0.0406	0.0422	0.0706	0.0649	[88]	0.9912	0.9993	0.9998	0.9997	0.9998	0.9995	0.9997	0.9995
[37]	0.0003	0.0042	0.0155	0.0259	0.0490	0.0506	0.0831	0.0765	[89]	0.9944	0.9996	0.9999	0.9998	0.9999	0.9997	0.9998	0.9997
[38]	0.0004	0.0055	0.0195	0.0318	0.0587	0.0603	0.0972	0.0897	[90]	0.9965	0.9998	0.9999	0.9999	0.9999	0.9998	0.9999	0.9998
[39]	0.0006	0.0072	0.0244	0.0388	0.0699	0.0716	0.1131	0.1045	[91]	0.9979	0.9999	1.0000	0.9999	1.0000	0.9999	0.9999	0.9999
[40]	0.0009	0.0093	0.0302	0.0471	0.0827	0.0843	0.1307	0.1211	[92]	0.9988	0.9999	1.0000	1.0000	1.0000	0.9999	1.0000	0.9999
[41]	0.0012	0.0120	0.0372	0.0568	0.0973	0.0988	0.1502	0.1394	[93]	0.9994	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	0.9999
[42]	0.0016	0.0153	0.0456	0.0680	0.1138	0.1150	0.1716	0.1596	[94]	0.9997	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[43]	0.0022	0.0194	0.0554	0.0810	0.1322	0.1332	0.1949	0.1817	[95]	0.9999	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[44]	0.0030	0.0244	0.0669	0.0958	0.1527	0.1532	0.2201	0.2057	[96]	0.9999	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[45]	0.0040	0.0305	0.0802	0.1126	0.1752	0.1753	0.2472	0.2315	[97]	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[46]	0.0054	0.0378	0.0955	0.1314	0.1999	0.1993	0.2761	0.2590	[98]	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[47]	0.0071	0.0466	0.1130	0.1525	0.2267	0.2253	0.3066	0.2883	[99]	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[100]	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	[100]	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
[101]	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	[101]	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000

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Sample size =128

B = 0.5(0.2)1.9

AMU = 1.8 (P0 = 0.0359)

P1 0.0609 0.0997 0.1481 0.2060 0.2726 0.3462 0.4242 0.5039

	B = ** (0.5) ** (0.7) ** (0.9) ** (1.1) ** (1.3) ** (1.5) ** (1.7) ** (1.9) **													
100 QMIN	86.50	75.000	74.500	73.500	71.500	69.500	66.500	63.500	[48]	0.2519	0.0098	0.0439	0.1166	0.165

Sample size =128

B = 0.5(0.2)1.9

AMU = 2.1 (PO = 0.0179)

P1 0.0369 0.0629 0.0972 0.1408 0.1940 0.2564 0.3267 0.4029

Table with 8 columns of numerical values, rows labeled 00 to 47, and a header row with B values: B = 0.5, 0.7, 0.9, 1.1, 1.3, 1.5, 1.7, 1.9.

Table with 8 columns of numerical values, rows labeled 48 to 101, and a header row with B values: B = 0.5, 0.7, 0.9, 1.1, 1.3, 1.5, 1.7, 1.9.

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Sample size =128

B = 0.5(0.2)1.9

AMU = 2.2 (PO = 0.0139)

P1 0.0307 0.0529 0.0829 0.1218 0.1702 0.2281 0.2946 0.3682

Table with 8 columns of numerical values, rows labeled 00 to 47, and a header row with B values: B = 0.5, 0.7, 0.9, 1.1, 1.3, 1.5, 1.7, 1.9.

Table with 8 columns of numerical values, rows labeled 48 to 101, and a header row with B values: B = 0.5, 0.7, 0.9, 1.1, 1.3, 1.5, 1.7, 1.9.

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0.01 0.1335 0.0954 0.0742 0.0607 0.0514 0.0445 0.0393 0.0352
 0.02 0.1000 0.1416 0.1158 0.0980 0.0849 0.0749 0.0671 0.0618
 0.03 0.1000 0.2435 0.1896 0.1551 0.1312 0.1137 0.1004 0.0898
 0.04 0.1000 0.1000 0.2281 0.1866 0.1579 0.1369 0.1208 0.1081
 0.05 0.1000 0.1000 0.2135 0.1807 0.1566 0.1381 0.1236
 0.06 0.2739 0.2509 0.1000 0.2372 0.2007 0.1739 0.1535 0.1373
 0.07 0.7183 0.6449 0.5928 0.5486 0.5080 0.4785 0.4593 0.4444
 0.08 0.2279 0.6526 0.5996 0.5548 0.5138 0.4835 0.4444 0.4091
 0.09 0.7375 0.6603 0.6063 0.5610 0.5196 0.4893 0.4494 0.4139
 0.10 0.1000 0.9242 0.8652 0.8137 0.7650 0.7331 0.6869 0.6429
 0.11 0.1000 0.9389 0.8789 0.8268 0.7778 0.7438 0.6976 0.6533
 0.12 0.1000 0.9541 0.8933 0.8407 0.7913 0.7500 0.7089 0.6645
 0.13 0.1000 0.9415 0.8820 0.8340 0.7896 0.7495 0.7042 0.6645
 0.14 0.1000 0.9600 0.9060 0.8566 0.8082 0.7608 0.7207 0.6839
 0.15 0.1000 0.1000 0.9803 0.9272 0.8776 0.8293 0.7818 0.7399

*****TEST CRITERION / T *****
 * S.SIZE= 4 " Ramp case" AMU= .7011.e. FO= 0.24196) *
 * GMIN x100: 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 *
 * SCALEx100: 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 *
 * P1 x 100: 17.83 25.80 33.73 41.35 48.38 54.62 59.94 64.30 *

0.01 0.0679 0.0485 0.0378 0.0309 0.0262 0.0227 0.0200 0.0179
 0.02 0.1758 0.1256 0.0977 0.0799 0.0676 0.0586 0.0517 0.0465
 0.03 0.1000 0.1817 0.1413 0.1157 0.0979 0.0848 0.0748 0.0670
 0.04 0.1000 0.2273 0.1768 0.1466 0.1224 0.1061 0.0937 0.0837
 0.05 0.1000 0.1000 0.2071 0.1695 0.1434 0.1243 0.1097 0.0981
 0.06 0.1000 0.1000 0.2340 0.1915 0.1620 0.1404 0.1239 0.1108
 0.07 0.6522 0.5908 0.5443 0.5032 0.4804 0.4383 0.4015 0.3688
 0.08 0.6620 0.5986 0.5511 0.5095 0.4862 0.4436 0.4065 0.3734
 0.09 0.6717 0.6065 0.5580 0.5157 0.4920 0.4490 0.4115 0.3781
 0.10 0.9520 0.8781 0.8210 0.7700 0.7445 0.6959 0.6500 0.6066
 0.11 0.9706 0.8942 0.8359 0.7841 0.7400 0.7070 0.6609 0.6171
 0.12 0.9898 0.9110 0.8515 0.7990 0.7500 0.7189 0.6725 0.6284
 0.13 0.1000 0.9670 0.9045 0.8502 0.7993 0.7505 0.7139 0.6688
 0.14 0.1000 0.9883 0.9251 0.8705 0.8193 0.7700 0.7310 0.6857
 0.15 0.1000 0.1000 0.9479 0.8933 0.8421 0.7925 0.7450 0.7053

*****TEST CRITERION / T *****
 * S.SIZE= 4 " Ramp case" AMU= .5011.e. FO= 0.24253 *
 * GMIN x100: 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 *
 * SCALEx100: 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 *
 * P1 x 100: 18.59 26.56 34.57 41.72 48.38 54.17 59.01 62.89 *

0.01 0.0116 0.0083 0.0065 0.0053 0.0045 0.0039 0.0034 0.0031
 0.02 0.1061 0.0758 0.0589 0.0482 0.0408 0.0354 0.0312 0.0279
 0.03 0.1767 0.1262 0.0982 0.0803 0.0680 0.0589 0.0520 0.0465
 0.04 0.2347 0.1677 0.1304 0.1067 0.0903 0.0783 0.0690 0.0618
 0.05 0.1000 0.2035 0.1533 0.1295 0.1098 0.0950 0.0838 0.0750
 0.06 0.1000 0.2353 0.1830 0.1498 0.1267 0.1093 0.0969 0.0867
 0.07 0.5850 0.5333 0.4843 0.4380 0.3990 0.3646 0.3341 0.3064
 0.08 0.5949 0.5433 0.5014 0.4905 0.4437 0.4042 0.3695 0.3386
 0.09 0.6043 0.5513 0.5084 0.4968 0.4495 0.4095 0.3744 0.3432
 0.10 0.8939 0.8267 0.7723 0.7061 0.6577 0.6123 0.5697 0.5297
 0.11 0.9145 0.8444 0.7883 0.7100 0.6691 0.6335 0.5918 0.5518
 0.12 0.9258 0.8628 0.8053 0.7335 0.6812 0.6352 0.5918 0.5518
 0.13 0.1000 0.9248 0.8631 0.8085 0.7573 0.7244 0.6774 0.6327
 0.14 0.1000 0.9486 0.8858 0.8305 0.7787 0.7422 0.6949 0.6498
 0.15 0.1000 0.9747 0.9111 0.8554 0.8030 0.7528 0.7155 0.6798

*****TEST CRITERION / T *****
 * S.SIZE= 4 " Ramp case" AMU= .5011.e. FO= 0.30854) *
 * GMIN x100: 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 *
 * SCALEx100: 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 *
 * P1 x 100: 19.15 27.07 34.69 41.72 47.96 53.28 57.64 61.07 *

0.01 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500
 0.02 0.0452 0.0325 0.0251 0.0205 0.0174 0.0151 0.0133 0.0119
 0.03 0.1078 0.0770 0.0599 0.0490 0.0415 0.0359 0.0317 0.0284
 0.04 0.1600 0.1143 0.0889 0.0728 0.0616 0.0534 0.0471 0.0421
 0.05 0.2056 0.1469 0.1142 0.0935 0.0791 0.0685 0.0605 0.0541
 0.06 0.2459 0.1760 0.1369 0.1120 0.0948 0.0822 0.0723 0.0649
 0.07 0.5161 0.1000 0.4916 0.4390 0.3967 0.3605 0.3287 0.3004
 0.08 0.5262 0.1000 0.4986 0.4452 0.4023 0.3657 0.3335 0.3049
 0.09 0.5363 0.1000 0.4974 0.4514 0.4079 0.3709 0.3383 0.3094
 0.10 0.8293 0.7699 0.7182 0.6683 0.6185 0.5740 0.5325 0.4944
 0.11 0.8519 0.7890 0.7306 0.6787 0.6301 0.5852 0.5432 0.5047
 0.12 0.8754 0.8091 0.7545 0.7036 0.6591 0.6226 0.5922 0.5547
 0.13 0.9536 0.8773 0.8170 0.7624 0.7133 0.6701 0.6329 0.5961
 0.14 0.9838 0.9037 0.8417 0.7855 0.7350 0.7051 0.6759 0.6454
 0.15 0.1000 0.9330 0.8696 0.8134 0.7606 0.7262 0.6787 0.6356

*****TEST CRITERION / T *****
 * S.SIZE= 4 " Ramp case" AMU= .4811.e. FO= 0.34457) *
 * GMIN x100: 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 *
 * SCALEx100: 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 *
 * P1 x 100: 19.52 27.33 34.69 41.35 47.16 51.98 55.84 57.86 *

```

* S.SIZE= 4      " Ramp case"      ANU= .80(i.e. PO= 0.2110) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 17.02 24.83 32.80 40.61 47.92 54.62 61.41 65.25 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      0.2088 0.1492 0.1161 0.0950 0.0804 0.0697 0.0615 0.0550
0.02      -0.1000 0.2447 0.1906 0.1560 0.1320 0.1144 0.1009 0.0903
0.03      -0.1000-0.1000 0.2428 0.1987 0.1681 0.1457 0.1226 0.1151
0.04      0.2660-0.1000-0.1000 0.2328 0.1970 0.1707 0.1506 0.1248
0.05      0.3046 0.2756 0.2522-0.1000 0.2213 0.1918 0.1693 0.1514
0.06      0.3386 0.3015 0.2739-0.1000 0.2427 0.2104 0.1856 0.1661
0.49      -0.1000 0.6979 0.6401 0.5930 0.5505 0.5107 0.4778 0.4407
0.50      -0.1000 0.7055 0.6467 0.5990 0.5563 0.5161 0.4829 0.4456
0.51      -0.1000 0.7131 0.6533 0.6051 0.5620 0.5215 0.4820 0.4504
0.89      -0.1000 0.9657 0.9052 0.8536 0.8053 0.7586 0.7229 0.6787
0.90      -0.1000 0.9790 0.9177 0.8657 0.8173 0.7704 0.7333 0.6969
0.91      -0.1000 0.9927 0.9308 0.8785 0.8299 0.7828 0.7443 0.6998
0.94      -0.1000-0.1000 0.9744 0.9219 0.8733 0.8261 0.7796 0.7387
0.95      -0.1000-0.1000 0.9909 0.9387 0.8904 0.8434 0.7970 0.7514
0.96      -0.1000-0.1000-0.1000 0.9574 0.9097 0.8631 0.8169 0.7712

```

```

* S.SIZE= 4      " Ramp case"      ANU= .90(i.e. PO= 0.1840) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 16.05 23.67 31.59 39.52 47.12 54.17 61.41 65.73 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      -0.1000 0.2100 0.1633 0.1337 0.1131 0.0980 0.0865 0.0774
0.02      -0.1000-0.1000 0.2447 0.2004 0.1695 0.1469 0.1297 0.1160
0.03      0.2822 0.2595-0.1000 0.2463 0.2086 0.1808 0.1595 0.1427
0.04      0.3304 0.2960 0.2700-0.1000 0.2394 0.2075 0.1831 0.1633
0.05      0.3717 0.3273 0.2961 0.2697-0.1000 0.2300 0.2030 0.1816
0.06      0.4083 0.3549 0.3191 0.2899 0.2636 0.2495 0.2204 0.1972
0.49      -0.1000-0.1000 0.6862 0.6362 0.5921 0.5510 0.5120 0.4777
0.50      -0.1000-0.1000 0.6928 0.6421 0.5977 0.5564 0.5171 0.4826
0.51      -0.1000-0.1000 0.6993 0.6481 0.6033 0.5617 0.5222 0.4875
0.89      -0.1000-0.1000 0.9411 0.8897 0.8423 0.7964 0.7513 0.7135
0.90      -0.1000-0.1000 0.9525 0.9009 0.8535 0.8074 0.7621 0.7235
0.91      -0.1000-0.1000 0.9643 0.9127 0.8652 0.8191 0.7738 0.7342
0.94      -0.1000-0.1000-0.1000 0.9521 0.9052 0.8596 0.8144 0.7695
0.95      -0.1000-0.1000-0.1000 0.9673 0.9209 0.8757 0.8307 0.7860
0.96      -0.1000-0.1000-0.1000 0.9839 0.9384 0.8939 0.8494 0.8048

```

```

* S.SIZE= 4      " Ramp case"      ANU= 1.00(i.e. PO= 0.1586) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 14.99 22.34 30.15 38.12 45.93 53.28 59.94 65.73 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      -0.1000-0.1000 0.2160 0.1768 0.1496 0.1297 0.1144 0.1024
0.02      0.2829 0.2606-0.1000 0.2485 0.2107 0.1826 0.1611 0.1442
0.03      0.3475 0.3097 0.2822 0.2583-0.1000 0.2188 0.1931 0.1727
0.04      0.3997 0.3490 0.3149 0.2869 0.2613 0.2472 0.2182 0.1952
0.05      0.4440 0.3823 0.3424 0.3111 0.2834 0.2578 0.2392 0.2140
0.06      0.4829 0.4115 0.3665 0.3321 0.3026 0.2756 0.2505 0.2305
0.49      -0.1000-0.1000 0.7315 0.6783 0.6326 0.5905 0.5506 0.5125
0.50      -0.1000-0.1000 0.7378 0.6841 0.6381 0.5958 0.5556 0.5174
0.51      -0.1000-0.1000 0.7444 0.6900 0.6436 0.6010 0.5607 0.5223
0.89      -0.1000-0.1000 0.9224 0.9224 0.8761 0.8313 0.7870 0.7474
0.90      -0.1000-0.1000 0.9337 0.9327 0.8864 0.8417 0.7974 0.7535
0.91      -0.1000-0.1000 0.9444 0.9434 0.8972 0.8526 0.8084 0.7644
0.94      -0.1000-0.1000-0.1000 0.9790 0.9339 0.8902 0.8465 0.8028
0.95      -0.1000-0.1000-0.1000 0.9925 0.9482 0.9050 0.8619 0.8184
0.96      -0.1000-0.1000-0.1000-0.1000 0.9639 0.9217 0.8792 0.8362

```

```

* S.SIZE= 4      " Ramp case"      ANU= 1.10(i.e. PO= 0.1356) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 13.86 20.89 28.51 36.43 44.36 51.98 59.01 65.25 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      -0.1000-0.1000-0.1000 0.2243 0.1892 0.1645 0.1452 0.1299
0.02      0.3482 0.3110 0.2841 0.2604-0.1000 0.2213 0.1953 0.1747
0.03      0.4184 0.3637 0.3277 0.2988 0.2728-0.1000 0.2292 0.2051
0.04      0.4743 0.4055 0.3621 0.3289 0.3002 0.2738-0.1000 0.2288
0.05      -0.1000 0.4407 0.3910 0.3541 0.3230 0.2949 0.2690 0.2486
0.06      -0.1000 0.4715 0.4162 0.3759 0.3427 0.3132 0.2861 0.2613
0.49      0.7667-0.1000-0.1000 0.7194 0.6721 0.6291 0.5885 0.5496
0.50      0.7774-0.1000-0.1000 0.7251 0.6775 0.6343 0.5935 0.5544
0.51      0.7879 0.7517-0.1000 0.7308 0.6829 0.6395 0.5985 0.5593
0.89      -0.1000-0.1000-0.1000 0.9518 0.9067 0.8634 0.8203 0.7773
0.90      -0.1000-0.1000-0.1000 0.9611 0.9162 0.8730 0.8301 0.7872
0.91      -0.1000-0.1000-0.1000 0.9708 0.9261 0.8832 0.8404 0.7976
0.94      -0.1000-0.1000-0.1000-0.1000 0.9595 0.9178 0.8761 0.8339
0.95      -0.1000-0.1000-0.1000-0.1000 0.9723 0.9315 0.8903 0.8486
0.96      -0.1000-0.1000-0.1000-0.1000 0.9864 0.9466 0.9064 0.8652

```

```

* S.SIZE= 4      " Ramp case"      AMU=1.20(i.e. PO= 0.11507) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 12.67 19.35 26.70 34.51 42.42 50.24 57.64 64.37 *
*****
PEQ < T] .....TEST CRITERION ,T .....
0.01      0.3109 0.2836 0.2619-0.1000 0.2336 0.2125 0.1787 0.1599
0.02      0.4194 0.3649 0.3294 0.3010 0.2754 0.2509 0.2320 0.2075
0.03      0.4947 0.4212 0.3756 0.3413 0.3120 0.2851 0.2600 0.2396
0.04      -0.1000 0.4655 0.4117 0.3726 0.3403 0.3114 0.2847 0.2601
0.05      -0.1000-0.1000 0.4419 0.3987 0.3638 0.3331 0.3051 0.2793
0.06      -0.1000-0.1000 0.4681 0.4213 0.3841 0.3512 0.3226 0.2958
0.49      0.8286 0.7853 0.7503-0.1000 0.7105 0.6667 0.6236 0.5861
0.50      0.8387 0.7939 0.7570-0.1000 0.7158 0.6718 0.6305 0.5909
0.51      0.8486 0.8013 0.7638-0.1000 0.7211 0.6768 0.6354 0.5956
0.89      -0.1000-0.1000-0.1000 0.9782 0.9343 0.8926 0.8511 0.8094
0.90      -0.1000-0.1000-0.1000 0.9866 0.9430 0.9015 0.8603 0.8187
0.91      -0.1000-0.1000-0.1000 0.9954 0.9521 0.9109 0.8699 0.8285
0.94      -0.1000-0.1000-0.1000-0.1000 0.9822 0.9427 0.9031 0.8627
0.95      -0.1000-0.1000-0.1000-0.1000 0.9937 0.9551 0.9162 0.8764
0.96      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9687 0.9310 0.8919

```

```

* S.SIZE= 4      " Ramp case"      AMU=1.30(i.e. PO= 0.09680) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 11.51 17.75 24.78 32.39 40.32 48.25 55.86 62.89 *
*****
PEQ < T] .....TEST CRITERION ,T .....
0.01      0.3729 0.3353 0.3058 0.2810 0.2571 0.2434 0.2148 0.1922
0.02      0.4962 0.4228 0.3774 0.3435 0.3146 0.2880 0.2630 0.2426
0.03      -0.1000 0.4825 0.4260 0.3855 0.3524 0.3231 0.2960 0.2709
0.04      -0.1000-0.1000 0.4637 0.4180 0.3816 0.3500 0.3213 0.2947
0.05      -0.1000-0.1000 0.4951 0.4450 0.4057 0.3722 0.3421 0.3143
0.06      0.5147-0.1000-0.1000 0.4683 0.4265 0.3913 0.3599 0.3312
0.49      0.8863 0.8334 0.7934 0.7568 0.7460 0.7032 0.6617 0.6219
0.50      0.8959 0.8410 0.8000 0.7627-0.1000 0.7082 0.6665 0.6266
0.51      0.9054 0.8485 0.8065 0.7688-0.1000 0.7131 0.6713 0.6312
0.89      -0.1000-0.1000-0.1000-0.1000 0.9592 0.9191 0.8794 0.8392
0.90      -0.1000-0.1000-0.1000-0.1000 0.9671 0.9274 0.8879 0.8480
0.91      -0.1000-0.1000-0.1000-0.1000 0.9753 0.9360 0.8969 0.8572
0.94      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9649 0.9275 0.8892
0.95      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9760 0.9395 0.9019
0.96      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9882 0.9529 0.9163

```

```

* S.SIZE= 4      " Ramp case"      AMU=1.40(i.e. PO= 0.07670) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 10.33 16.12 22.78 30.13 37.94 45.91 53.72 61.07 *
*****
PEQ < T] .....TEST CRITERION ,T .....
0.01      0.4534 0.3912 0.3523 0.3224 0.2961 0.2712-0.1000 0.2268
0.02      -0.1000 0.4846 0.4280 0.3878 0.3551 0.3261 0.2992 0.2741
0.03      -0.1000-0.1000 0.4788 0.4313 0.3941 0.3620 0.3329 0.3059
0.04      0.5050-0.1000-0.1000 0.4649 0.4240 0.3895 0.3586 0.3302
0.05      0.5430 0.5154-0.1000 0.4928 0.4487 0.4121 0.3798 0.3502
0.06      0.5774 0.5421 0.5134-0.1000 0.4700 0.4316 0.3979 0.3673
0.49      0.9406 0.8776 0.8334 0.7953 0.7586 0.7386 0.6967 0.6568
0.50      0.9498 0.8848 0.8397 0.8011 0.7640 0.7435 0.7014 0.6614
0.51      0.9588 0.8919 0.8459 0.8068 0.7694 0.7485 0.7061 0.6659
0.89      -0.1000-0.1000-0.1000-0.1000 0.9815 0.9431 0.9052 0.8668
0.90      -0.1000-0.1000-0.1000-0.1000 0.9887 0.9506 0.9131 0.8750
0.91      -0.1000-0.1000-0.1000-0.1000 0.9961 0.9585 0.9214 0.8836
0.94      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9846 0.9495 0.9133
0.95      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9945 0.9604 0.9250
0.96      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9724 0.9382

```

```

* S.SIZE= 4      " Ramp case"      AMU=1.50(i.e. PO= 0.06681) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 9.13 14.50 20.74 27.78 35.39 43.32 51.25 58.86 *
*****
PEQ < T] .....TEST CRITERION ,T .....
0.01      -0.1000 0.4513 0.4016 0.3656 0.3358 0.3088 0.2833 0.2592
0.02      -0.1000-0.1000 0.4812 0.4338 0.3968 0.3650 0.3362 0.3093
0.03      0.5154-0.1000-0.1000 0.4788 0.4368 0.4017 0.3705 0.3417
0.04      0.5647 0.5336 0.5082-0.1000 0.4675 0.4297 0.3966 0.3664
0.05      0.6057 0.5650 0.5344 0.5062 0.4928 0.4528 0.4180 0.3866
0.06      0.6415 0.5922 0.5573 0.5266-0.1000 0.4723 0.4364 0.4039
0.49      0.9922 0.9188 0.8704 0.8309 0.7941 0.7573 0.7307 0.6906
0.50      -0.1000 0.9256 0.8763 0.8363 0.7992 0.7623 0.7353 0.6951
0.51      -0.1000 0.9324 0.8822 0.8417 0.8044 0.7673 0.7399 0.6996
0.89      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9646 0.9287 0.8921
0.90      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9715 0.9359 0.8997
0.91      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9786 0.9435 0.9078
0.94      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9690 0.9351
0.95      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9788 0.9459
0.96      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9896 0.9579

```



```

* S.SIZE= 4 " Ramp case" AMU=2.00(i.e. PO= 0.0227) *
*****
* QMIN x100:50.000050.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 0.5000 0.5000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 4.41 7.41 11.29 16.13 21.92 28.57 33.93 43.74 *
*****
P[0 < T] .....TEST CRITERION ,T .....
0.01 0.6920 0.6321 0.5738 0.5420 0.5220-0.1000 0.4719 0.4393
0.02 0.7551 0.7076 0.6439 0.6091 0.5790 0.5499 0.5201 0.4923
0.03 0.7793-0.1000 0.6899 0.6488 0.6151 0.5839 0.5530 0.5217
0.04 0.8018 0.7669 0.7249 0.6789 0.6422 0.6095 0.5777 0.5457
0.05 0.8225 0.7832-0.1000 0.7036 0.6645 0.6303 0.5977 0.5652
0.06 0.8419 0.7984-0.1000 0.7246 0.6834 0.6479 0.6146 0.5818
0.49 -0.1000-0.1000-0.1000 0.9730 0.9341 0.9001 0.8676 0.8348
0.50 -0.1000-0.1000-0.1000 0.9772 0.9379 0.9038 0.8713 0.8385
0.51 -0.1000-0.1000-0.1000 0.9813 0.9418 0.9075 0.8750 0.8422
0.89 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9874
0.90 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9923
0.91 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9973
0.94 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.95 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.96 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000

```

```

* S.SIZE= 4 " Ramp case" AMU=2.10(i.e. PO= 0.0178) *
*****
* QMIN x100:50.000050.000050.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 3.69 6.29 9.72 14.08 19.40 25.64 32.67 40.29 *
*****
P[0 < T] .....TEST CRITERION ,T .....
0.01 0.7472 0.6736 0.6293 0.5853 0.5585 0.5316 0.5035 0.4762
0.02 0.7738-0.1000 0.6955 0.6473 0.6147 0.5847 0.5549 0.5244
0.03 0.8005 0.7691 0.7401 0.6874 0.6508 0.6184 0.5874 0.5561
0.04 0.8249 0.7881 0.7594 0.7178 0.6790 0.6438 0.6118 0.5797
0.05 0.8473 0.8055 0.7745 0.7428 0.7092 0.6643 0.6312 0.5988
0.06 0.8681 0.8215 0.7884-0.1000 0.7190 0.6818 0.6478 0.6149
0.49 -0.1000-0.1000-0.1000 0.9964 0.9563 0.9223 0.8906 0.8591
0.50 -0.1000-0.1000-0.1000-0.1000 0.9600 0.9258 0.8941 0.8626
0.51 -0.1000-0.1000-0.1000-0.1000 0.9636 0.9293 0.8976 0.8661
0.89 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.90 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.91 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.94 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.95 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.96 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000

```

```

* S.SIZE= 4 " Ramp case" AMU=2.20(i.e. PO= 0.0139) *
*****
* QMIN x100:50.000050.000050.000050.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 3.07 5.29 8.29 12.18 17.02 22.81 29.46 36.82 *
*****
P[0 < T] .....TEST CRITERION ,T .....
0.01 0.7572 0.7192 0.6670 0.6301 0.5935 0.5660 0.5380 0.5088
0.02 0.7919 0.7654 0.7368 0.6898 0.6499 0.6187 0.5887 0.5584
0.03 0.8218 0.7884 0.7627 0.7292 0.6861 0.6521 0.6206 0.5895
0.04 0.8486 0.8089 0.7802 0.7541 0.7133 0.6772 0.6445 0.6126
0.05 0.8730 0.8275 0.7961 0.7684 0.7354 0.6976 0.6638 0.6313
0.06 -0.1000 0.8445 0.8105 0.7816-0.1000 0.7149 0.6801 0.6471
0.49 -0.1000-0.1000-0.1000-0.1000 0.9772 0.9429 0.9118 0.8815
0.50 -0.1000-0.1000-0.1000-0.1000 0.9807 0.9462 0.9151 0.8848
0.51 -0.1000-0.1000-0.1000-0.1000 0.9841 0.9495 0.9184 0.8881
0.89 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.90 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.91 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.94 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.95 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.96 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000

```

```

* S.SIZE= 4 " Ramp case" AMU=2.30(i.e. PO= 0.0107) *
*****
* QMIN x100:50.000050.000050.000050.000050.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 1.0000 1.0000 1.0000 *
* P1 x 100: 2.52 4.41 7.00 10.43 14.79 20.11 26.35 33.39 *
*****
P[0 < T] .....TEST CRITERION ,T .....
0.01 0.7720 0.7551 0.7071 0.6651 0.6322 0.5995 0.5715 0.5426
0.02 0.8107 0.7823 0.7601 0.7269 0.6871 0.6519 0.6214 0.5912
0.03 0.8441 0.8076 0.7816 0.7576 0.7227 0.6851 0.6528 0.6217
0.04 0.8736 0.8299 0.8003 0.7748 0.7499 0.7101 0.6763 0.6444
0.05 -0.1000 0.8498 0.8170 0.7899 0.7635 0.7303 0.6954 0.6627
0.06 -0.1000 0.8679 0.8321 0.8035 0.7764 0.7477 0.7115 0.6782
0.49 -0.1000-0.1000-0.1000-0.1000 0.9970 0.9621 0.9314 0.9021
0.50 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9653 0.9345 0.9052
0.51 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9685 0.9376 0.9084
0.89 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.90 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.91 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.94 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.95 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000
0.96 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.1000

```


0.91 0.8922 0.8593 0.8593 0.8599 0.8194 0.8033 0.7870 0.7687
-0.1000 1.0000 0.9123 0.8512 0.8580 0.8586 0.8284 0.8015
-0.1000 0.9897 0.9111 0.8848 0.8821 0.8424 0.8228
-0.1000 0.1000 0.9663 0.9340 0.9039 0.1000 0.8389
0.05 -0.1000 0.1000 0.9904 0.9463 0.9201 0.8900 0.8518
0.06 -0.1000 0.1000 0.9651 0.9339 0.9030 0.8667 0.8628
-0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
-0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.51 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.50 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.49 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.51 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.89 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.91 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.94 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.95 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000

*****TEST CRITERION / T *****
P/E < T] *****
* S.SIZE= 4 " Ramp case" AMU=3.10(1.e., PU=C.00097) *
* GMIN X100: 75.000075.000075.000075.000075.000050.000050.000050.0000
* SCALEX100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.5000 0.5000 0.5000
* P1 X 100: 0.37 0.72 1.29 2.18 3.50 5.38 7.98 11.41 *

0.01 0.9171 0.8623 0.8599 0.8209 0.8033 0.7874 0.7652 0.7590
0.02 0.9631 0.9314 0.8898 0.8619 0.8423 0.8216 0.8010 0.7829
0.03 -0.1000 0.9539 0.9244 0.8909 0.8658 0.8448 0.8250 0.8046
0.04 -0.1000 0.9925 0.9383 0.9133 0.8767 0.8426 0.8210 0.8046
0.05 -0.1000 0.1000 0.9625 0.9317 0.8942 0.1000 0.8555 0.8342
-0.1000 0.1000 0.9830 0.9400 0.9090 0.2473 0.2671 0.8455
0.49 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.50 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.51 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.89 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.91 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.94 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.95 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000

*****TEST CRITERION / T *****
P/E < T] *****
* S.SIZE= 4 " Ramp case" AMU=2.90(1.e., PU=C.00133) *
* GMIN X100: 75.000075.000075.000075.000075.000050.000050.000050.0000
* SCALEX100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.5000 0.5000 0.5000
* P1 X 100: 0.49 0.94 1.65 2.74 4.52 6.55 9.55 13.43 *

0.01 0.8622 0.8274 0.8053 0.7885 0.7725 0.7550 0.7255 0.6554
0.02 0.9349 0.8803 0.8481 0.8251 0.8056 0.7865 0.7658 0.7599
0.03 -0.1000 0.9195 0.8517 0.8295 0.8090 0.7878 0.7643
0.04 -0.9895 0.1000 0.8812 0.8729 0.8484 0.8268 0.8068 0.7815
0.05 -0.1000 0.9519 0.9059 1.0000 0.8641 0.8411 0.8189 0.7955
0.06 -0.1000 0.9781 0.9266 0.8924 0.1000 0.8536 0.8309 0.8074
0.49 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.50 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.51 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.89 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.91 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.94 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000
0.95 -0.1000 0.1000 0.1000 0.1000 0.1000 0.1000 0.1000

*****TEST CRITERION / T *****
P/E < T] *****
* S.SIZE= 4 " Ramp case" AMU=2.50(1.e., PU=C.00257) *
* GMIN X100: 75.000075.000050.000050.000050.000050.000050.000050.0000
* SCALEX100: 0.2500 0.2500 0.2500 0.2500 0.5000 0.5000 0.5000 0.5000
* P1 X 100: 0.82 1.53 2.62 4.20 6.45 9.42 10.51 18.15 *

```

* S.SIZE= 4 " Ramp case" AMU=5.27(i.e. PO= 0.00069) *
*****
* QMIN x100:75.000075.000075.000075.000075.000075.000075.000050.000050.0000 *
* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.5000 0.5000 *
* P1 x 100: 0.28 0.55 1.00 1.72 2.80 4.39 6.61 9.61 *
*****
P[Q < T] .....TEST CRITERION ,T .....
0.01 0.9466 0.9183 0.8801 0.8548 0.8357 0.8194 0.8034 0.7863
0.02 -0.1000 0.9736 0.9359 0.9011 0.8758 0.8555 0.8372 0.8190
0.03 -0.1000-0.1000 0.9642 0.9318 0.9023 0.8792 0.8591 0.8400
0.04 -0.1000-0.1000 0.9941 0.9495 0.9224 0.8971-0.1000 0.8558
0.05 -0.1000-0.1000-0.1000 0.9694-0.1000 0.9116 0.8862 0.8585
0.06 -0.1000-0.1000-0.1000 0.9861 0.9492 0.9235 0.8979 0.8771
0.49 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.50 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.51 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.89 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.90 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.91 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.94 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.95 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.96 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000

```

```

* S.SIZE= 4 " Ramp case" AMU=3.30(i.e. PO= 0.00048) *
*****
* QMIN x100:75.000075.000075.000075.000075.000075.000075.000050.0000 *
* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.5000 *
* P1 x 100: 0.21 0.42 0.77 1.34 2.23 3.54 5.43 8.03 *
*****
P[Q < T] .....TEST CRITERION ,T .....
0.01 0.9963-0.1000 0.9024 0.8736 0.8526 0.8353 0.8195 0.8032
0.02 -0.1000-0.1000 0.9516 0.9216 0.8939 0.8722 0.8535 0.8357
0.03 -0.1000-0.1000 0.9920 0.9478 0.9207 0.8960 0.8754 0.8564
0.04 -0.1000-0.1000-0.1000 0.9724 1.0000 0.9140 0.8918 0.8718
0.05 -0.1000-0.1000-0.1000 0.9922 0.9546 0.9285 0.9058 0.8826
0.06 -0.1000-0.1000-0.1000-0.1000 0.9688 0.9387 0.9162 0.8933
0.49 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.50 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.51 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.89 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.90 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.91 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.94 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.95 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.96 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000

```

```

* S.SIZE= 4 " Ramp case" AMU=1.75(i.e. PO= 0.00034) *
*****
* QMIN x100:75.000075.000075.000075.000075.000075.000075.000075.0000 *
* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 *
* P1 x 100: 0.15 0.31 0.59 1.04 1.75 2.84 4.42 6.65 *
*****
P[Q < T] .....TEST CRITERION ,T .....
0.01 -0.1000 0.9618 0.9259 0.8933 0.8699 0.8514 0.8352 0.8194
0.02 -0.1000-0.1000 0.9794 1.0000 0.9121 0.8888 0.8694 0.8516
0.03 -0.1000-0.1000-0.1000 0.9707-0.1000 0.9128 0.8912 0.8720
0.04 -0.1000-0.1000-0.1000 0.9952 0.9572 0.9307 0.9074 0.8872
0.05 -0.1000-0.1000-0.1000-0.1000 0.9741 0.9435 0.9206 0.8995
0.06 -0.1000-0.1000-0.1000-0.1000 0.9882 0.9560 0.9316 0.9097
0.49 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.50 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.51 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.89 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.90 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.91 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.94 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.95 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.96 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000

```

```

* S.SIZE= 6      " Ramp case"      AMU= .40(i.e. PO= 0.34452) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 19.52 27.33 34.69 41.35 47.14 51.98 55.86 58.86 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      0.1736 0.1501 0.1316 0.1181 0.0999 0.0866 0.0764 0.0663
0.02      0.2282 0.1925 0.1678 0.1475 0.1299 0.1153 0.1017 0.0910
0.03      -0.1000 0.2220 0.1926 0.1696 0.1500 0.1332 0.1191 0.1065
0.04      0.2601 0.2453 0.2122 0.1869 0.1657 0.1475 0.1319 0.1188
0.05      0.2794 0.2513 0.2287 0.2014 0.1788 0.1595 0.1429 0.1287
0.06      0.2965 0.2656 0.2430 0.2140 0.1902 0.1699 0.1524 0.1373
0.49      0.5562 0.5128 0.4771 0.4374 0.4008 0.3672 0.3361 0.3081
0.50      0.5613 0.5172 0.4812 0.4412 0.4044 0.3706 0.3393 0.3111
0.51      0.5663 0.5217 0.4853 0.4451 0.4081 0.3741 0.3426 0.3142
0.89      -0.1000 0.7206 0.6733 0.6280 0.5856 0.5437 0.5040 0.4671
0.90      0.7577 0.7295 0.6821 0.6366 0.5937 0.5515 0.5116 0.4743
0.91      0.7701 0.7390 0.6914 0.6457 0.6025 0.5600 0.5197 0.4820
0.94      0.8128 0.7627 0.7246 0.6785 0.6334 0.5905 0.5491 0.5101
0.95      0.8296 0.7786 0.7382 0.6920 0.6467 0.6033 0.5614 0.5220
0.96      0.8483 0.7967 -0.1000 0.7078 0.6623 0.6183 0.5760 0.5360

```

```

* S.SIZE= 8      " Ramp case"      AMU= .50(i.e. PO= 0.30854) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 19.15 27.07 34.69 41.72 47.96 53.28 57.64 61.07 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      0.2209 0.1871 0.1634 0.1437 0.1264 0.1118 0.0986 0.0882
0.02      -0.1000 0.2343 0.2031 0.1790 0.1586 0.1410 0.1258 0.1131
0.03      0.2803 0.2528 0.2301 0.2027 0.1801 0.1607 0.1439 0.1296
0.04      0.3053 0.2735 -0.1000 0.2212 0.1968 0.1760 0.1580 0.1426
0.05      0.3265 0.2909 0.2618 0.2366 0.2107 0.1887 0.1697 0.1533
0.06      0.3452 0.3061 0.2754 0.2499 0.2227 0.1997 0.1798 0.1627
0.49      0.6042 0.5562 0.5147 0.4769 0.4387 0.4032 0.3704 0.3405
0.50      0.6092 0.5606 0.5188 0.4808 0.4424 0.4067 0.3738 0.3436
0.51      0.6142 0.5650 0.5229 0.4847 0.4461 0.4102 0.3770 0.3468
0.89      0.7937 -0.1000 0.7123 0.6672 0.6235 0.5812 0.5406 0.5022
0.90      0.8044 0.7566 0.7207 0.6755 0.6313 0.5890 0.5481 0.5095
0.91      0.8157 0.7671 0.7296 0.6844 0.6401 0.5975 0.5563 0.5173
0.94      0.8539 0.8035 0.7569 0.7161 0.6714 0.6276 0.5856 0.5456
0.95      0.8687 0.8180 0.7713 0.7292 0.6844 0.6403 0.5980 0.5575
0.96      -0.1000 0.8345 0.7878 0.7444 0.6995 0.6553 0.6124 0.5715

```

```

* S.SIZE= 8      " Ramp case"      AMU= .60(i.e. PO= 0.27425) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 18.59 26.56 34.37 41.72 48.38 54.17 59.01 62.89 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      -0.1000 0.2290 0.1989 0.1755 0.1555 0.1381 0.1255 0.1105
0.02      0.2933 0.2642 0.2420 0.2133 0.1895 0.1696 0.1521 0.1371
0.03      0.3277 0.2924 0.2637 0.2386 0.2126 0.1905 0.1713 0.1548
0.04      0.3551 0.3146 0.2835 0.2556 0.2302 0.2066 0.1862 0.1685
0.05      -0.1000 0.3332 0.2999 0.2708 0.2448 0.2200 0.1985 0.1799
0.06      -0.1000 0.3494 0.3141 0.2839 0.2564 0.2316 0.2092 0.1898
0.49      0.6256 0.5990 0.5557 0.5153 0.4772 0.4402 0.4057 0.3740
0.50      0.6306 0.6034 0.5598 0.5192 0.4809 0.4437 0.4091 0.3772
0.51      0.6357 0.6077 0.5638 0.5231 0.4846 0.4473 0.4125 0.3804
0.89      0.8363 0.7880 0.7494 0.7049 0.6612 0.6185 0.5771 0.5377
0.90      0.8459 0.7971 0.7523 0.7130 0.6691 0.6261 0.5847 0.5450
0.91      0.8561 0.8068 0.7617 0.7216 0.6777 0.6345 0.5928 0.5528
0.94      -0.1000 0.8401 0.7947 0.7501 0.7082 0.6645 0.6220 0.5811
0.95      -0.1000 0.8533 0.8081 0.7634 0.7208 0.6770 0.6342 0.5930
0.96      0.8826 0.8679 0.8233 0.7788 0.7355 0.6916 0.6485 0.6069

```

```

* S.SIZE= 8      " Ramp case"      AMU= .70(i.e. PO= 0.24196) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 17.88 25.80 33.73 41.35 48.38 54.62 59.94 64.30 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      0.2675 0.2602 0.2380 0.2100 0.1869 0.1670 0.1497 0.1349
0.02      0.3423 0.3048 0.2753 -0.1000 0.2232 0.2004 0.1805 0.1632
0.03      -0.1000 0.3352 0.3021 0.2732 0.2473 0.2223 0.2008 0.1820
0.04      0.3804 0.3588 0.3228 0.2922 0.2645 0.2393 0.2164 0.1964
0.05      0.4003 -0.1000 0.3400 0.3080 0.2792 0.2529 0.2293 0.2084
0.06      0.4177 0.3840 0.3548 0.3215 0.2918 0.2648 0.2404 0.2187
0.49      0.6724 0.6307 0.5961 0.5549 0.5154 0.4777 0.4417 0.4084
0.50      0.6773 0.6350 0.6002 0.5588 0.5191 0.4812 0.4452 0.4116
0.51      0.6822 0.6394 0.6042 0.5626 0.5228 0.4848 0.4486 0.4149
0.89      -0.1000 0.8254 0.7814 0.7411 0.6980 0.6552 0.6135 0.5733
0.90      -0.1000 0.8337 0.7897 0.7489 0.7057 0.6628 0.6210 0.5806
0.91      -0.1000 0.8426 0.7985 0.7551 0.7140 0.6711 0.6289 0.5883
0.94      0.8863 0.8729 0.8292 0.7860 0.7436 0.7005 0.6578 0.6164
0.95      0.9049 -0.1000 0.8416 0.7986 0.7552 0.7127 0.6699 0.6282
0.96      0.9253 0.8805 0.8556 0.8131 0.7698 0.7269 0.6840 0.6420

```

*****TEST CRITERION 'T'*****
 P1 x 100: 13.86 20.89 28.51 36.43 44.38 51.98 59.01 65.25 *
 * SCALEX100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
 * GMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
 * S.SIZE= 8 " Ramp case" AMU=1.1041.e. PU=0.135673 *
 0.01 0.4568 0.4205 0.3897 0.3602 0.3294 0.3012 0.2751 0.2514
 -0.1000 0.4686 0.4330 0.4008 0.3696 0.3391 0.3109 0.2851
 0.02 0.5198-0.1000 0.4612 0.4271 0.3946 0.3635 0.3340 0.3069
 0.04 0.5446 0.5117 0.4828 0.4471 0.4137 0.3817 0.3515 0.3235
 0.05 0.5654 0.5293-0.1000 0.4835 0.4294 0.3667 0.3058 0.2487
 0.06 0.5835 0.5445 0.5105 0.4776 0.4427 0.4095 0.3780 0.3487
 0.49 0.8083 0.7705 0.7429 0.7036 0.6648 0.6259 0.5875 0.5500
 0.50 0.8129 0.7746 0.7465 0.7071 0.6683 0.6294 0.5909 0.5533
 0.51 0.8175 0.7786-0.1000 0.7107 0.6718 0.6328 0.5943 0.5566
 0.90 0.9803 0.9389 0.9025 0.8733 0.8361 0.7974 0.7576 0.7175
 0.91 0.9887 0.9468 0.9103-0.1000 0.8431 0.8046 0.7649 0.7248
 0.94 -0.1000 0.9729 0.9369 0.9011 0.8677 0.8301 0.7908 0.7507
 0.95 -0.1000 0.9827 0.9472 0.9119 0.8753 0.8405 0.8015 0.7614
 0.96 -0.1000 0.9932 0.9585 0.9240 0.8877 0.8525 0.8138 0.7739

*****TEST CRITERION 'T'*****
 P1 x 100: 14.99 22.34 30.15 38.12 45.93 53.28 59.94 65.73 *
 * SCALEX100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
 * GMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
 * S.SIZE= 8 " Ramp case" AMU=1.1041.e. PU=0.158663 *
 0.01 0.4087 0.3794 0.3523 0.3206 0.2920 0.2655 0.2414 0.2198
 0.02 0.4634 0.4250 0.3929 0.3627 0.3343 0.3026 0.2763 0.2525
 0.04 0.4999 0.4555 0.4204 0.3879 0.3567 0.3266 0.2989 0.2737
 -0.1000 0.4790 0.4415 0.4078 0.3755 0.3447 0.3160 0.2898
 0.05 0.5197 0.4983 0.4588 0.4240 0.3910 0.3597 0.3301 0.3031
 0.06 0.5369 0.5038 0.4737 0.4379 0.4043 0.3724 0.3422 0.3145
 0.49 0.7674 0.7496 0.7074 0.6678 0.6285 0.5898 0.5514 0.5145
 0.50 0.7723-0.1000 0.7112 0.6715 0.6321 0.5933 0.5548 0.5178
 0.51 0.7771-0.1000 0.7149 0.6752 0.6358 0.5968 0.5583 0.5211
 0.89 0.9407 0.9005-0.1000 0.8386 0.7992 0.7598 0.7183 0.6778
 0.90 0.9500 0.9091-0.1000 0.8054 0.8053 0.7659 0.7253 0.6846
 0.91 0.9597 0.9181 0.8803 0.8527 0.8137 0.7735 0.7328 0.6920
 0.94 0.9911 0.9482 0.9102-0.1000 0.8400 0.8003 0.7596 0.7187
 0.95 -0.1000 0.9596 0.9219 0.8840 0.8507 0.8113 0.7707 0.7298
 0.96 -0.1000 0.9721 0.9349 0.8976 0.8629 0.8240 0.7836 0.7427

*****TEST CRITERION 'T'*****
 P1 x 100: 16.05 23.67 31.59 39.52 47.17 54.17 60.41 65.73 *
 * SCALEX100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
 * GMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
 * S.SIZE= 8 " Ramp case" AMU=.9011.e. PU=0.184063 *
 0.01 -0.1000 0.3442 0.3111 0.2824 0.2557 0.2312 0.2090 0.1897
 0.02 0.4147 0.3835 0.3556 0.3231 0.2940 0.2672 0.2429 0.2211
 0.04 0.4764 0.4349 0.4010 0.3701 0.3377 0.3084 0.2815 0.2573
 0.05 0.4987 0.4536 0.4179 0.3849 0.3533 0.3230 0.2953 0.2702
 -0.1000 0.4698 0.4325 0.3986 0.3666 0.3355 0.3071 0.2813
 -0.1000 0.2715 0.2703 0.2673 0.2605 0.2591 0.2527 0.2479 0.2489
 -0.1000 0.2715 0.2715 0.2715 0.2715 0.2715 0.2715 0.2715 0.2715
 0.49 0.7156 0.6742 0.6343 0.5956 0.5583 0.5149 0.4789
 0.50 0.7220 0.6762 0.6356 0.5978 0.5576 0.5188 0.4817 0.4467
 0.51 0.7268 0.6805 0.6396 0.6016 0.5613 0.5223 0.4851 0.4500
 -0.1000 0.8590 0.8163 0.7742 0.7334 0.6911 0.6493 0.6086
 -0.1000 0.8665 0.8240 0.7820 0.7405 0.6986 0.6567 0.6158
 0.90 0.8852-0.1000 0.8322 0.7903 0.7490 0.7066 0.6646 0.6236
 0.91 0.9144 0.8754 0.8352 0.8151 0.7741 0.7331 0.6915 0.6506
 0.94 0.9620 0.9189 0.8792 0.8500 0.8092 0.7684 0.7269 0.6855
 0.95 0.9757 0.9321 0.8923 0.8609 0.8212 0.7800 0.7384 0.6969
 0.96 0.9905 0.9467 0.9071 0.8736 0.8343 0.7924 0.7517 0.7102

*****TEST CRITERION 'T'*****
 P1 x 100: 17.02 24.83 32.80 40.81 47.96 54.62 60.41 65.25 *
 * SCALEX100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
 * GMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
 * S.SIZE= 8 " Ramp case" AMU=.8011.e. PU=0.211863 *
 0.01 0.3562 0.3005 0.2720 0.2472 0.2207 0.1981 0.1784 0.1612
 -0.1000 0.3487 0.3144 0.2850 0.2579 0.2332 0.2108 0.1913
 0.02 0.4015 0.3625 0.3107 0.2820 0.2558 0.2320 0.2110
 0.04 0.4267 0.3926 0.3542 0.3104 0.3005 0.2873 0.2671
 0.05 0.4480 0.4105 0.3777 0.3467 0.3156 0.2873 0.2616 0.2386
 0.06 0.4667 0.4261 0.3920 0.3607 0.3286 0.2995 0.2731 0.2493
 0.49 0.7173 0.6720 0.6316 0.5939 0.5539 0.5152 0.4782 0.4434
 0.50 0.7220 0.6762 0.6356 0.5978 0.5576 0.5188 0.4817 0.4467
 0.51 0.7268 0.6805 0.6396 0.6016 0.5613 0.5223 0.4851 0.4500
 -0.1000 0.8590 0.8163 0.7742 0.7334 0.6911 0.6493 0.6086
 -0.1000 0.8665 0.8240 0.7820 0.7405 0.6986 0.6567 0.6158
 0.90 0.8852-0.1000 0.8322 0.7903 0.7490 0.7066 0.6646 0.6236
 0.91 0.9144 0.8754 0.8352 0.8151 0.7741 0.7331 0.6915 0.6506
 0.94 0.9620 0.9189 0.8792 0.8500 0.8092 0.7684 0.7269 0.6855
 0.95 0.9757 0.9321 0.8923 0.8609 0.8212 0.7800 0.7384 0.6969
 0.96 0.9910 0.9467 0.9071 0.8736 0.8343 0.7924 0.7517 0.7102

```
* S.SIZE= 8      " Ramp case"      AMU=1.20(i.e. PO= 0.11507) *  
*****  
* GMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *  
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *  
* P1 x 100:   12.69  19.35  26.70  34.51  42.45  50.28  57.64  64.50 *  
*****  
PEQ < T ]      .....TEST CRITERION ,T .....  
0.01      -0.1000 0.4637 0.4295 0.3981 0.3678 0.3377 0.3099 0.2844  
0.02      0.5314 0.5018 0.4740 0.4398 0.4074 0.3761 0.3465 0.3189  
0.03      0.5649 0.5302 -0.1000 0.4665 0.4329 0.4006 0.3699 0.3411  
0.04      0.5912 0.5521 0.5187 0.4867 0.4521 0.4191 0.3876 0.3580  
0.05      0.6131 0.5702 0.5353 0.5016 0.4678 0.4342 0.4020 0.3718  
0.06      -0.1000 0.5858 0.5495 0.5152 0.4812 0.4470 0.4144 0.3836  
0.49      0.8464 0.8054 0.7698 0.7377 0.6996 0.6613 0.6230 0.5851  
0.50      0.8508 0.8093 0.7734 0.7411 0.7030 0.6647 0.6262 0.5884  
0.51      0.8552 0.8131 0.7771 0.7446 0.7064 0.6680 0.6296 0.5916  
0.89      0.9993 0.9576 0.9226 0.8880 0.8574 0.8205 0.7820 0.7427  
0.90      -0.1000 0.9643 0.9293 0.8949 0.8636 0.8269 0.7885 0.7492  
0.91      -0.1000 0.9712 0.9363 0.9020 0.8702 0.8337 0.7955 0.7562  
0.94      -0.1000 0.9936 0.9597 0.9265 0.8948 0.8577 0.8202 0.7813  
0.95      -0.1000-0.1000 0.9686 0.9361 0.9049 0.8675 0.8303 0.7916  
0.96      -0.1000-0.1000 0.9783 0.9467 0.9153 0.8777 0.8420 0.8036
```

```
* S.SIZE= 8      " Ramp case"      AMU=1.30(i.e. PO= 0.09680) *  
*****  
* GMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *  
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *  
* P1 x 100:   11.51  17.75  24.78  32.39  40.32  48.25  55.86  62.89 *  
*****  
PEQ < T ]      .....TEST CRITERION ,T .....  
0.01      0.5241-0.1000 0.4702 0.4371 0.4055 0.3750 0.3456 0.3183  
0.02      0.5769 0.5413 0.5101 0.4791 0.4456 0.4135 0.3826 0.3535  
0.03      0.6126 0.5706 0.5369 0.5042 0.4712 0.4381 0.4062 0.3761  
0.04      -0.1000 0.5931 0.5573 0.5237 0.4905 0.4566 0.4240 0.3931  
0.05      0.7500 0.6117 0.5740 0.5396 0.5055 0.4717 0.4386 0.4070  
0.06      0.6419-0.1000 0.5882 0.5531 0.5187 0.4845 0.4509 0.4189  
0.49      -0.1000 0.8379 0.8020 0.7671 0.7329 0.6953 0.6574 0.6196  
0.50      -0.1000 0.8415 0.8054 0.7705 0.7362 0.6986 0.6607 0.6228  
0.51      -0.1000 0.8451 0.8088 0.7739 0.7395 0.7019 0.6639 0.6260  
0.89      -0.1000 0.9802 0.9465 0.9141 0.8802 0.8481 0.8113 0.7731  
0.90      -0.1000 0.9860 0.9525 0.9202 0.8866 0.8542 0.8175 0.7795  
0.91      -0.1000 0.9919 0.9586 0.9266 0.8933 0.8606 0.8242 0.7862  
0.94      -0.1000-0.1000 0.9789 0.9484 0.9164 0.8820 0.8476 0.8102  
0.95      -0.1000-0.1000 0.9865 0.9568 0.9255 0.8917 0.8571 0.8201  
0.96      -0.1000-0.1000 0.9947 0.9661 0.9357 0.9027 0.8681 0.8315
```

```
* S.SIZE= 8      " Ramp case"      AMU=1.40(i.e. PO= 0.08076) *  
*****  
* GMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *  
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *  
* P1 x 100:   10.33  16.12  22.78  30.13  37.94  45.91  53.72  61.07 *  
*****  
PEQ < T ]      .....TEST CRITERION ,T .....  
0.01      0.5685 0.5356 0.5062 0.4762 0.4436 0.4122 0.3812 0.3530  
0.02      0.6242 0.5816 0.5481 0.5161 0.4833 0.4508 0.4190 0.3886  
0.03      -0.1000 0.6119 0.5751 0.5418 0.5086 0.4754 0.4427 0.4114  
0.04      0.6467-0.1000 0.5956 0.5612 0.5275 0.4939 0.4605 0.4285  
0.05      0.6663 0.6367 0.6124 0.5770 0.5428 0.5087 0.4751 0.4425  
0.06      0.6833 0.6510-0.1000 0.5904 0.5558 0.5214 0.4874 0.4544  
0.49      -0.1000 0.8681 0.8317 0.7978 0.7631 0.7279 0.6907 0.6532  
0.50      -0.1000 0.8717 0.8350 0.8010 0.7664 0.7311 0.6939 0.6564  
0.51      -0.1000-0.1000 0.8382 0.8042 0.7696 0.7343 0.6971 0.6595  
0.89      -0.1000 0.9995 0.9670 0.9367 0.9053 0.8736 0.8387 0.8020  
0.90      -0.1000-0.1000 0.9722 0.9422 0.9110 0.8778 0.8446 0.8081  
0.91      -0.1000-0.1000 0.9776 0.9479 0.9171 0.8841 0.8509 0.8145  
0.94      -0.1000-0.1000 0.9950 0.9670 0.9378 0.9062 0.8729 0.8373  
0.95      -0.1000-0.1000-0.1000 0.9743 0.9459 0.9150 0.8814 0.8467  
0.96      -0.1000-0.1000-0.1000 0.9823 0.9549 0.9249 0.8920 0.8574
```

```
* S.SIZE= 8      " Ramp case"      AMU=1.50(i.e. PO= 0.06681) *  
*****  
* GMIN x100: 50.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *  
* SCALEx100: 0.5000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *  
* P1 x 100:    9.18  14.50  20.74  27.78  35.39  43.32  51.25  58.86 *  
*****  
PEQ < T ]      .....TEST CRITERION ,T .....  
0.01      0.6221 0.5752 0.5435 0.5129 0.4816 0.4494 0.4182 0.3882  
0.02      0.6570 0.6227 0.5859 0.5531 0.5207 0.4880 0.4554 0.4241  
0.03      0.6826 0.6356 0.6132 0.5787 0.5455 0.5122 0.4791 0.4469  
0.04      0.7037 0.6559 0.6269 0.5979 0.5641 0.5304 0.4969 0.4640  
0.05      0.7219 0.6727 0.6425 0.6136 0.5792 0.5451 0.5112 0.4780  
0.06      0.7379 0.6872 0.6558-0.1000 0.5920 0.5576 0.5234 0.4899  
0.49      -0.1000-0.1000 0.8593 0.8262 0.7930 0.7583 0.7227 0.6858  
0.50      -0.1000-0.1000 0.8624 0.8292 0.7960 0.7614 0.7257 0.6889  
0.51      -0.1000-0.1000 0.8654 0.8323 0.7991 0.7645 0.7288 0.6919  
0.89      -0.1000-0.1000 0.9846 0.9563 0.9273 0.8962 0.8640 0.8291  
0.90      -0.1000-0.1000 0.9891 0.9611 0.9325 0.9017 0.8696 0.8349  
0.91      -0.1000-0.1000 0.9937 0.9661 0.9379 0.9075 0.8750 0.8410  
0.94      -0.1000-0.1000-0.1000 0.9827 0.9563 0.9275 0.8960 0.8625  
0.95      -0.1000-0.1000-0.1000 0.9890 0.9634 0.9354 0.9045 0.8713  
0.96      -0.1000-0.1000-0.1000 0.9957 0.9713 0.9443 0.9142 0.8812
```

```

* S.SIZE= 8      " Ramp case"      AMU=1.67(i.e. PO= 0.09420) *
*****
* QMIN x100:50.000050.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 0.5000 0.5000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100:   8.09 12.93 16.72 25.37 32.77 40.54 48.50 56.31 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      0.6491 0.6184 0.5808 0.5494 0.5121 0.4864 0.4545 0.4236
0.02      0.6883 0.6547 0.6235 0.5894 0.5569 0.5243 0.4916 0.4595
0.03      0.7172 0.6789 0.6422 0.6149 0.5814 0.5482 0.5150 0.4822
0.04      0.7404 0.6981 0.6611 0.6310 0.5998 0.5662 0.5325 0.4993
0.05      0.7556 0.7142 0.6765 0.6458 0.6146 0.5807 0.5468 0.5132
0.06      0.7663 0.7281 0.6896 0.6583 0.6262 0.5930 0.5588 0.5249
0.49      -0.1000 0.9283-0.1000 0.8524 0.8206 0.7875 0.7528 0.7171
0.50      -0.1000 0.9318-0.1000 0.8553 0.8235 0.7905 0.7558 0.7200
0.51      -0.1000 0.9353-0.1000 0.8582 0.8264 0.7934 0.7587 0.7230
0.89      -0.1000-0.1000 0.9996 0.9730 0.9464 0.9179 0.8868 0.8544
0.90      -0.1000-0.1000-0.1000 0.9773 0.9511 0.9229 0.8922 0.8598
0.91      -0.1000-0.1000-0.1000 0.9817 0.9559 0.9282 0.8978 0.8655
0.94      -0.1000-0.1000-0.1000 0.9959 0.9721 0.9461 0.9172 0.8856
0.95      -0.1000-0.1000-0.1000-0.1000 0.9723 0.9531 0.9250 0.8939
0.96      -0.1000-0.1000-0.1000-0.1000 0.9850 0.9609 0.9337 0.9034

```

```

* S.SIZE= 8      " Ramp case"      AMU=1.70(i.e. PO= 0.04457) *
*****
* QMIN x100:50.000050.000050.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100:   7.05 11.41 16.73 22.97 30.00 37.62 45.54 53.47 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      0.6783 0.6481 0.6190 0.5853 0.5540 0.5224 0.4905 0.4589
0.02      0.7234 0.6855 0.6554-0.1000 0.5923 0.5598 0.5271 0.4947
0.03      0.7526 0.7113 0.6789 0.6462 0.6164 0.5834 0.5502 0.5172
0.04      0.7667 0.7314 0.6969 0.6641 0.6332 0.6010 0.5675 0.5341
0.05      0.7795 0.7480 0.7118 0.6786 0.6474 0.6152 0.5815 0.5478
0.06      0.7912 0.7588 0.7245 0.6909 0.6595 0.6269 0.5933 0.5594
0.49      0.9464-0.1000 0.9121-0.1000 0.8461 0.8147 0.7815 0.7469
0.50      0.9506-0.1000 0.9152-0.1000 0.8489 0.8175 0.7844 0.7498
0.51      0.9548-0.1000 0.9182-0.1000 0.8516 0.8203 0.7872 0.7525
0.89      -0.1000-0.1000-0.1000 0.9874 0.9630 0.9370 0.9084 0.8772
0.90      -0.1000-0.1000-0.1000 0.9911 0.9671 0.9415 0.9133 0.8824
0.91      -0.1000-0.1000-0.1000 0.9949 0.9713 0.9462 0.9184 0.8879
0.94      -0.1000-0.1000-0.1000-0.1000 0.9854 0.9621 0.9360 0.9069
0.95      -0.1000-0.1000-0.1000-0.1000 0.9907 0.9683 0.9430 0.9145
0.96      -0.1000-0.1000-0.1000-0.1000 0.9964 0.9751 0.9508 0.9232

```

```

* S.SIZE= 8      " Ramp case"      AMU=1.80(i.e. PO= 0.03593) *
*****
* QMIN x100:50.000050.000050.000050.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100:   6.09  9.97 14.81 20.60 27.26 34.62 42.42 50.39 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      0.7118 0.6774 0.6496 0.6210 0.5889 0.5575 0.5257 0.4939
0.02      0.7556 0.7177 0.6860 0.6569 0.6254 0.5943 0.5619 0.5293
0.03      0.7740 0.7449 0.7100 0.6797 0.6435 0.6174 0.5846 0.5516
0.04      0.7900 0.7604 0.7283 0.6970 0.6656 0.6342 0.6015 0.5682
0.05      0.8041 0.7725 0.7433 0.7110 0.6795 0.6479 0.6152 0.5817
0.06      0.8150 0.7834 0.7549 0.7229 0.6912 0.6595 0.6267 0.5931
0.49      0.9741 0.9401 0.9342 0.9010 0.8697 0.8398 0.8083 0.7751
0.50      0.9781 0.9434 0.9370 0.9038 0.8723 0.8425 0.8110 0.7778
0.51      0.9820 0.9466-0.1000 0.9066 0.8749 0.8451 0.8137 0.7805
0.89      -0.1000-0.1000-0.1000 0.9997 0.9772 0.9536 0.9276 0.8988
0.90      -0.1000-0.1000-0.1000-0.1000 0.9808 0.9576 0.9320 0.9035
0.91      -0.1000-0.1000-0.1000-0.1000 0.9845 0.9618 0.9366 0.9086
0.94      -0.1000-0.1000-0.1000-0.1000 0.9966 0.9758 0.9525 0.9260
0.95      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9811 0.9586 0.9329
0.96      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9870 0.9655 0.9407

```

```

* S.SIZE= 8      " Ramp case"      AMU=1.90(i.e. PO= 0.02872) *
*****
* QMIN x100:50.000050.000050.000050.000050.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 1.0000 1.0000 1.0000 *
* P1 x 100:   5.20  8.64 12.99 18.31 24.55 31.59 39.20 47.13 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      0.7498 0.7086 0.6793 0.6519 0.6231 0.5916 0.5601 0.5283
0.02      0.7758 0.7506 0.7167 0.7500 0.6583 0.6272 0.5956 0.5632
0.03      0.7969 0.7687 0.7411 0.7100 0.6805 0.6495 0.6178 0.5851
0.04      0.8132 0.7836 0.7573 0.7271 0.6970 0.6661 0.6342 0.6014
0.05      0.8290 0.7964 0.7693 0.7410 0.7104 0.6794 0.6475 0.6146
0.06      0.8429 0.8078 0.7797 0.7524 0.7218 0.6907 0.6587 0.6257
0.49      0.9999 0.9617-0.1000 0.9220 0.8923 0.8630 0.8332 0.8016
0.50      -0.1000 0.9647 0.9376 0.9246 0.8949 0.8655 0.8358 0.8042
0.51      -0.1000 0.9677 0.9403 0.9271 0.8975 0.8679 0.8383 0.8068
0.89      -0.1000-0.1000-0.1000-0.1000 0.9893 0.9679 0.9444 0.9181
0.90      -0.1000-0.1000-0.1000-0.1000 0.9924 0.9715 0.9484 0.9224
0.91      -0.1000-0.1000-0.1000-0.1000 0.9956 0.9752 0.9525 0.9270
0.94      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9873 0.9666 0.9428
0.95      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9919 0.9720 0.9490
0.96      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9968 0.9781 0.9560

```



```

* S.SIZE= 8 " Ramp case" AMU=2.10(i.e. PD= 0.02275) *
*****
* QMIN x100:50.000050.000050.000050.000050.000050.000050.000050.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 1.0000 *
* P1 x 100: 4.41 7.41 11.29 15.13 21.92 28.52 35.93 43.74 *
*****
PEQ < T] .....TEST CRITERION ,T .....
0.01 0.7668 0.7476 0.7092 0.6816 0.6541 0.6275 0.5937 0.5619
0.02 0.7977 0.7716 0.7475 0.7170 0.6885 0.6591 0.6282 0.5961
0.03 0.8204 0.7912 0.7664 0.7395 0.7102 0.6806 0.6497 0.6176
0.04 0.8405 0.8071 0.7809 0.7555 0.7263 0.6966 0.6657 0.6334
0.05 0.8575 0.8201 0.7932 0.7674 0.7394 0.7095 0.6785 0.6463
0.06 0.8726 0.8320 0.8037 0.7776 0.7504 0.7203 0.6894 0.6571
0.49 -0.1000 0.9815 0.9534-0.1000 0.9127 0.8847 0.8564 0.8263
0.50 -0.1000 0.9844 0.9560-0.1000 0.9150 0.8871 0.8588 0.8287
0.51 -0.1000 0.9872 0.9585-0.1000 0.9174 0.8895 0.8612 0.8312
0.89 -0.1000-0.1000-0.1000-0.1000 0.9997 0.9802 0.9591 0.9352
0.90 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9833 0.9626 0.9391
0.91 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9866 0.9663 0.9433
0.94 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9970 0.9787 0.9575
0.95 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9834 0.9630
0.96 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9885 0.9692

```

```

* S.SIZE= 8 " Ramp case" AMU=2.10(i.e. PD= 0.01756) *
*****
* QMIN x100:50.000050.000050.000050.000050.000050.000050.000050.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 3.69 6.29 9.72 14.08 19.40 25.64 32.67 40.29 *
*****
PEQ < T] .....TEST CRITERION ,T .....
0.01 0.7860 0.7639 0.7454 0.7186 0.6836 0.6556 0.6258 0.5947
0.02 0.8213 0.7931 0.7701 0.7459 0.7172 0.6889 0.6592 0.6280
0.03 0.8481 0.8139 0.7891 0.7652 0.7386 0.7098 0.6800 0.6488
0.04 0.8697 0.8308 0.8040 0.7796 0.7540 0.7253 0.6954 0.6643
0.05 0.8765 0.8450 0.8163 0.7914 0.7658 0.7378 0.7079 0.6767
0.06 0.8840 0.8573 0.8270 0.8015 0.7758 0.7483 0.7184 0.6872
0.49 -0.1000 0.9999 0.9702 0.9467 0.9305 0.9046 0.8774 0.8492
0.50 -0.1000-0.1000 0.9726 0.9490 0.9326 0.9069 0.8797 0.8516
0.51 -0.1000-0.1000 0.9749 0.9512 0.9348 0.9091 0.8820 0.8539
0.89 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9907 0.9717 0.9502
0.90 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9934 0.9748 0.9538
0.91 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9962 0.9781 0.9575
0.94 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9888 0.9701
0.95 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9929 0.9750
0.96 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9972 0.9804

```

```

* S.SIZE= 8 " Ramp case" AMU=2.20(i.e. PD= 0.01390) *
*****
* QMIN x100:50.000050.000050.000050.000050.000050.000050.000050.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 3.07 5.29 8.29 12.18 17.02 22.21 28.46 36.82 *
*****
PEQ < T] .....TEST CRITERION ,T .....
0.01 0.8080 0.7833 0.7630 0.7441 0.7119 0.6748 0.6563 0.6261
0.02 0.8487 0.8153 0.7918 0.7696 0.7451 0.7172 0.6886 0.6585
0.03 -0.1000 0.8381 0.8115 0.7882 0.7643 0.7375 0.7087 0.6786
0.04 0.8816 0.8558 0.8267 0.8025 0.7784 0.7524 0.7237 0.6936
0.05 0.8913 0.8706 0.8393 0.8141 0.7899 0.7640 0.7357 0.7056
0.06 0.9001 0.8778 0.8501 0.8241 0.7996 0.7738 0.7458 0.7157
0.49 -0.1000-0.1000 0.9856 0.9619 0.9406 0.9222 0.8971 0.8702
0.50 -0.1000-0.1000 0.9878 0.9640 0.9426 0.9243 0.8992 0.8724
0.51 -0.1000-0.1000 0.9900 0.9660 0.9447 0.9263 0.9014 0.8747
0.89 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9998 0.9826 0.9634
0.90 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9853 0.9665
0.91 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9881 0.9698
0.94 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9974 0.9809
0.95 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9851
0.96 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9897

```

```

* S.SIZE= 8 " Ramp case" AMU=2.30(i.e. PD= 0.01072) *
*****
* QMIN x100:75.000050.000050.000050.000050.000050.000050.000050.0000 *
* SCALEx100: 0.2500 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 2.52 4.41 7.00 10.43 14.79 20.11 26.35 33.39 *
*****
PEQ < T] .....TEST CRITERION ,T .....
0.01 0.8418 0.8042 0.7832 0.7631 0.7432 0.7126 0.6852 0.6561
0.02 0.8761 0.8392 0.8134 0.7915 0.7692 0.7441 0.7165 0.7500
0.03 0.8880 0.8632 0.8337 0.8103 0.7875 0.7630 0.7359 0.7069
0.04 0.8986 0.8772 0.8493 0.8244 0.8013 0.7769 0.7503 0.7214
0.05 0.9085 0.8846 0.8621 0.8360 0.8124 0.7881 0.7617 0.7330
0.06 0.9177 0.8922 0.8732 0.8459 0.8218 0.7975 0.7712 0.7427
0.49 -0.1000-0.1000 1.0000 0.9756 0.9549-0.1000 0.9146 0.8896
0.50 -0.1000-0.1000-0.1000 0.9776 0.9568-0.1000 0.9166 0.8917
0.51 -0.1000-0.1000-0.1000 0.9795 0.9587 0.9384 0.9186 0.8938
0.89 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9918 0.9747
0.90 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9942 0.9775
0.91 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9967 0.9804
0.94 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9900
0.95 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9936
0.96 -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9975

```



```

* S.SIZE= 8      " Ramp case"      AMU=2.80(i.e. PO=(.00256) *
*****
* GMIN x100:75.000075.000075.000075.000075.000075.000075.000050.000050.0000 *
* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.5000 0.5000 *
* P1 x 100:   0.82   1.53   2.62   4.20   6.47   9.42  13.31  18.15 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      0.9037 0.8912 0.8810 0.8697 0.8480 0.8242 0.8045 0.7828
0.02      0.9293 0.9108 0.8975 0.8854 0.8738 0.8496 0.8295 0.8081
0.03      0.9502 0.9262 0.9104 0.8971 0.8833 0.8654 0.8449 0.8237
0.04      0.9675 0.9389 0.9211 0.9066 0.8925 0.8768 0.8564 0.8351
0.05      -0.1000 0.9499 0.9302 0.9147 0.9002 0.8845 0.8655 0.8443
0.06      0.9691 0.9596 0.9380 0.9218 0.9069 0.8912 0.8732 0.8520
0.49      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9914 0.9753 0.9594
0.50      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9927 0.9767 0.9603
0.51      -0.1000-0.1000-0.1000-0.1000-0.1000 0.9940 0.9780 0.9621
0.89      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.90      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.91      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.94      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.95      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.96      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000

```

```

* S.SIZE= 8      " Ramp case"      AMU=2.90(i.e. PO= 0.00187) *
*****
* GMIN x100:87.500075.000075.000075.000075.000075.000075.000050.0000 *
* SCALEx100: 0.1250 0.2500 0.2500 0.2500 0.2500 0.2500 0.5000 0.5000 *
* P1 x 100:   0.63   1.20   2.09   3.41   5.29   7.89  11.32  15.68 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      0.9137 0.8995 0.8892 0.8793 0.8661 0.8464 0.8234 0.8031
0.02      0.9434 0.9216 0.9075 0.8957 0.8835 0.8709 0.8475 0.8273
0.03      0.9662 0.9383 0.9213 0.9079 0.8951 0.8809 0.8624 0.8422
0.04      -0.1000 0.9520 0.9325 0.9178 0.9043 0.8901 0.8735 0.8531
0.05      -0.1000 0.9636 0.9419 0.9260 0.9120 0.8977 0.8814 0.8619
0.06      0.9943-0.1000 0.9501 0.9332 0.9187 0.9042 0.8881 0.8692
0.49      -0.1000-0.1000-0.1000-0.1000-0.1000 1.0000 0.9842 0.9692
0.50      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9855 0.9704
0.51      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9867 0.9717
0.89      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.90      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.91      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.94      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.95      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.96      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000

```

```

* S.SIZE= 8      " Ramp case"      AMU=3.00(i.e. PO= 0.00135) *
*****
* GMIN x100:87.500087.500075.000075.000075.000075.000075.000075.0000 *
* SCALEx100: 0.1250 0.1250 0.2500 0.2500 0.2500 0.2500 0.5000 0.5000 *
* P1 x 100:   0.49   0.94   1.65   2.74   4.32   6.55   9.55  13.43 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      0.9250 0.9086 0.8976 0.8880 0.8776 0.8633 0.8446 0.8220
0.02      0.9585 0.9332 0.9177 0.9057 0.8942 0.8815 0.8675 0.8451
0.03      0.9832 0.9514 0.9324 0.9185 0.9061 0.8932 0.8783 0.8593
0.04      -0.1000 0.9659 0.9440 0.9286 0.9154 0.9022 0.8875 0.8698
0.05      -0.1000 0.9780 0.9538 0.9370 0.9231 0.9096 0.8949 0.8780
0.06      -0.1000-0.1000 0.9622 0.9442 0.9297 0.9159 0.9013 0.8846
0.49      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9924 0.9779
0.50      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9936 0.9791
0.51      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9947 0.9803
0.89      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.90      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.91      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.94      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.95      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.96      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000

```

```

* S.SIZE= 8      " Ramp case"      AMU=3.10(i.e. PO= 0.00097) *
*****
* GMIN x100:87.500087.500087.500075.000075.000075.000075.000075.0000 *
* SCALEx100: 0.1250 0.1250 0.1250 0.2500 0.2500 0.2500 0.5000 0.5000 *
* P1 x 100:   0.37   0.72   1.29   2.18   3.50   5.38   7.98  11.41 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      0.9531 0.9186 0.9219 0.8967 0.8871 0.8757 0.8608 0.8425
0.02      0.9751 0.9458 0.9284 0.9156 0.9045 0.8929 0.8794 0.8642
0.03      -0.1000 0.9651 0.9439 0.9289 0.9166 0.9045 0.8911 0.8752
0.04      -0.1000 0.9803 0.9560 0.9393 0.9259 0.9134 0.8999 0.8845
0.05      -0.1000-0.1000 0.9660 0.9478 0.9336 0.9206 0.9071 0.8919
0.06      -0.1000 0.9959 0.9746 0.9551 0.9401 0.9268 0.9132 0.8981
0.49      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 1.0000 0.9859
0.50      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9870
0.51      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000 0.9881
0.89      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.90      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.91      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.94      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.95      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000
0.96      -0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000-0.1000

```



```
*****
* S.SIZE= 16
* Ramp case" AMU= .50(1.e. PO= 0.30854) *
*****
* GMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 19.15 27.07 36.69 41.72 47.96 53.28 57.64 61.07 *
*****
PEQ < T]
*****TEST CRITERION / T *****
0.01 0.3264 0.2958 0.2663 0.2393 0.2149 0.1932 0.1742 0.1578
0.02 0.3589 0.3258 0.2949 0.2662 0.2399 0.2164 0.1957 0.1777
0.04 0.3935 0.3599 0.3272 0.2966 0.2685 0.2431 0.2205 0.2006
0.05 0.4065 0.3720 0.3386 0.3074 0.2786 0.2526 0.2293 0.2088
0.06 0.4172 0.3819 0.3483 0.3166 0.2873 0.2607 0.2369 0.2158
0.07 0.4268 0.3908 0.3568 0.3248 0.2958 0.2688 0.2458 0.2258
0.08 0.4356 0.3998 0.3654 0.3334 0.3044 0.2774 0.2544 0.2344
0.09 0.4436 0.4080 0.3734 0.3414 0.3124 0.2854 0.2624 0.2424
0.10 0.4511 0.4157 0.3811 0.3491 0.3201 0.2931 0.2701 0.2501
0.11 0.4581 0.4231 0.3881 0.3561 0.3271 0.3001 0.2771 0.2571
0.12 0.4645 0.4301 0.3951 0.3631 0.3341 0.3071 0.2841 0.2641
0.13 0.4705 0.4371 0.4021 0.3701 0.3411 0.3141 0.2911 0.2711
0.14 0.4762 0.4441 0.4091 0.3771 0.3481 0.3211 0.2981 0.2781
0.15 0.4817 0.4511 0.4161 0.3841 0.3551 0.3281 0.3051 0.2851
0.16 0.4871 0.4581 0.4231 0.3911 0.3621 0.3351 0.3121 0.2921
0.17 0.4924 0.4651 0.4301 0.3981 0.3691 0.3421 0.3191 0.2991
0.18 0.4975 0.4721 0.4371 0.4051 0.3761 0.3491 0.3261 0.3061
0.19 0.5025 0.4791 0.4441 0.4121 0.3831 0.3561 0.3331 0.3131
0.20 0.5074 0.4861 0.4511 0.4191 0.3901 0.3631 0.3401 0.3201
0.21 0.5122 0.4931 0.4581 0.4261 0.3971 0.3701 0.3471 0.3271
0.22 0.5169 0.5001 0.4651 0.4331 0.4041 0.3811 0.3581 0.3341
0.23 0.5215 0.5071 0.4721 0.4401 0.4111 0.3921 0.3691 0.3451
0.24 0.5260 0.5141 0.4791 0.4471 0.4181 0.4031 0.3841 0.3601
0.25 0.5304 0.5211 0.4861 0.4541 0.4251 0.4101 0.3951 0.3711
0.26 0.5347 0.5281 0.4931 0.4611 0.4321 0.4171 0.4021 0.3821
0.27 0.5389 0.5351 0.5001 0.4681 0.4391 0.4241 0.4091 0.3911
0.28 0.5430 0.5421 0.5071 0.4751 0.4461 0.4311 0.4161 0.3981
0.29 0.5470 0.5491 0.5141 0.4821 0.4531 0.4381 0.4231 0.4051
0.30 0.5509 0.5561 0.5211 0.4891 0.4601 0.4451 0.4301 0.4121
0.31 0.5547 0.5631 0.5281 0.4961 0.4671 0.4521 0.4371 0.4191
0.32 0.5584 0.5701 0.5351 0.5031 0.4741 0.4591 0.4441 0.4261
0.33 0.5620 0.5771 0.5421 0.5101 0.4811 0.4661 0.4511 0.4331
0.34 0.5655 0.5841 0.5491 0.5171 0.4881 0.4731 0.4581 0.4401
0.35 0.5689 0.5911 0.5561 0.5241 0.4951 0.4801 0.4651 0.4471
0.36 0.5722 0.5981 0.5631 0.5311 0.5021 0.4871 0.4721 0.4541
0.37 0.5754 0.6051 0.5701 0.5381 0.5091 0.4941 0.4791 0.4611
0.38 0.5785 0.6121 0.5771 0.5451 0.5161 0.5011 0.4861 0.4681
0.39 0.5815 0.6191 0.5841 0.5521 0.5231 0.5081 0.4931 0.4751
0.40 0.5844 0.6261 0.5911 0.5591 0.5301 0.5151 0.5001 0.4821
0.41 0.5872 0.6331 0.5981 0.5661 0.5371 0.5221 0.5071 0.4891
0.42 0.5900 0.6401 0.6051 0.5731 0.5441 0.5291 0.5141 0.4961
0.43 0.5927 0.6471 0.6121 0.5801 0.5511 0.5361 0.5211 0.5031
0.44 0.5954 0.6541 0.6191 0.5871 0.5581 0.5431 0.5281 0.5101
0.45 0.5980 0.6611 0.6261 0.5941 0.5651 0.5501 0.5351 0.5171
0.46 0.6006 0.6681 0.6331 0.6011 0.5721 0.5571 0.5421 0.5241
0.47 0.6031 0.6751 0.6401 0.6081 0.5791 0.5641 0.5491 0.5311
0.48 0.6056 0.6821 0.6471 0.6151 0.5861 0.5711 0.5561 0.5381
0.49 0.6080 0.6891 0.6541 0.6221 0.5931 0.5781 0.5631 0.5451
0.50 0.6104 0.6961 0.6611 0.6291 0.6001 0.5851 0.5701 0.5521
0.51 0.6128 0.7031 0.6681 0.6361 0.6071 0.5921 0.5771 0.5591
0.52 0.6151 0.7101 0.6751 0.6431 0.6141 0.5991 0.5841 0.5661
0.53 0.6174 0.7171 0.6821 0.6501 0.6211 0.6061 0.5911 0.5731
0.54 0.6196 0.7241 0.6891 0.6571 0.6281 0.6131 0.5981 0.5801
0.55 0.6218 0.7311 0.6961 0.6641 0.6351 0.6201 0.6051 0.5871
0.56 0.6240 0.7381 0.7031 0.6711 0.6421 0.6271 0.6121 0.5941
0.57 0.6261 0.7451 0.7101 0.6781 0.6491 0.6341 0.6191 0.6011
0.58 0.6282 0.7521 0.7171 0.6851 0.6561 0.6411 0.6261 0.6081
0.59 0.6303 0.7591 0.7241 0.6921 0.6631 0.6481 0.6331 0.6151
0.60 0.6324 0.7661 0.7311 0.6991 0.6701 0.6551 0.6401 0.6221
0.61 0.6345 0.7731 0.7381 0.7061 0.6771 0.6621 0.6471 0.6291
0.62 0.6365 0.7801 0.7451 0.7131 0.6841 0.6691 0.6541 0.6361
0.63 0.6385 0.7871 0.7521 0.7201 0.6911 0.6761 0.6611 0.6431
0.64 0.6405 0.7941 0.7591 0.7271 0.6981 0.6831 0.6681 0.6501
0.65 0.6425 0.8011 0.7661 0.7341 0.7051 0.6901 0.6751 0.6571
0.66 0.6445 0.8081 0.7731 0.7411 0.7121 0.6971 0.6821 0.6641
0.67 0.6464 0.8151 0.7801 0.7481 0.7191 0.7041 0.6891 0.6711
0.68 0.6483 0.8221 0.7871 0.7551 0.7261 0.7111 0.6961 0.6781
0.69 0.6502 0.8291 0.7941 0.7621 0.7331 0.7181 0.7031 0.6851
0.70 0.6521 0.8361 0.8011 0.7691 0.7401 0.7251 0.7101 0.6921
0.71 0.6540 0.8431 0.8081 0.7761 0.7471 0.7321 0.7171 0.6991
0.72 0.6559 0.8501 0.8151 0.7831 0.7541 0.7391 0.7241 0.7061
0.73 0.6578 0.8571 0.8221 0.7901 0.7611 0.7461 0.7311 0.7131
0.74 0.6597 0.8641 0.8291 0.7971 0.7681 0.7531 0.7381 0.7201
0.75 0.6616 0.8711 0.8361 0.8041 0.7751 0.7601 0.7451 0.7271
0.76 0.6635 0.8781 0.8431 0.8111 0.7821 0.7671 0.7521 0.7341
0.77 0.6654 0.8851 0.8501 0.8181 0.7891 0.7741 0.7591 0.7411
0.78 0.6673 0.8921 0.8571 0.8251 0.7961 0.7811 0.7661 0.7481
0.79 0.6692 0.8991 0.8641 0.8321 0.8031 0.7881 0.7731 0.7551
0.80 0.6711 0.9061 0.8711 0.8391 0.8101 0.7951 0.7801 0.7621
0.81 0.6730 0.9131 0.8781 0.8461 0.8171 0.8021 0.7871 0.7691
0.82 0.6749 0.9201 0.8851 0.8531 0.8241 0.8141 0.7941 0.7761
0.83 0.6768 0.9271 0.8921 0.8601 0.8311 0.8211 0.8011 0.7831
0.84 0.6787 0.9341 0.8991 0.8671 0.8381 0.8281 0.8081 0.7901
0.85 0.6806 0.9411 0.9061 0.8741 0.8451 0.8351 0.8151 0.7971
0.86 0.6825 0.9481 0.9131 0.8811 0.8521 0.8421 0.8221 0.8041
0.87 0.6844 0.9551 0.9201 0.8881 0.8591 0.8491 0.8291 0.8111
0.88 0.6863 0.9621 0.9271 0.8951 0.8661 0.8561 0.8361 0.8181
0.89 0.6882 0.9691 0.9341 0.9021 0.8731 0.8631 0.8431 0.8251
0.90 0.6901 0.9761 0.9411 0.9091 0.8801 0.8701 0.8501 0.8321
0.91 0.6920 0.9831 0.9481 0.9161 0.8871 0.8771 0.8571 0.8391
0.92 0.6939 0.9901 0.9551 0.9231 0.8941 0.8841 0.8641 0.8461
0.93 0.6958 0.9971 0.9621 0.9301 0.9011 0.8911 0.8711 0.8531
0.94 0.6977 1.0041 0.9691 0.9371 0.9081 0.8981 0.8781 0.8601
0.95 0.6996 1.0111 0.9761 0.9441 0.9151 0.9051 0.8851 0.8671
0.96 0.7015 1.0181 0.9831 0.9511 0.9221 0.9121 0.8921 0.8741
0.97 0.7034 1.0251 0.9901 0.9581 0.9291 0.9191 0.8991 0.8811
0.98 0.7053 1.0321 0.9971 0.9651 0.9361 0.9261 0.9061 0.8881
0.99 0.7072 1.0391 1.0041 0.9721 0.9431 0.9331 0.9131 0.8951
1.00 0.7091 1.0461 1.0111 0.9791 0.9501 0.9401 0.9201 0.9021
```

```
*****
* S.SIZE= 16
* Ramp case" AMU= .40(1.e. PO= 0.34453) *
*****
* GMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 19.52 27.35 34.69 41.35 47.14 51.98 55.86 58.86 *
*****
PEQ < T]
*****TEST CRITERION / T *****
0.01 0.2882 0.2584 0.2309 0.2060 0.1829 0.1645 0.1478 0.1335
0.02 0.3187 0.2879 0.2586 0.2319 0.2078 0.1866 0.1681 0.1522
0.04 0.3388 0.3071 0.2765 0.2486 0.2234 0.2011 0.1815 0.1645
0.05 0.3544 0.3211 0.2901 0.2614 0.2353 0.2121 0.1917 0.1739
0.06 0.3673 0.3329 0.3013 0.2718 0.2451 0.2212 0.2001 0.1817
0.07 0.3783 0.3429 0.3108 0.2808 0.2535 0.2290 0.2074 0.1884
0.08 0.3880 0.3517 0.3199 0.2894 0.2618 0.2376 0.2157 0.2000
0.09 0.3968 0.3598 0.3284 0.2976 0.2696 0.2458 0.2240 0.2117
0.10 0.4047 0.3675 0.3361 0.3051 0.2771 0.2536 0.2320 0.2217
0.11 0.4118 0.3749 0.3435 0.3123 0.2841 0.2609 0.2395 0.2317
0.12 0.4189 0.3821 0.3507 0.3194 0.2911 0.2681 0.2470 0.2410
0.13 0.4259 0.3892 0.3577 0.3264 0.2981 0.2753 0.2544 0.2494
0.14 0.4328 0.3962 0.3647 0.3334 0.3051 0.2825 0.2618 0.2578
0.15 0.4396 0.4031 0.3716 0.3404 0.3121 0.2896 0.2691 0.2662
0.16 0.4464 0.4101 0.3786 0.3474 0.3191 0.2967 0.2764 0.2736
0.17 0.4531 0.4171 0.3856 0.3544 0.3261 0.3038 0.2837 0.2808
0.18 0.4598 0.4241 0.3926 0.3614 0.3331 0.3109 0.2908 0.2880
0.19 0.4665 0.4311 0.3996 0.3684 0.3399 0.3180 0.2979 0.2952
0.20 0.4732 0.4381 0.4066 0.3754 0.3461 0.3251 0.3050 0.3024
0.21 0.4799 0.4451 0.4136 0.3824 0.3531 0.3321 0.3121 0.3096
0.22 0.4866 0.4521 0.4206 0.3894 0.3601 0.3391 0.3191 0.3168
0.23 0.4933 0.4591 0.4276 0.3964 0.3671 0.3461 0.3261 0.3240
0.24 0.5000 0.4661 0.4346 0.4034 0.3741 0.3531 0.3331 0.3312
0.25 0.5067 0.4731 0.4416 0.4104 0.3811 0.3601 0.3401 0.3384
0.26 0.5134 0.4801 0.4486 0.4174 0.3881 0.3671 0.3471 0.3456
0.27 0.5201 0.4871 0.4556 0.4244 0.3951 0.3741 0.3541 0.3528
0.28 0.5268 0.4941 0.4626 0.4314 0.4021 0.3811 0.3611 0.3600
0.29 0.5335 0.5011 0.4696 0.4384 0.4091 0.3881 0.3681 0.3672
0.30 0.5402 0.5081 0.4766 0.4454 0.4161 0.3951 0.3751 0.3744
0.31 0.5469 0.5151 0.4836 0.4524 0.4231 0.4021 0.3821 0.3816
0.32 0.5536 0.5221 0.4906 0.4594 0.4301 0.4091 0.3891 0.3888
0.33 0.5603 0.5291 0.4976 0.4664 0.4371 0.4161 0.3961 0.3960
0.34 0.5670 0.5361 0.5046 0.4734 0.4441 0.4231 0.4031 0.4032
0.35 0.5737 0.5431 0.5116 0.4804 0.4511 0.4301 0.4101 0.4104
0.36 0.5804 0.5501 0.5186 0.4874 0.4581 0.4371 0.4171 0.4176
0.37 0.5871 0.5571 0.5256 0.4944 0.4651 0.4441 0.4241 0.4248
0.38 0.5938 0.5641 0.5326 0.5014 0.4721 0.4511 0.4311 0.4320
0.39 0.6005 0.5711 0.5396 0.5084 0.4791 0.4581 0.4381 0.4392
0.40 0.6072 0.5781 0.5466 0.5154 0.4861 0.4651 0.4451 0.4464
0.41 0.6139 0.5851 0.5536 0.5224 0.4931 0.4721 0.4521 0.4536
0.42 0.6206 0.5921 0.5606 0.5294 0.5001 0.4791 0.4591 0.4608
0.43 0.6273 0.5991 0.5676 0.5364 0.5071 0.4861 0.4661 0.4680
0.44 0.6340 0.6061 0.5746 0.5434 0.5141 0.4931 0.4731 0.4752
0.45 0.6407 0.6131 0.5816 0.5504 0.5211 0.5001 0.4801 0.4824
0.46 0.6474 0.6201 0.5886 0.5574 0.5281 0.5071 0.4871 0.4896
0.47 0.6541 0.6271 0.5956 0.5644 0.5351 0.5141 0.4941 0.4968
0.48 0.6608 0.6341 0.6026 0.5714 0.5421 0.5211 0.5011 0.5040
0.49 0.6675 0.6411 0.6096 0.5784 0.5491 0.5281 0.5081 0.5112
0.50 0.6742 0.6481 0.6166 0.5854 0.5561 0.5351 0.5151 0.5184
0.51 0.6809 0.6551 0.6236 0.5924 0.5631 0.5421 0.5221 0.5256
0.52 0.6876 0.6621 0.6306 0.5994 0.5701 0.5491 0.5291 0.5328
0.53 0.6943 0.6691 0.6376 0.6064 0.5771 0.5561 0.5361 0.5400
0.54 0.7010 0.6761 0.6446 0.6134 0.5841 0.5631 0.5431 0.5472
0.55 0.7077 0.6831 0.6516 0.6204 0.5911 0.5701 0.5501 0.5544
0.56 0.7144 0.6901 0.6586 0.6274 0.5981 0.5771 0.5571 0.5616
0.57 0.7211 0.6971 0.6656 0.6344 0.6051 0.5841 0.5641 0.5688
0.58 0.7278 0.7041 0.6726 0.6414 0.6121 0.5911 0.5711 0.5760
0.59 0.7345 0.7111 0.6796 0.6484 0.6191 0.5981 0.5781 0.5832
0.60 0.7412 0.7181 0.6866 0.6554 0.6261 0.6051 0.5851 0.5904
0.61 0.7479 0.7251 0.6936 0.6624 0.6331 0.6121 0.5921 0.5976
0.62 0.7546 0.7321 0.7006 0.6694 0.6401 0.6191 0.6091 0.6048
0.63 0.7613 0.7391 0.7076 0.6764 0.6471 0.6261 0.6161 0.6120
0.64 0.7680 0.7461 0.7146 0.6834 0.6541 0.6331 0.6231 0.6192
0.65 0.7747 0.7531 0.7216 0.6904 0.6611 0.6401 0.6301 0.6264
0.66 0.7814 0.7601 0.7286 0.6974 0.6681 0.6471 0.6371 0.6336
0.67 0.7881 0.7671 0.7356 0.7044 0.6751 0.6541 0.6441 0.6408
0.68 0.7948 0.7741 0.7426 0.7114 0.6821 0.6611 0.6511 0.6480
0.69 0.8015 0.7811 0.7496 0.7184 0.6891 0.6681 0.6581 0.6552
0.70 0.8082 0.7881 0.7566 0.7254 0.6961 0.6751 0.6651 0.6624
0.71 0.8149 0.7951 0.7636 0.7324 0.7031 0.6821 0.6721 0.6696
0.72 0.8216 0.8021 0.7706 0.7394 0.7101 0.6891 0.6791 0.6768
0.73 0.8283 0.8091 0.7776 0.7464 0.7171 0.6961 0.6861 0.6840
0.74 0.8350 0.8161 0.7846 0.7534 0.7241 0.7031 0.6931 0.6912
0.75 0.8417 0.8231 0.7916 0.7604 0.7311 0.7101 0.7001 0.6984
0.76 0.8484 0.8301 0.7986 0.7674 0.7381 0.7171 0.7071 0.7056
0.77 0.8551 0.8371 0.8056 0.7744 0.7451 0.7241 0.7141 0.7128
0.78 0.8618 0.8441 0.8126 0.7814 0.7521 0.7311 0.7211 0.7200
0.79 0.8685 0.8511 0.8196 0.7884 0.7591 0.7381 0.7281 0.7272
0.80 0.8752 0.8581 0.8266 0.7954 0.7661 0.7451 0.7351 0.7344
0.81 0.8819 0.8651 0.8336 0.8024 0.7731 0.7521 0.7421 0.7416
0.82 0.8886 0.8721 0.8406 0.8094 0.7801 0.7591 0.7491 0.7488
0.83 0.8953 0.8791 0.8476 0.8164 0.7871 0.7661 0.7561 0.7560
0.84 0.9020 0.8861 0.8546 0.8234 0.7941 0.7731 0.7631 0.7632
0.85 0.9087 0.8931 0.8616 0.8304 0.8011 0.7801 0.7701 0.7704
0.86 0.9154 0.9001 0.8686 0.8374 0.8081 0.7871 0.7771 0.7776
0.87 0.9221 0.9071 0.8756 0.8444 0.8151 0.7941 0.7841 0.7848
0.88 0.9288 0.9141 0.8826 0.8514 0.8221 0.8011 0.7911 0.7920
0.89 0.9355 0.9211 0.8896 0.8584 0.8291 0.8081 0.7981 0.7992
0.90 0.9422 0.9281 0.8966 0.8654 0.8361 0.8151 0.8051 0.8064
0.91 0.9489 0.9351 0.9036 0.8724 0.8431 0.8221 0.8121 0.8136
0.92 0.9556 0.9421 0.9106 0.8794 0.8501 0.8291 0.8191 0.8208
0.93 0.9623 0.9491 0.9176 0.8864 0.8571 0.8361 0.8261 0.8280
0.94 0.9690 0.9561 0.9246 0.8934 0.8641 0.8431 0.8331 0.8352
0.95 0.9757 0.9631 0.9316 0.9004 0.8711 0.8501 0.8401 0.8424
0.96 0.9824 0.9701 0.9386 0.9074 0.8781 0.8571 0.847
```

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* S.SIZE= 16      " Ramp case"      AMU= .65(i.e. PO= 0.27425) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 18.59 26.56 34.37 41.72 48.38 54.17 59.01 62.89 *
*****
PCQ < T]      .....TEST CRITERION ,T .....
0.01      0.3674 0.3341 0.3033 0.2743 0.2477 0.2238 0.2026 0.1840
0.02      0.3981 0.3650 0.3325 0.3020 0.2737 0.2481 0.2252 0.2049
0.03      0.4190 0.3843 0.3512 0.3197 0.2905 0.2638 0.2398 0.2186
0.04      0.4350 0.3991 0.3654 0.3332 0.3032 0.2758 0.2510 0.2290
0.05      0.4460 0.4112 0.3769 0.3442 0.3138 0.2856 0.2602 0.2375
0.06      0.4567 0.4216 0.3868 0.3537 0.3226 0.2940 0.2680 0.2449
0.49      0.6345 0.5958 0.5560 0.5166 0.4785 0.4421 0.4081 0.3767
0.50      0.6375 0.5986 0.5588 0.5193 0.4811 0.4446 0.4105 0.3789
0.51      0.6405 0.6015 0.5615 0.5220 0.4837 0.4471 0.4128 0.3812
0.89      0.7723 0.7328 0.6913 0.6494 0.6077 0.5669 0.5278 0.4908
0.90      0.7784 0.7386 0.6971 0.6551 0.6133 0.5724 0.5331 0.4959
0.91      0.7848 0.7448 0.7033 0.6613 0.6193 0.5783 0.5388 0.5014
0.94      0.8073 0.7667 0.7256 0.6834 0.6411 0.5995 0.5593 0.5211
0.95      0.8132 0.7761 0.7348 0.6926 0.6502 0.6084 0.5680 0.5295
0.96      0.8247 0.7869 0.7456 0.7034 0.6608 0.6188 0.5781 0.5393

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* S.SIZE= 16      " Ramp case"      AMU= .70(i.e. PO= 0.24196) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 17.88 25.80 33.73 41.35 48.38 54.62 59.94 64.30 *
*****
PCQ < T]      .....TEST CRITERION ,T .....
0.01      0.4063 0.3736 0.3412 0.3106 0.2821 0.2561 0.2327 0.2120
0.02      0.4372 0.4043 0.3710 0.3389 0.3089 0.2813 0.2563 0.2339
0.03      0.4584 0.4241 0.3899 0.3571 0.3261 0.2975 0.2715 0.2482
0.04      0.4741 0.4388 0.4042 0.3708 0.3392 0.3098 0.2831 0.2590
0.05      0.4871 0.4509 0.4159 0.3820 0.3498 0.3199 0.2925 0.2679
0.06      0.4981 0.4612 0.4259 0.3915 0.3589 0.3285 0.3007 0.2755
0.49      0.6732 0.6338 0.5945 0.5551 0.5163 0.4790 0.4436 0.4106
0.50      0.6761 0.6366 0.5973 0.5578 0.5189 0.4815 0.4460 0.4129
0.51      0.6789 0.6394 0.6000 0.5604 0.5215 0.4840 0.4484 0.4152
0.89      0.8063 0.7670 0.7272 0.6860 0.6446 0.6036 0.5638 0.5258
0.90      0.8121 0.7727 0.7328 0.6916 0.6501 0.6090 0.5691 0.5309
0.91      0.8143 0.7748 0.7348 0.6936 0.6521 0.6114 0.5718 0.5336
0.94      0.8373 0.8002 0.7603 0.7192 0.6774 0.6359 0.5952 0.5562
0.95      0.8465 0.8090 0.7692 0.7282 0.6864 0.6446 0.6038 0.5645
0.96      0.8571 0.8184 0.7797 0.7386 0.6968 0.6549 0.6139 0.5743

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* S.SIZE= 16      " Ramp case"      AMU= .80(i.e. PO= 0.21186) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 17.02 24.83 32.80 40.61 47.96 54.62 60.41 65.25 *
*****
PCQ < T]      .....TEST CRITERION ,T .....
0.01      0.4460 0.4129 0.3799 0.3480 0.3170 0.2900 0.2645 0.2417
0.02      0.4785 0.4439 0.4099 0.3768 0.3453 0.3158 0.2889 0.2645
0.03      0.4996 0.4636 0.4290 0.3951 0.3628 0.3325 0.3045 0.2792
0.04      0.5132 0.4785 0.4434 0.4090 0.3760 0.3451 0.3164 0.2904
0.05      0.5257 0.4907 0.4551 0.4203 0.3869 0.3554 0.3262 0.2995
0.06      0.5365 0.5007 0.4650 0.4299 0.3961 0.3641 0.3345 0.3074
0.49      0.7078 0.6710 0.6322 0.5930 0.5541 0.5160 0.4795 0.4452
0.50      0.7106 0.6737 0.6349 0.5957 0.5566 0.5185 0.4820 0.4475
0.51      0.7135 0.6765 0.6376 0.5983 0.5592 0.5210 0.4844 0.4498
0.89      0.8352 0.7999 0.7613 0.7214 0.6806 0.6398 0.5996 0.5609
0.90      0.8409 0.8052 0.7667 0.7268 0.6860 0.6451 0.6049 0.5660
0.91      0.8469 0.8109 0.7725 0.7327 0.6918 0.6508 0.6105 0.5714
0.94      0.8674 0.8308 0.7932 0.7535 0.7127 0.6715 0.6307 0.5911
0.95      -0.1000 0.8393 0.8018 0.7622 0.7213 0.6801 0.6392 0.5994
0.96      0.8802 0.8492 0.8117 0.7723 0.7315 0.6902 0.6491 0.6091

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```

* S.SIZE= 16      " Ramp case"      AMU= .90(i.e. PO= 0.18406) *
*****
* QMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 16.05 23.67 31.59 39.52 47.14 54.17 60.41 65.73 *
*****
PCQ < T]      .....TEST CRITERION ,T .....
0.01      0.4866 0.4524 0.4190 0.3861 0.3546 0.3250 0.2977 0.2728
0.02      0.5171 0.4835 0.4490 0.4151 0.3824 0.3514 0.3227 0.2964
0.03      0.5376 0.5029 0.4681 0.4336 0.4001 0.3684 0.3387 0.3115
0.04      0.5533 0.5176 0.4825 0.4475 0.4135 0.3812 0.3509 0.3230
0.05      0.5637 0.5296 0.4942 0.4588 0.4244 0.3916 0.3608 0.3324
0.06      0.5742 0.5398 0.5040 0.4685 0.4337 0.4005 0.3693 0.3404
0.49      0.7433 0.7062 0.6688 0.6302 0.5913 0.5529 0.5156 0.4801
0.50      0.7460 0.7088 0.6714 0.6328 0.5938 0.5554 0.5180 0.4824
0.51      0.7487 0.7115 0.6740 0.6353 0.5964 0.5579 0.5205 0.4848
0.89      0.8650 0.8297 0.7936 0.7551 0.7154 0.6750 0.6349 0.5957
0.90      0.8701 0.8349 0.7988 0.7604 0.7207 0.6803 0.6401 0.6008
0.91      -0.1000 0.8404 0.8043 0.7660 0.7263 0.6859 0.6456 0.6062
0.94      0.8903 0.8598 0.8239 0.7861 0.7465 0.7060 0.6655 0.6257
0.95      0.8991 0.8676 0.8321 0.7944 0.7549 0.7144 0.6738 0.6339
0.96      0.9091 0.8755 0.8416 0.8040 0.7647 0.7242 0.6836 0.6434

```

```

* S.SIZE= 16      " Ramp case"      AMU=1.00(i.e. PO= 0.15266) *
*****
* GMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 14.99 22.34 30.15 38.12 45.98 53.22 59.94 65.73 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      0.5245 0.4918 0.4580 0.4245 0.3920 0.3610 0.3319 0.3053
0.02      0.5570 0.5222 0.4879 0.4536 0.4200 0.3878 0.3575 0.3294
0.03      0.5749 0.5416 0.5069 0.4721 0.4379 0.4049 0.3738 0.3449
0.04      0.5899 0.5563 0.5211 0.4859 0.4518 0.4178 0.3861 0.3566
0.05      0.6022 0.5677 0.5327 0.4972 0.4622 0.4284 0.3962 0.3661
0.06      0.6128 0.5777 0.5425 0.5068 0.4715 0.4373 0.4048 0.3743
0.49      0.7735 0.7402 0.7038 0.6662 0.6277 0.5893 0.5516 0.5152
0.50      0.7761 0.7427 0.7063 0.6687 0.6302 0.5918 0.5540 0.5176
0.51      0.7788 0.7452 0.7088 0.6712 0.6328 0.5942 0.5564 0.5199
0.89      0.8863 0.8581 0.8236 0.7871 0.7497 0.7092 0.6694 0.6301
0.90      0.8918 0.8629 0.8285 0.7921 0.7536 0.7143 0.6745 0.6351
0.91      0.8975 0.8680 0.8338 0.7975 0.7592 0.7197 0.6799 0.6404
0.94      0.9169 0.8845 0.8525 0.8166 0.7786 0.7393 0.6993 0.6596
0.95      0.9247 0.8924 0.8602 0.8245 0.7867 0.7474 0.7075 0.6676
0.96      0.9326 0.9014 0.8690 0.8337 0.7961 0.7569 0.7169 0.6770

```

```

* S.SIZE= 16      " Ramp case"      AMU=1.10(i.e. PO= 0.13567) *
*****
* GMIN x100: 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 13.86 20.89 28.51 36.43 44.36 51.98 59.01 65.25 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      -0.1000 0.5300 0.4966 0.4629 0.4298 0.3975 0.3670 0.3387
0.02      0.5928 0.5605 0.5262 0.4919 0.4578 0.4246 0.3929 0.3633
0.03      0.6130 0.5791 0.5450 0.5102 0.4756 0.4418 0.4094 0.3790
0.04      0.6252 0.5933 0.5591 0.5240 0.4890 0.4548 0.4219 0.3909
0.05      0.6371 0.6049 0.5704 0.5351 0.4999 0.4653 0.4320 0.4006
0.06      0.6472 0.6148 0.5800 0.5446 0.5091 0.4743 0.4407 0.4089
0.49      0.8051 0.7714 0.7371 0.7007 0.6631 0.6255 0.5872 0.5502
0.50      0.8076 0.7738 0.7396 0.7032 0.6656 0.6274 0.5895 0.5525
0.51      0.8102 0.7763 0.7420 0.7056 0.6680 0.6299 0.5919 0.5548
0.89      0.9128 0.8818 0.8515 0.8169 0.7802 0.7419 0.7028 0.6637
0.90      0.9175 0.8866 0.8562 0.8217 0.7851 0.7469 0.7078 0.6686
0.91      0.9226 0.8913 0.8611 0.8268 0.7903 0.7521 0.7130 0.6738
0.94      -0.1000 0.9094 0.8779 0.8450 0.8085 0.7710 0.7320 0.6926
0.95      -0.1000 0.9163 0.8853 0.8524 0.8166 0.7788 0.7398 0.7005
0.96      0.9429 0.9243 0.8938 0.8610 0.8255 0.7879 0.7490 0.7096

```

```

* S.SIZE= 16      " Ramp case"      AMU=1.20(i.e. PO= 0.11507) *
*****
* GMIN x100: 50.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 0.5000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 12.69 19.35 26.70 34.51 42.41 50.28 57.64 64.30 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      0.6004 0.5672 0.5345 0.5009 0.4673 0.4344 0.4027 0.3729
0.02      0.6308 0.5969 0.5637 0.5296 0.4958 0.4615 0.4288 0.3978
0.03      0.6490 0.6157 0.5821 0.5477 0.5130 0.4787 0.4454 0.4137
0.04      0.6630 0.6290 0.5958 0.5613 0.5263 0.4916 0.4579 0.4257
0.05      0.6746 0.6403 0.6070 0.5723 0.5371 0.5021 0.4681 0.4355
0.06      0.6845 0.6498 0.6164 0.5816 0.5463 0.5111 0.4767 0.4438
0.49      0.8390 0.8013 0.7684 0.7336 0.6972 0.6597 0.6220 0.5848
0.50      0.8415 0.8036 0.7707 0.7360 0.6995 0.6621 0.6244 0.5871
0.51      -0.1000 0.8060 0.7731 0.7384 0.7019 0.6644 0.6267 0.5894
0.89      -0.1000 0.9062 0.8762 0.8447 0.8099 0.7731 0.7350 0.6964
0.90      0.9405 0.9105 0.8806 0.8492 0.8145 0.7778 0.7398 0.7012
0.91      0.9481 0.9150 0.8854 0.8540 0.8195 0.7829 0.7449 0.7063
0.94      -0.1000 0.9305 0.9021 0.8709 0.8371 0.8009 0.7631 0.7245
0.95      -0.1000 0.9368 0.9088 0.8778 0.8443 0.8083 0.7707 0.7321
0.96      -0.1000 0.9389 0.9164 0.8859 0.8527 0.8170 0.7795 0.7410

```

```

* S.SIZE= 16      " Ramp case"      AMU=1.30(i.e. PO= 0.09680) *
*****
* GMIN x100: 50.0000 50.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 0.5000 0.5000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 11.51 17.75 24.78 32.39 40.32 48.25 55.86 62.89 *
*****
P[Q < T]      .....TEST CRITERION ,T .....
0.01      0.6357 0.6038 0.5713 0.5382 0.5046 0.4712 0.4387 0.4076
0.02      0.6643 0.6327 0.5999 0.5665 0.5323 0.4982 0.4648 0.4327
0.03      0.6832 0.6505 0.6179 0.5842 0.5498 0.5153 0.4814 0.4487
0.04      0.6964 0.6640 0.6312 0.5975 0.5629 0.5281 0.4939 0.4607
0.05      0.7069 0.6749 0.6421 0.6083 0.5735 0.5385 0.5040 0.4705
0.06      0.7161 0.6842 0.6513 0.6174 0.5826 0.5474 0.5126 0.4789
0.49      0.8645 0.8303 0.7977 0.7646 0.7296 0.6932 0.6560 0.6188
0.50      0.8668 0.8326 0.8000 0.7669 0.7319 0.6955 0.6583 0.6211
0.51      0.8691 0.8348 0.8022 0.7692 0.7342 0.6977 0.6605 0.6233
0.89      0.9663 0.9320 0.8997 0.8670 0.8374 0.8024 0.7656 0.7279
0.90      -0.1000 0.9361 0.9038 0.8742 0.8418 0.8069 0.7702 0.7325
0.91      -0.1000 0.9361 0.9038 0.8742 0.8418 0.8069 0.7702 0.7325
0.94      0.9704 0.9536 0.9232 0.8945 0.8630 0.8288 0.7926 0.7551
0.95      0.9773 0.9615 0.9291 0.9010 0.8698 0.8359 0.7999 0.7625
0.96      0.9847 0.9689 0.9360 0.9085 0.8776 0.8441 0.8083 0.7710

```

```

* S.SIZE= 16      " Ramp case"      AMU=1.40(i.e. PO= 0.08078) *
*****
* QMIN x100:50.000050.000050.000050.000050.0000 0.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 1.0000 1.0000 1.0000 1.0000 *
* P1 x 100: 10.35 16.12 22.78 30.13 37.94 45.91 53.72 61.07 *
*****
PEQ < T]      .....TEST CRITERION ,T .....

```

0.01	0.6685	0.6383	0.6071	0.5747	0.5412	0.5077	0.4746	0.4426
0.02	0.6969	0.6661	0.6349	0.6023	0.5688	0.5344	0.5006	0.4678
0.03	0.7138	0.6838	0.6523	0.6196	0.5857	0.5513	0.5171	0.4837
0.04	0.7270	0.6966	0.6653	0.6326	0.5986	0.5640	0.5295	0.4957
0.05	0.7379	0.7070	0.6758	0.6430	0.6090	0.5742	0.5395	0.5055
0.06	0.7472	0.7158	0.6847	0.6519	0.6178	0.5829	0.5481	0.5138
0.49	0.8880	0.8555	0.8232	0.7938	0.7603	0.7251	0.6888	0.6520
0.50	0.8903	0.8576	0.8274	0.7959	0.7625	0.7273	0.6910	0.6542
0.51	0.8927	0.8597	0.8295	0.7981	0.7647	0.7295	0.6932	0.6564
0.89	-0.1000	0.9483	0.9220	0.8935	0.8627	0.8297	0.7946	0.7580
0.90	-0.1000	0.9531	0.9258	0.8975	0.8667	0.8340	0.7990	0.7624
0.91	0.9725	0.9582	0.9297	0.9017	0.8712	0.8385	0.8038	0.7672
0.94	0.9876	-0.1000	0.9422	0.9162	0.8866	0.8547	0.8203	0.7842
0.95	0.9932	0.9694	0.9489	0.9222	0.8930	0.8613	0.8272	0.7912
0.96	0.9991	0.9759	0.9564	0.9290	0.9003	0.8690	0.8352	0.7994

```

* S.SIZE= 16      " Ramp case"      AMU=1.50(i.e. PO= 0.06681) *
*****
* QMIN x100:50.000050.000050.000050.000049.0000 0.0000 0.0000 0.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 1.0000 1.0000 1.0000 *
* P1 x 100: 9.18 14.50 20.74 27.78 35.39 43.32 51.25 58.86 *
*****
PEQ < T]      .....TEST CRITERION ,T .....

```

0.01	0.7009	0.6709	0.6411	0.6097	0.5770	0.5435	0.5102	0.4775
0.02	0.7274	0.6979	0.6680	0.6366	0.6037	0.5699	0.5360	0.5026
0.03	0.7451	0.7145	0.6849	0.6534	0.6208	0.5865	0.5523	0.5185
0.04	0.7567	0.7270	0.6974	0.6660	0.6330	0.5989	0.5645	0.5304
0.05	0.7662	0.7372	0.7075	0.6762	0.6431	0.6090	0.5744	0.5401
0.06	0.7745	0.7459	0.7160	0.6847	0.6517	0.6175	0.5828	0.5483
0.49	0.9072	0.8783	0.8502	0.8207	0.7891	0.7554	0.7202	0.6840
0.50	0.9093	0.8803	0.8522	0.8227	0.7912	0.7575	0.7223	0.6862
0.51	0.9115	0.8824	0.8542	0.8248	0.7933	0.7597	0.7245	0.6883
0.89	0.9813	-0.1000	0.9385	0.9141	0.8851	0.8549	0.8217	0.7865
0.90	0.9850	-0.1000	0.9425	0.9177	0.8897	0.8590	0.8258	0.7908
0.91	0.9889	-0.1000	0.9468	0.9215	0.8938	0.8632	0.8303	0.7953
0.94	-0.1000	0.9789	0.9616	0.9349	0.9081	0.8784	0.8460	0.8116
0.95	-0.1000	0.9838	0.9676	0.9398	0.9139	0.8846	0.8525	0.8183
0.96	-0.1000	0.9891	0.9700	0.9466	0.9208	0.8917	0.8601	0.8261

```

* S.SIZE= 16      " Ramp case"      AMU=1.60(i.e. PO= 0.05460) *
*****
* QMIN x100:50.000050.000050.000050.000050.000049.000047.000044.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 8.09 12.93 18.72 25.37 32.73 40.54 48.50 56.31 *
*****
PEQ < T]      .....TEST CRITERION ,T .....

```

0.01	0.7296	0.7027	0.6734	0.6432	0.6115	0.5786	0.5454	0.5125
0.02	0.7557	0.7261	0.6994	0.6693	0.6375	0.6044	0.5708	0.5372
0.03	0.7718	0.7445	0.7155	0.6856	0.6538	0.6206	0.5868	0.5528
0.04	0.7827	0.7559	0.7276	0.6977	0.6660	0.6327	0.5987	0.5646
0.05	0.7927	0.7653	0.7373	0.7075	0.6758	0.6425	0.6084	0.5741
0.06	0.8012	0.7733	0.7456	0.7158	0.6841	0.6508	0.6167	0.5822
0.49	0.9281	0.9000	0.8728	0.8454	0.8158	0.7839	0.7500	0.7149
0.50	0.9301	0.9019	0.8747	0.8474	0.8178	0.7859	0.7521	0.7169
0.51	0.9320	0.9038	0.8765	0.8493	0.8198	0.7880	0.7541	0.7190
0.89	0.9959	0.9738	0.9575	0.9323	0.9066	0.8780	0.8468	0.8134
0.90	0.9990	0.9770	0.9611	0.9356	0.9101	0.8818	0.8507	0.8174
0.91	-0.1000	0.9804	0.9649	0.9385	0.9135	0.8858	0.8549	0.8217
0.94	-0.1000	0.9912	0.9717	0.9519	0.9270	0.8998	0.8697	0.8371
0.95	-0.1000	0.9951	0.9762	0.9572	0.9323	0.9056	0.8758	0.8435
0.96	-0.1000	0.9994	0.9813	0.9633	0.9382	0.9122	0.8828	0.8508

```

* S.SIZE= 16      " Ramp case"      AMU=1.70(i.e. PO= 0.04457) *
*****
* QMIN x100:50.000050.000050.000050.000050.000049.000046.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 7.05 11.41 16.73 22.97 30.00 37.62 45.54 53.47 *
*****
PEQ < T]      .....TEST CRITERION ,T .....

```

0.01	0.7569	0.7310	0.7046	0.6751	0.6445	0.6125	0.5796	0.5465
0.02	0.7805	0.7556	0.7292	0.7002	0.6697	0.6376	0.6045	0.5710
0.03	0.7966	0.7706	0.7447	0.7159	0.6855	0.6534	0.6201	0.5864
0.04	0.8092	0.7819	0.7559	0.7276	0.6972	0.6652	0.6318	0.5980
0.05	0.8179	0.7912	0.7651	0.7370	0.7067	0.6747	0.6415	0.6073
0.06	0.8250	0.7991	0.7729	0.7449	0.7147	0.6827	0.6493	0.6153
0.49	0.9386	0.9180	0.8936	0.8679	0.8405	0.8104	0.7782	0.7442
0.50	0.9409	0.9197	0.8954	0.8698	0.8423	0.8124	0.7801	0.7462
0.51	0.9434	0.9215	0.8971	0.8716	0.8442	0.8143	0.7821	0.7482
0.89	-0.1000	0.9866	-0.1000	0.9487	0.9250	0.8989	0.8699	0.8384
0.90	-0.1000	0.9893	0.9704	0.9520	0.9282	0.9024	0.8736	0.8422
0.91	-0.1000	0.9921	0.9735	0.9554	0.9317	0.9061	0.8775	0.8463
0.94	-0.1000	-0.1000	0.9836	0.9673	0.9437	0.9190	0.8913	0.8608
0.95	-0.1000	-0.1000	0.9874	0.9692	0.9487	0.9243	0.8969	0.8667
0.96	-0.1000	-0.1000	0.9915	0.9741	0.9544	0.9303	0.9034	0.8736


```
* S.SIZE= 16      " Ramp case"          AMU=1.20(i.e. PO= 0.03593) *  
*****  
* QMIN x100:50.000050.000050.000050.000050.000050.000050.000049.0000 *  
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *  
* P1 x 100: 6.09 9.97 14.81 20.60 27.26 34.62 42.42 50.59 *  
*****  
PEQ < T]      .....TEST CRITERION ,T .....
```

0.01	0.7807	0.7576	0.7327	0.7059	0.6759	0.6450	0.6127	0.5799
0.02	0.8063	0.7807	0.7563	0.7297	0.7003	0.6694	0.6370	0.6039
0.03	0.8204	0.7956	0.7710	0.7447	0.7155	0.6847	0.6523	0.6191
0.04	0.8304	0.8069	0.7819	0.7556	0.7265	0.6960	0.6637	0.6304
0.05	0.8389	0.8157	0.7908	0.7646	0.7359	0.7052	0.6729	0.6395
0.06	0.8463	0.8227	0.7983	0.7721	0.7436	0.7130	0.6806	0.6472
0.49	0.9600	0.9349	0.9118	0.8884	0.8629	0.8350	0.8045	0.7720
0.50	0.9622	0.9366	0.9134	0.8902	0.8647	0.8368	0.8064	0.7759
0.51	0.9644	0.1000	0.9150	0.8918	0.8665	0.8386	0.8083	0.7752
0.89	-0.1000	0.9971	0.9797	0.9638	0.9411	0.9176	0.8909	0.8615
0.90	-0.1000	0.9993	0.9821	0.9667	0.9442	0.9208	0.8943	0.8651
0.91	-0.1000	0.1000	0.9847	0.1000	0.9475	0.9242	0.8980	0.8689
0.94	-0.1000	0.1000	0.9931	0.9768	0.9528	0.9359	0.9107	0.8825
0.95	-0.1000	0.1000	0.9962	0.9806	0.9632	0.9407	0.9159	0.8880
0.96	-0.1000	0.1000	0.9995	0.9847	0.9683	0.9463	0.9219	0.8944

```
* S.SIZE= 16      " Ramp case"          AMU=1.90(i.e. PO= 0.02972) *  
*****  
* QMIN x100:75.000050.000050.000050.000050.000050.000050.000049.0000 *  
* SCALEx100: 0.2500 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *  
* P1 x 100: 5.20 8.64 12.99 18.31 24.55 31.55 38.20 47.13 *  
*****  
PEQ < T]      .....TEST CRITERION ,T .....
```

0.01	0.8092	0.7817	0.7588	0.7336	0.7027	0.6759	0.6446	0.6123
0.02	0.8279	0.8050	0.8125	0.7565	0.7294	0.6995	0.6683	0.6358
0.03	0.8413	0.8189	0.7956	0.7708	0.7439	0.7143	0.6830	0.6506
0.04	0.8520	0.8287	0.8062	0.7815	0.7545	0.7252	0.6941	0.6616
0.05	0.8610	0.8368	0.8147	0.7900	0.7632	0.7340	0.7029	0.6704
0.06	0.8687	0.8750	0.8216	0.7972	0.7706	0.7415	0.7104	0.6780
0.49	0.9773	0.9489	0.9281	0.9067	0.8834	0.8575	0.8289	0.7981
0.50	0.9792	0.9507	0.9296	0.9083	0.8850	0.8592	0.8307	0.7999
0.51	0.9812	0.9524	0.9311	0.9098	0.8867	0.8609	0.8325	0.8017
0.89	-0.1000	0.1000	0.9896	0.9734	0.9560	0.9341	0.9099	0.8826
0.90	-0.1000	0.1000	0.9917	0.9758	0.9578	0.9370	0.9130	0.8860
0.91	-0.1000	0.1000	0.9938	0.9783	0.9617	0.9400	0.9163	0.8895
0.94	-0.1000	0.1000	0.9986	0.9866	0.9702	0.9510	0.9280	0.9021
0.95	-0.1000	0.1000	0.9997	0.9897	0.9739	0.9554	0.9328	0.9075
0.96	-0.1000	0.1000	0.9999	0.9930	0.9781	0.9603	0.9382	0.9132

```
* S.SIZE= 16      " Ramp case"          AMU=2.00(i.e. PO= 0.02275) *  
*****  
* QMIN x100:75.000075.000075.000050.000050.000050.000050.000050.0000 *  
* SCALEx100: 0.2500 0.2500 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *  
* P1 x 100: 4.41 7.41 11.29 16.13 21.92 28.58 35.93 43.74 *  
*****  
PEQ < T]      .....TEST CRITERION ,T .....
```

0.01	0.8264	0.8030	0.7839	0.7596	0.7338	0.7058	0.6763	0.6430
0.02	0.8473	0.8271	0.8050	0.7816	0.7560	0.7282	0.6985	0.6665
0.03	0.8619	0.8398	0.8184	0.7953	0.7689	0.7423	0.7126	0.6806
0.04	0.8731	0.8496	0.8281	0.8054	0.7803	0.7527	0.7231	0.6914
0.05	0.8796	0.8577	0.8359	0.8136	0.7865	0.7611	0.7316	0.7000
0.06	0.8854	0.8646	0.8426	0.8203	0.7955	0.7682	0.7387	0.7073
0.49	-0.1000	0.9666	0.9420	0.9229	0.9017	0.8779	0.8514	0.8224
0.50	-0.1000	0.9682	0.9436	0.9244	0.9033	0.8795	0.8531	0.8241
0.51	-0.1000	0.1000	0.9452	0.9258	0.9048	0.8811	0.8548	0.8259
0.89	-0.1000	0.1000	0.9977	0.9834	0.9686	0.9488	0.9267	0.9018
0.90	-0.1000	0.1000	0.9995	0.9854	0.9696	0.9514	0.9295	0.9049
0.91	-0.1000	0.1000	0.9975	0.9875	0.9721	0.9543	0.9326	0.9082
0.94	-0.1000	0.1000	0.9994	0.9904	0.9804	0.9640	0.9432	0.9198
0.95	-0.1000	0.1000	0.9969	0.9885	0.9735	0.9678	0.9476	0.9245
0.96	-0.1000	0.1000	0.9996	0.9870	0.9714	0.9525	0.9299	0.9029

```
* S.SIZE= 16      " Ramp case"          AMU=2.10(i.e. PO= 0.01726) *  
*****  
* QMIN x100:75.000075.000075.000050.000050.000050.000050.000050.0000 *  
* SCALEx100: 0.2500 0.2500 0.2500 0.5000 0.5000 0.5000 0.5000 0.5000 *  
* P1 x 100: 3.69 6.29 9.72 14.08 19.40 25.64 32.67 40.29 *  
*****  
PEQ < T]      .....TEST CRITERION ,T .....
```

0.01	0.8449	0.8264	0.8080	0.7837	0.7596	0.7331	0.7045	0.6745
0.02	0.8679	0.8461	0.8271	0.8048	0.7810	0.7547	0.7263	0.6962
0.03	0.8797	0.8591	0.8394	0.8178	0.7942	0.7682	0.7399	0.7098
0.04	0.8874	0.8690	0.8487	0.8272	0.8040	0.7782	0.7513	0.7200
0.05	0.8943	0.8762	0.8562	0.8349	0.8119	0.7863	0.7582	0.7282
0.06	0.9004	0.8818	0.8626	0.8413	0.8185	0.7930	0.7651	0.7352
0.49	-0.1000	0.9768	0.9573	0.9373	0.9180	0.8964	0.8720	0.8449
0.50	-0.1000	0.9782	0.9587	0.9382	0.9194	0.8979	0.8735	0.8465
0.51	0.9856	0.9797	0.9601	0.9396	0.9208	0.8994	0.8751	0.8482
0.89	-0.1000	0.1000	0.9915	0.9775	0.9615	0.9415	0.9189	0.8919
0.90	-0.1000	0.1000	0.9932	0.9795	0.9795	0.9639	0.9442	0.9218
0.91	-0.1000	0.1000	0.9950	0.9816	0.9664	0.9470	0.9248	0.8978
0.94	-0.1000	0.1000	0.9986	0.9886	0.9742	0.9566	0.9354	0.9109
0.95	-0.1000	0.1000	0.9993	0.9913	0.9774	0.9605	0.9397	0.9149
0.96	-0.1000	0.1000	0.9994	0.9941	0.9810	0.9648	0.9446	0.9200

* S.SIZE= 16 " Ramp case" AMU=2.20(i.e. PO= 0.01850) *

* QMIN x100:75.000075.000075.000075.000075.000050.000050.000050.000050.0000 *
* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 3.07 5.29 8.29 12.18 17.02 22.81 29.46 36.82 *

P[Q < T]TEST CRITERION ,T

0.01	0.8649	0.8446	0.8270	0.8080	0.7836	0.7587	0.7315	0.7025
0.02	0.8828	0.8650	0.8460	0.8269	0.8040	0.7795	0.7525	0.7236
0.03	0.8930	0.8769	0.8581	0.8388	0.8166	0.7923	0.7657	0.7368
0.04	0.9016	0.8845	0.8672	0.8477	0.8259	0.8019	0.7754	0.7467
0.05	0.9090	0.8910	0.8742	0.8549	0.8332	0.8095	0.7832	0.7546
0.06	0.9156	0.8967	0.8797	0.8609	0.8395	0.8159	0.7898	0.7613
0.49	0.9953	0.1000	0.1000	0.9509	0.9324	0.9129	0.8906	0.8655
0.50	0.9970	0.1000	0.9695	0.9522	0.9337	0.9143	0.8921	0.8670
0.51	0.9987	0.1000	0.9708	0.9535	0.9350	0.9156	0.8935	0.8686
0.89	-0.1000	-0.1000	-0.1000	0.9981	0.9859	0.9716	0.9547	0.9342
0.90	-0.1000	-0.1000	-0.1000	0.9996	0.9870	0.9737	0.9570	0.9368
0.91	-0.1000	-0.1000	-0.1000	0.9894	0.9758	0.9595	0.9395	0.9195
0.94	-0.1000	-0.1000	-0.1000	0.9952	0.9830	0.9680	0.9492	0.9292
0.95	-0.1000	-0.1000	-0.1000	0.9974	0.9857	0.9711	0.9531	0.9331
0.96	-0.1000	-0.1000	-0.1000	0.9997	0.9888	0.9748	0.9574	0.9374

* S.SIZE= 16 " Ramp case" AMU=2.30(i.e. PO= 0.01072) *

* QMIN x100:75.000075.000075.000075.000075.000050.000050.000050.000050.0000 *
* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 2.52 4.41 7.00 10.43 14.79 20.11 26.35 33.39 *

P[Q < T]TEST CRITERION ,T

0.01	0.8617	0.8629	0.8451	0.8273	0.8074	0.7826	0.7570	0.7292
0.02	0.8972	0.8807	0.8639	0.8457	0.8259	0.8024	0.7772	0.7496
0.03	0.9089	0.9063	0.8753	0.8572	0.8376	0.8146	0.7897	0.7624
0.04	0.9183	0.8985	0.8830	0.8657	0.8462	0.8236	0.7989	0.7718
0.05	0.9263	0.9052	0.8893	0.8726	0.8531	0.8308	0.8063	0.7794
0.06	0.9333	0.9109	0.8948	0.8780	0.8589	0.8369	0.8126	0.7858
0.49	-0.1000	0.9871	0.9783	0.9624	0.9455	0.9275	0.9073	0.8843
0.50	-0.1000	0.9884	0.9794	0.9636	0.9468	0.9288	0.9087	0.8857
0.51	-0.1000	0.9897	0.9806	0.9647	0.9480	0.9300	0.9100	0.8872
0.89	-0.1000	-0.1000	-0.1000	0.9928	0.9805	0.9659	0.9477	0.9250
0.90	-0.1000	-0.1000	-0.1000	0.9942	0.9823	0.9680	0.9500	0.9275
0.91	-0.1000	-0.1000	-0.1000	0.9957	0.9841	0.9698	0.9525	0.9300
0.94	-0.1000	-0.1000	-0.1000	0.9991	0.9881	0.9732	0.9561	0.9341
0.95	-0.1000	-0.1000	-0.1000	0.9974	0.9864	0.9711	0.9545	0.9325
0.96	-0.1000	-0.1000	-0.1000	0.9949	0.9839	0.9684	0.9514	0.9294

* S.SIZE= 16 " Ramp case" AMU=2.40(i.e. PO= 0.00820) *

* QMIN x100:75.000075.000075.000075.000075.000050.000050.000050.000050.0000 *
* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.5000 0.5000 0.5000 *
* P1 x 100: 2.03 3.64 5.26 8.86 12.75 17.59 23.38 30.03 *

P[Q < T]TEST CRITERION ,T

0.01	0.8929	0.8804	0.8624	0.8453	0.8265	0.8061	0.7808	0.7545
0.02	0.9108	0.8953	0.8796	0.8631	0.8445	0.8242	0.8000	0.7741
0.03	0.9237	0.9058	0.8895	0.8741	0.8558	0.8355	0.8119	0.7802
0.04	0.9339	0.9139	0.8971	0.8817	0.8640	0.8439	0.8206	0.7952
0.05	0.9389	0.9207	0.9033	0.8879	0.8706	0.8506	0.8277	0.8025
0.06	0.9429	0.9266	0.9086	0.8932	0.8759	0.8563	0.8336	0.8086
0.49	-0.1000	0.9967	0.1000	0.9719	0.9570	0.9405	0.9222	0.9013
0.50	-0.1000	0.9979	0.1000	0.9730	0.9582	0.9417	0.9235	0.9026
0.51	-0.1000	0.9991	0.1000	0.9740	0.9593	0.9429	0.9247	0.9039
0.89	-0.1000	-0.1000	-0.1000	0.9984	0.9878	0.9750	0.9594	0.9404
0.90	-0.1000	-0.1000	-0.1000	0.9998	0.9892	0.9760	0.9615	0.9425
0.91	-0.1000	-0.1000	-0.1000	0.9988	0.9882	0.9748	0.9592	0.9402
0.94	-0.1000	-0.1000	-0.1000	0.9999	0.9893	0.9759	0.9603	0.9413
0.95	-0.1000	-0.1000	-0.1000	0.9977	0.9871	0.9737	0.9581	0.9391
0.96	-0.1000	-0.1000	-0.1000	0.9957	0.9851	0.9717	0.9561	0.9371

* S.SIZE= 16 " Ramp case" AMU=2.50(i.e. PO= 0.00621) *

* QMIN x100:75.000075.000075.000075.000075.000050.000050.000050.000050.0000 *
* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.5000 0.5000 0.5000 *
* P1 x 100: 1.65 2.97 4.86 7.45 10.89 15.24 20.56 26.80 *

P[Q < T]TEST CRITERION ,T

0.01	0.9054	0.8919	0.8779	0.8622	0.8450	0.8257	0.8040	0.7781
0.02	0.9256	0.9080	0.8928	0.8788	0.8621	0.8431	0.8217	0.7968
0.03	0.9531	0.9190	0.9027	0.8886	0.8726	0.8539	0.8328	0.8084
0.04	0.9424	0.9274	0.9103	0.8959	0.8801	0.8618	0.8409	0.8169
0.05	0.9469	0.9344	0.9165	0.9019	0.8862	0.8682	0.8475	0.8238
0.06	0.9512	0.9382	0.9217	0.9069	0.8913	0.8735	0.8530	0.8296
0.49	-0.1000	0.1000	0.9900	0.9805	0.9668	0.9521	0.9354	0.9165
0.50	-0.1000	0.1000	0.9910	0.9812	0.9675	0.9528	0.9366	0.9177
0.51	-0.1000	0.1000	0.9920	0.9822	0.9682	0.9543	0.9377	0.9189
0.89	-0.1000	-0.1000	-0.1000	0.9938	0.9832	0.9688	0.9522	0.9332
0.90	-0.1000	-0.1000	-0.1000	0.9950	0.9844	0.9700	0.9534	0.9344
0.91	-0.1000	-0.1000	-0.1000	0.9963	0.9857	0.9713	0.9547	0.9357
0.94	-0.1000	-0.1000	-0.1000	0.9993	0.9887	0.9743	0.9577	0.9387
0.95	-0.1000	-0.1000	-0.1000	0.9977	0.9871	0.9727	0.9561	0.9371
0.96	-0.1000	-0.1000	-0.1000	0.9955	0.9849	0.9705	0.9539	0.9349

* S.SIZE= 16 " Ramp case" AMU=2.60(i.e. PO= 0.00466) *

* QMIN x100:87.500075.000075.000075.000075.000075.000075.000075.000075.0000 *
* SCALEx100: 0.1250 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 *
* P1 x 100: 1.32 2.41 3.99 6.21 9.21 13.10 17.94 23.73 *

P[Q < T]

Table with 10 columns and 16 rows of numerical data, representing test criteria for AMU=2.60.

* S.SIZE= 16 " Ramp case" AMU=2.70(i.e. PO= 0.00347) *

* QMIN x100:87.500087.500075.000075.000075.000075.000075.000075.000075.0000 *
* SCALEx100: 0.1250 0.1250 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 *
* P1 x 100: 1.04 1.93 3.25 5.13 7.73 11.16 15.52 20.84 *

P[Q < T]

Table with 10 columns and 16 rows of numerical data, representing test criteria for AMU=2.70.

* S.SIZE= 16 " Ramp case" AMU=2.80(i.e. PO= 0.00256) *

* QMIN x100:87.500087.500087.500075.000075.000075.000075.000075.000075.0000 *
* SCALEx100: 0.1250 0.1250 0.1250 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 *
* P1 x 100: 0.82 1.53 2.62 4.20 6.43 9.42 13.31 18.15 *

P[Q < T]

Table with 10 columns and 16 rows of numerical data, representing test criteria for AMU=2.80.

* S.SIZE= 16 " Ramp case" AMU=2.90(i.e. PO= 0.00187) *

* QMIN x100:87.500087.500087.500087.500075.000075.000075.000075.000075.0000 *
* SCALEx100: 0.1250 0.1250 0.1250 0.1250 0.2500 0.2500 0.2500 0.2500 0.2500 *
* P1 x 100: 0.63 1.20 2.09 3.41 5.20 7.89 11.32 15.68 *

P[Q < T]

Table with 10 columns and 16 rows of numerical data, representing test criteria for AMU=2.90.

* S.SIZE= 32 " Ramp case" AMU=1.40(i.e. PO= 0.00078) *

* QMIN x100:50.000050.000050.000050.000047.000044.000042.000038.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 10.33 16.12 22.78 30.13 37.94 45.91 53.72 61.07 *

P[Q < T]TEST CRITERION ,T

Table with 10 columns and 19 rows of numerical data, representing test results for AMU=1.40. Values range from approximately 0.49 to 0.96.

* S.SIZE= 32 " Ramp case" AMU=1.50(i.e. PO= 0.06681) *

* QMIN x100:50.000050.000050.000050.000049.000047.000044.000041.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 9.18 14.50 20.74 27.78 35.39 43.32 51.25 58.86 *

P[Q < T]TEST CRITERION ,T

Table with 10 columns and 19 rows of numerical data, representing test results for AMU=1.50. Values range from approximately 0.49 to 0.96.

* S.SIZE= 32 " Ramp case" AMU=1.60(i.e. PO= 0.05480) *

* QMIN x100:50.000050.000050.000050.000049.000047.000044.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 8.09 12.93 18.72 25.37 32.73 40.54 48.50 56.31 *

P[Q < T]TEST CRITERION ,T

Table with 10 columns and 19 rows of numerical data, representing test results for AMU=1.60. Values range from approximately 0.49 to 0.96.

* S.SIZE= 32 " Ramp case" AMU=1.70(i.e. PO= 0.04457) *

* QMIN x100:75.000050.000050.000050.000050.000050.000049.000046.0000 *
* SCALEx100: 0.2500 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 7.05 11.41 16.73 22.97 30.00 37.62 45.54 53.47 *

P[Q < T]TEST CRITERION ,T

Table with 10 columns and 19 rows of numerical data, representing test results for AMU=1.70. Values range from approximately 0.49 to 0.96.

* S.SIZE= 32 " Ramp case" AMU=1.80(i.e. PO= 0.03595) *

* QMIN x100:75.000075.000075.000050.000050.000050.000050.000048.0000 *

* SCALEx100: 0.2500 0.2500 0.2500 0.5000 0.5000 0.5000 0.5000 0.5000 *

* P1 x 100: 6.09 9.97 14.81 20.60 27.26 34.62 42.42 50.39 *

P[Q < T]TEST CRITERION ,T

0.01	0.8311	0.8108	0.7879	0.7625	0.7337	0.7188	0.6714	0.6384
0.02	0.8461	0.8259	0.8034	0.7783	0.7656	0.7198	0.6879	0.6548
0.03	0.8552	0.8354	0.8131	0.7881	0.7601	0.7301	0.6982	0.6651
0.04	0.8620	0.8424	0.8203	0.7955	0.7677	0.7377	0.7059	0.6728
0.05	0.8676	0.8480	0.8261	0.8014	0.7732	0.7439	0.7122	0.6790
0.06	0.8724	0.8527	0.8310	0.8064	0.7789	0.7492	0.7174	0.6843
0.49	0.9444	0.9258	0.9067	0.8851	0.8604	0.8329	0.8028	0.7707
0.50	0.9455	0.9269	0.9079	0.8863	0.8617	0.8342	0.8041	0.7720
0.51	0.9467	0.9279	0.9090	0.8875	0.8629	0.8355	0.8055	0.7734
0.89	-0.1000	0.9751	0.9570	0.9387	0.9173	0.8928	0.8652	0.8350
0.90	-0.1000	0.9767	0.9589	0.9408	0.9196	0.8952	0.8678	0.8377
0.91	-0.1000	0.9791	0.9609	0.9430	0.9220	0.8978	0.8705	0.8405
0.94	0.9946	0.9850	0.9680	0.9508	0.9305	0.9069	0.8802	0.8507
0.95	0.9970	0.9881	0.9705	0.9539	0.9340	0.9107	0.8842	0.8549
0.96	0.9996	0.9916	0.9741	0.9575	0.9380	0.9151	0.8889	0.8598

* S.SIZE= 32 " Ramp case" AMU=1.90(i.e. PO= 0.02872) *

* QMIN x100:75.000075.000075.000050.000050.000050.000050.000049.0000 *

* SCALEx100: 0.2500 0.2500 0.2500 0.5000 0.5000 0.5000 0.5000 0.5000 *

* P1 x 100: 5.20 8.64 12.99 18.31 24.55 31.59 39.20 47.13 *

P[Q < T]TEST CRITERION ,T

0.01	0.8524	0.8320	0.8111	0.7875	0.7613	0.7320	0.7012	0.6691
0.02	0.8660	0.8464	0.8258	0.8025	0.7766	0.7477	0.7171	0.6850
0.03	0.8744	0.8552	0.8350	0.8119	0.7862	0.7576	0.7271	0.6950
0.04	0.8804	0.8618	0.8418	0.8189	0.7933	0.7649	0.7345	0.7025
0.05	0.8854	0.8671	0.8472	0.8245	0.7991	0.7708	0.7405	0.7085
0.06	0.8896	0.8716	0.8518	0.8293	0.8040	0.7758	0.7456	0.7137
0.49	0.9571	0.9395	0.9225	0.9030	0.8806	0.8552	0.8270	0.7966
0.50	0.9581	0.9406	0.9235	0.9041	0.8818	0.8564	0.8283	0.7978
0.51	0.9591	0.9416	0.9245	0.9052	0.8829	0.8576	0.8295	0.7991
0.89	0.9929	-0.1000	0.9682	0.9521	0.9331	0.9110	0.8857	0.8575
0.90	0.9945	-0.1000	0.9700	0.9539	0.9352	0.9132	0.8880	0.8600
0.91	0.9961	0.9879	0.9721	0.9559	0.9373	0.9156	0.8906	0.8627
0.94	-0.1000	-0.1000	0.9790	0.9629	0.9450	0.9240	0.8996	0.8723
0.95	-0.1000	-0.1000	0.9818	0.9656	0.9462	0.9274	0.9033	0.8762
0.96	-0.1000	0.9944	-0.1000	0.9844	0.9651	0.9434	0.9176	0.8880

* S.SIZE= 32 " Ramp case" AMU=2.00(i.e. PO= 0.02275) *

* QMIN x100:75.000075.000075.000075.000075.000075.000074.500050.000050.000050.0000 *

* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.5000 0.5000 0.5000 *

* P1 x 100: 4.41 7.41 11.29 16.13 21.92 29.50 39.93 43.74 *

P[Q < T]TEST CRITERION ,T

0.01	0.8695	0.8530	0.8323	0.8106	0.7862	0.7592	0.7332	0.6984
0.02	0.8818	0.8660	0.8462	0.8249	0.8000	0.7741	0.7452	0.7138
0.03	0.8898	0.8740	0.8548	0.8338	0.8100	0.7835	0.7547	0.7235
0.04	0.8959	0.8799	0.8612	0.8404	0.8167	0.7904	0.7618	0.7307
0.05	0.9009	0.8848	0.8663	0.8457	0.8222	0.7960	0.7674	0.7365
0.06	0.9051	0.8889	0.8706	0.8501	0.8268	0.8007	0.7723	0.7415
0.49	0.9677	0.9518	0.9362	0.9189	0.8987	0.8755	0.8494	0.8207
0.50	0.9687	0.9527	0.9371	0.9199	0.8997	0.8766	0.8505	0.8219
0.51	0.9696	0.9536	0.9381	0.9209	0.9008	0.8777	0.8517	0.8231
0.89	0.9999	-0.1000	0.9785	0.9635	0.9468	0.9270	0.9041	0.8781
0.90	-0.1000	-0.1000	0.9802	0.9651	0.9487	0.9291	0.9063	0.8804
0.91	-0.1000	-0.1000	0.9820	0.9669	0.9507	0.9312	0.9086	0.8830
0.94	-0.1000	0.9961	0.9873	0.9733	0.9576	0.9389	0.9169	0.8919
0.95	-0.1000	0.9979	0.9896	0.9759	0.9603	0.9420	0.9203	0.8955
0.96	-0.1000	0.9997	0.9922	0.9788	0.9635	0.9456	0.9243	0.8998

* S.SIZE= 32 " Ramp case" AMU=2.10(i.e. PO= 0.01786) *

* QMIN x100:75.000075.000075.000075.000075.000075.000074.500050.000050.0000 *

* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.5000 0.5000 0.5000 *

* P1 x 100: 3.69 6.29 9.72 14.08 19.40 25.64 32.67 40.29 *

P[Q < T]TEST CRITERION ,T

0.01	0.8842	0.8698	0.8531	0.8318	0.8092	0.7919	0.7564	0.7269
0.02	0.8967	0.8819	0.8657	0.8453	0.8231	0.7983	0.7709	0.7416
0.03	0.9048	0.8895	0.8735	0.8536	0.8318	0.8071	0.7800	0.7507
0.04	0.9100	0.8953	0.8792	0.8598	0.8382	0.8138	0.7867	0.7576
0.05	0.9143	0.8999	0.8839	0.8648	0.8433	0.8191	0.7922	0.7631
0.06	0.9180	0.9039	0.8879	0.8690	0.8477	0.8236	0.7968	0.7678
0.49	0.9781	0.9621	0.9483	0.9328	0.9148	0.8937	0.8697	0.8430
0.50	0.9792	0.9630	0.9492	0.9337	0.9157	0.8948	0.8708	0.8442
0.51	0.9802	0.9638	0.9500	0.9346	0.9167	0.8958	0.8719	0.8453
0.89	-0.1000	0.9949	0.9865	0.9733	0.9586	0.9412	0.9205	0.8968
0.90	-0.1000	0.9961	0.9879	0.9749	0.9603	0.9430	0.9225	0.8989
0.91	-0.1000	0.9972	0.9894	0.9765	0.9620	0.9450	0.9247	0.9013
0.94	-0.1000	-0.1000	-0.1000	0.9821	0.9681	0.9518	0.9323	0.9095
0.95	-0.1000	-0.1000	0.9938	0.9844	0.9706	0.9546	0.9354	0.9129
0.96	-0.1000	-0.1000	0.9956	0.9866	0.9735	0.9578	0.9390	0.9168

* S.SIZE= 32 " Ramp case" AMU=2.20(i.e. PU= 0.01390) *

* QMIN x100:75.000075.000075.000075.000075.000075.000075.000074.000050.0000 *

* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.5000 *

* P1 x 100: 3.07 5.29 8.29 12.18 17.02 22.01 29.46 36.82 *

PG < T]TEST CRITERION ,T

Table with 10 columns and 17 rows of numerical data for AMU=2.20. Values range from -0.1000 to 0.9818.

* S.SIZE= 32 " Ramp case" AMU=2.30(i.e. PU= 0.01072) *

* QMIN x100:87.500075.000075.000075.000075.000075.000075.000074.500073.5000 *

* SCALEx100: 0.1250 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 *

* P1 x 100: 2.52 4.41 7.00 10.43 14.79 20.11 26.35 33.39 *

PG < T]TEST CRITERION ,T

Table with 10 columns and 17 rows of numerical data for AMU=2.30. Values range from -0.1000 to 0.9964.

* S.SIZE= 32 " Ramp case" AMU=2.40(i.e. PU= 0.00820) *

* QMIN x100:87.500087.500087.500075.000075.000075.000075.000075.000074.5000 *

* SCALEx100: 0.1250 0.1250 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 *

* P1 x 100: 2.05 3.04 5.06 8.06 12.75 17.59 23.38 30.03 *

PG < T]TEST CRITERION ,T

Table with 10 columns and 17 rows of numerical data for AMU=2.40. Values range from -0.1000 to 0.9998.

* S.SIZE= 32 " Ramp case" AMU=2.50(i.e. PU= 0.00621) *

* QMIN x100:87.500087.500087.500075.000075.000075.000075.000075.000075.0000 *

* SCALEx100: 0.1250 0.1250 0.1250 0.2500 0.2500 0.2500 0.2500 0.2500 *

* P1 x 100: 1.65 2.97 4.86 7.45 10.89 15.24 20.56 26.80 *

PG < T]TEST CRITERION ,T

Table with 10 columns and 17 rows of numerical data for AMU=2.50. Values range from -0.1000 to 0.9970.

* S.SIZE= 32 " Ramp case" AMU=2.60(i.e. PO= 0.00466) *

* QMIN x100:87.500087.500087.500087.500087.500075.000075.000075.0000 *
* SCALEx100: 0.1250 0.1250 0.1250 0.1250 0.2500 0.2500 0.2500 0.2500 *
* P1 x 100: 1.32 2.41 3.99 6.21 9.21 13.10 17.94 23.73 *

PEQ < T]TEST CRITERION ,T
0.01 0.9421 0.9330 0.9230 0.9111 0.8970 0.8811 0.8628 0.8420
0.02 0.9501 0.9411 0.9322 0.9204 0.9070 0.8916 0.8736 0.8531
0.03 0.9560 0.9462 0.9376 0.9262 0.9132 0.8981 0.8804 0.8600
0.04 0.9606 0.9502 0.9453 0.9305 0.9178 0.9029 0.8854 0.8652
0.05 0.9645 0.9534 0.9446 0.9340 0.9214 0.9067 0.8894 0.8694
0.06 0.9678 0.9563 0.9473 0.9368 0.9245 0.9099 0.8928 0.8729
0.49 -0.1000-0.1000 0.9880 0.9791 0.9692 0.9578 0.9440 0.9275
0.50 -0.1000-0.1000 0.9885 0.9797 0.9698 0.9585 0.9448 0.9283
0.51 -0.1000-0.1000 0.9891 0.9802 0.9704 0.9592 0.9455 0.9291
0.89 -0.1000-0.1000-0.1000 1.0000 0.9938 0.9862 0.9759 0.9629
0.90 -0.1000-0.1000-0.1000-0.1000 0.9946 0.9871 0.9770 0.9643
0.91 -0.1000-0.1000-0.1000-0.1000 0.9954 0.9882 0.9783 0.9657
0.94 -0.1000-0.1000-0.1000-0.1000 0.9979 0.9916 0.9824 0.9706
0.95 -0.1000-0.1000-0.1000-0.1000 0.9989 0.9926 0.9841 0.9726
0.96 -0.1000-0.1000-0.1000-0.1000 0.9998 0.9941 0.9859 0.9749

* S.SIZE= 32 " Ramp case" AMU=2.70(i.e. PO= 0.00347) *

* QMIN x100:87.500087.500087.500087.500087.500075.000075.000075.0000 *
* SCALEx100: 0.1250 0.1250 0.1250 0.1250 0.1250 0.2500 0.2500 0.2500 *
* P1 x 100: 1.04 1.93 3.25 5.13 7.73 11.16 15.52 20.84 *

PEQ < T]TEST CRITERION ,T
0.01 0.9485 0.9416 0.9325 0.9227 0.9141 0.8952 0.8785 0.8592
0.02 0.9577 0.9531 0.9406 0.9314 0.9192 0.9050 0.8888 0.8699
0.03 0.9640 0.9544 0.9456 0.9367 0.9248 0.9111 0.8951 0.8765
0.04 0.9684 0.9585 0.9493 0.9404 0.9290 0.9155 0.8998 0.8814
0.05 0.9703 0.9617 0.9524 0.9435 0.9323 0.9191 0.9036 0.8854
0.06 0.9723 0.9645 0.9550 0.9462 0.9351 0.9221 0.9067 0.8887
0.49 -0.1000 0.9983 0.9925 0.9847 0.9761 0.9660 0.9540 0.9393
0.50 -0.1000 0.9989 0.9930 0.9852 0.9767 0.9666 0.9546 0.9400
0.51 -0.1000 0.9994 0.9935 0.9857 0.9772 0.9672 0.9553 0.9408
0.89 -0.1000-0.1000-0.1000-0.1000 0.9973 0.9910 0.9824 0.9713
0.90 -0.1000-0.1000-0.1000-0.1000 0.9979 0.9919 0.9834 0.9725
0.91 -0.1000-0.1000-0.1000-0.1000 0.9985 0.9925 0.9845 0.9738
0.94 -0.1000-0.1000-0.1000-0.1000 0.9992 0.9930 0.9880 0.9781
0.95 -0.1000-0.1000-0.1000-0.1000 0.9996 0.9934 0.9894 0.9798
0.96 -0.1000-0.1000-0.1000-0.1000 0.9997 0.9910 0.9818

* S.SIZE= 32 " Ramp case" AMU=2.80(i.e. PO= 0.00250) *

* QMIN x100:93.750087.500087.500087.500087.500087.500075.000075.0000 *
* SCALEx100: 0.0630 0.1250 0.1250 0.1250 0.1250 0.2500 0.2500 *
* P1 x 100: 0.82 1.53 2.62 4.20 6.43 9.42 13.31 18.15 *

PEQ < T]TEST CRITERION ,T
0.01 0.9556 0.9481 0.9404 0.9320 0.9256 0.9084 0.8928 0.8728
0.02 0.9657 0.9562 0.9480 0.9399 0.9308 0.9173 0.9024 0.8852
0.03 0.9698 0.9616 0.9529 0.9448 0.9354 0.9229 0.9083 0.8915
0.04 0.9723 0.9656 0.9565 0.9485 0.9391 0.9269 0.9127 0.8961
0.05 0.9766 0.9684 0.9595 0.9514 0.9421 0.9302 0.9162 0.8998
0.06 0.9768 0.9700 0.9620 0.9539 0.9447 0.9329 0.9191 0.9029
0.49 -0.1000-0.1000-0.1000 0.9893 0.9818 0.9731 0.9625 0.9497
0.50 -0.1000-0.1000-0.1000 0.9898 0.9823 0.9736 0.9631 0.9503
0.51 -0.1000-0.1000-0.1000 0.9902 0.9828 0.9742 0.9637 0.9510
0.89 -0.1000-0.1000-0.1000-0.1000 0.9949 0.9877 0.9784
0.90 -0.1000-0.1000-0.1000-0.1000 0.9955 0.9886 0.9794
0.91 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9955 0.9886 0.9794
0.94 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9982 0.9924 0.9843
0.95 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9990 0.9935 0.9857
0.96 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9999 0.9948 0.9874

* S.SIZE= 32 " Ramp case" AMU=2.90(i.e. PO= 0.00187) *

* QMIN x100:93.750093.750087.500087.500087.500087.500087.500075.0000 *
* SCALEx100: 0.0630 0.0630 0.1250 0.1250 0.1250 0.1250 0.2500 *
* P1 x 100: 0.63 1.20 2.09 3.41 5.29 7.89 11.32 15.68 *

PEQ < T]TEST CRITERION ,T
0.01 0.9654 0.9547 0.9480 0.9400 0.9311 0.9203 0.9102 0.8897
0.02 0.9703 0.9631 0.9555 0.9475 0.9389 0.9285 0.9149 0.8991
0.03 0.9734 0.9684 0.9603 0.9521 0.9437 0.9375 0.9203 0.9049
0.04 0.9762 0.9704 0.9639 0.9556 0.9473 0.9372 0.9243 0.9093
0.05 0.9787 0.9726 0.9668 0.9584 0.9501 0.9402 0.9275 0.9127
0.06 0.9810 0.9745 0.9685 0.9607 0.9525 0.9427 0.9302 0.9156
0.49 -0.1000-0.1000 0.9987 0.9932 0.9866 0.9791 0.9699 0.9586
0.50 -0.1000-0.1000 0.9991 0.9936 0.9871 0.9796 0.9704 0.9592
0.51 -0.1000-0.1000 0.9995 0.9940 0.9875 0.9800 0.9710 0.9598
0.89 -0.1000-0.1000-0.1000-0.1000 0.9976 0.9920 0.9842
0.90 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9982 0.9927 0.9851
0.91 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9987 0.9935 0.9861
0.94 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9999 0.9959 0.9893
0.95 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9997 0.9905
0.96 -0.1000-0.1000-0.1000-0.1000-0.1000 0.9977 0.9919

* S.SIZE= 64 " Ramp case" AMU= .40(i.e. PU= 0.34450) *

* QMIN x100:30.000027.000023.000020.000017.000014.000011.0000 9.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 19.52 27.33 34.69 41.35 47.14 51.92 55.86 58.86 *

PEQ < T]TEST CRITERION ,T

Table with 10 columns and 18 rows of numerical data for S.SIZE=64, AMU=0.40. Values range from 0.01 to 0.96 across the rows.

* S.SIZE= 64 " Ramp case" AMU= .50(i.e. PU= 0.30854) *

* QMIN x100:34.000030.000027.000023.000020.000017.000014.000012.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 19.15 27.07 34.69 41.72 47.96 53.28 57.64 61.07 *

PEQ < T]TEST CRITERION ,T

Table with 10 columns and 18 rows of numerical data for S.SIZE=64, AMU=0.50. Values range from 0.01 to 0.96 across the rows.

* S.SIZE= 64 " Ramp case" AMU= .60(i.e. PU= 0.27423) *

* QMIN x100:37.000034.000030.000027.000023.000020.000017.000014.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 18.59 26.56 34.37 41.72 48.37 54.17 59.01 62.89 *

PEQ < T]TEST CRITERION ,T

Table with 10 columns and 18 rows of numerical data for S.SIZE=64, AMU=0.60. Values range from 0.01 to 0.96 across the rows.

* S.SIZE= 64 " Ramp case" AMU= .70(i.e. PU= 0.24196) *

* QMIN x100:41.000037.000034.000030.000027.000023.000020.000017.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 17.88 25.80 33.73 41.35 48.78 54.62 59.94 64.50 *

PEQ < T]TEST CRITERION ,T

Table with 10 columns and 18 rows of numerical data for S.SIZE=64, AMU=0.70. Values range from 0.01 to 0.96 across the rows.

* S.SIZE= 64 " Ramp case" AMU= .80(i.e. PD= 0.21188) *

* QMIN x100: 44.000040.000037.000034.000030.000027.000023.000020.0000 *
 * SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
 * P1 x 100: 17.02 24.83 32.80 40.61 47.96 54.62 61.41 65.25 *

PER < T]TEST CRITERION ,T

0.01	0.5800	0.5441	0.5078	0.4718	0.4368	0.4034	0.3721	0.3432
0.02	0.5953	0.5592	0.5226	0.4862	0.4507	0.4168	0.3848	0.3553
0.03	0.6049	0.5688	0.5320	0.4954	0.4596	0.4253	0.3929	0.3630
0.04	0.6122	0.5760	0.5391	0.5023	0.4662	0.4317	0.3991	0.3688
0.05	0.6181	0.5818	0.5448	0.5079	0.4717	0.4369	0.4040	0.3735
0.06	0.6232	0.5868	0.5575	0.5126	0.4763	0.4413	0.4083	0.3775
0.49	0.7066	0.6698	0.6318	0.5931	0.5546	0.5170	0.4810	0.4469
0.50	0.7079	0.6712	0.6331	0.5944	0.5559	0.5183	0.4822	0.4480
0.51	0.7092	0.6725	0.6344	0.5958	0.5572	0.5195	0.4834	0.4492
0.89	0.7714	0.7351	0.6970	0.6577	0.6190	0.5788	0.5407	0.5043
0.90	0.7742	0.7379	0.6998	0.6605	0.6208	0.5815	0.5433	0.5068
0.91	0.7771	0.7409	0.7028	0.6635	0.6238	0.5844	0.5462	0.5096
0.94	0.7878	0.7517	0.7136	0.6743	0.6348	0.5949	0.5563	0.5194
0.95	0.7922	0.7562	0.7182	0.6788	0.6389	0.5993	0.5606	0.5235
0.96	0.7974	0.7615	0.7235	0.6841	0.6442	0.6045	0.5657	0.5284

* S.SIZE= 64 " Ramp case" AMU= .90(i.e. PD= 0.18406) *

* QMIN x100: 46.000043.000040.000037.000033.000030.000027.000023.0000 *
 * SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
 * P1 x 100: 16.05 23.67 31.59 39.52 47.14 54.17 61.41 65.73 *

PER < T]TEST CRITERION ,T

0.01	0.6169	0.5818	0.5459	0.5098	0.4741	0.4397	0.4071	0.3766
0.02	0.6397	0.5967	0.5606	0.5241	0.4881	0.4532	0.4200	0.3889
0.03	0.6413	0.6061	0.5698	0.5332	0.4969	0.4617	0.4282	0.3967
0.04	0.6485	0.6132	0.5768	0.5400	0.5036	0.4682	0.4343	0.4026
0.05	0.6542	0.6189	0.5825	0.5456	0.5090	0.4734	0.4394	0.4074
0.06	0.6591	0.6238	0.5873	0.5503	0.5136	0.4779	0.4437	0.4115
0.49	0.7398	0.7047	0.6678	0.6298	0.5914	0.5535	0.5166	0.4815
0.50	0.7411	0.7060	0.6691	0.6310	0.5927	0.5547	0.5178	0.4826
0.51	0.7424	0.7073	0.6704	0.6323	0.5939	0.5560	0.5190	0.4838
0.89	0.8020	0.7677	0.7311	0.6929	0.6538	0.6147	0.5762	0.5390
0.90	0.8046	0.7703	0.7338	0.6956	0.6565	0.6173	0.5788	0.5416
0.91	0.8074	0.7732	0.7367	0.6985	0.6594	0.6202	0.5816	0.5443
0.94	0.8175	0.7836	0.7472	0.7090	0.6699	0.6305	0.5917	0.5541
0.95	0.8218	0.7879	0.7514	0.7134	0.6743	0.6349	0.5960	0.5582
0.96	0.8267	0.7929	0.7567	0.7186	0.6794	0.6400	0.6009	0.5631

* S.SIZE= 64 " Ramp case" AMU= 1.00(i.e. PD= 0.15826) *

* QMIN x100: 49.000046.000043.000040.000037.000033.000030.000027.0000 *
 * SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
 * P1 x 100: 14.99 22.54 30.15 38.12 45.93 53.28 59.94 65.73 *

PER < T]TEST CRITERION ,T

0.01	0.6524	0.6185	0.5832	0.5473	0.5114	0.4763	0.4425	0.4104
0.02	0.6670	0.6330	0.5976	0.5615	0.5253	0.4897	0.4555	0.4231
0.03	0.6762	0.6422	0.6068	0.5705	0.5341	0.4983	0.4637	0.4310
0.04	0.6831	0.6491	0.6136	0.5772	0.5406	0.5047	0.4699	0.4369
0.05	0.6887	0.6547	0.6192	0.5827	0.5461	0.5099	0.4750	0.4418
0.06	0.6934	0.6594	0.6239	0.5874	0.5506	0.5144	0.4793	0.4459
0.49	0.7711	0.7378	0.7023	0.6653	0.6277	0.5905	0.5522	0.5168
0.50	0.7723	0.7390	0.7035	0.6665	0.6286	0.5907	0.5534	0.5174
0.51	0.7735	0.7403	0.7048	0.6678	0.6299	0.5919	0.5546	0.5193
0.89	0.8302	0.7981	0.7634	0.7266	0.6888	0.6497	0.6112	0.5736
0.90	0.8327	0.8007	0.7660	0.7292	0.6911	0.6524	0.6138	0.5761
0.91	0.8354	0.8034	0.7688	0.7320	0.6939	0.6552	0.6166	0.5788
0.94	0.8449	0.8133	0.7788	0.7422	0.7041	0.6653	0.6265	0.5885
0.95	0.8489	0.8174	0.7830	0.7464	0.7084	0.6695	0.6307	0.5926
0.96	0.8535	0.8221	0.7879	0.7514	0.7134	0.6745	0.6356	0.5976

* S.SIZE= 64 " Ramp case" AMU= 1.10(i.e. PD= 0.13567) *

* QMIN x100: 50.000048.000046.000043.000040.000036.000033.000030.0000 *
 * SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
 * P1 x 100: 13.26 20.89 28.51 36.43 44.36 51.98 59.01 65.25 *

PER < T]TEST CRITERION ,T

0.01	0.6862	0.6537	0.6194	0.5840	0.5482	0.5127	0.4772	0.4452
0.02	0.7003	0.6679	0.6335	0.5980	0.5620	0.5261	0.4912	0.4577
0.03	0.7092	0.6768	0.6424	0.6068	0.5706	0.5346	0.4994	0.4656
0.04	0.7159	0.6835	0.6491	0.6135	0.5772	0.5410	0.5056	0.4716
0.05	0.7212	0.6889	0.6545	0.6188	0.5825	0.5462	0.5106	0.4765
0.06	0.7258	0.6935	0.6591	0.6234	0.5870	0.5506	0.5149	0.4806
0.49	0.8001	0.7689	0.7351	0.6993	0.6623	0.6247	0.5874	0.5508
0.50	0.8013	0.7701	0.7363	0.7006	0.6635	0.6259	0.5885	0.5520
0.51	0.8025	0.7713	0.7375	0.7018	0.6647	0.6271	0.5897	0.5531
0.89	0.8560	0.8263	0.7936	0.7586	0.7217	0.6838	0.6455	0.6077
0.90	0.8583	0.8287	0.7961	0.7611	0.7242	0.6863	0.6480	0.6102
0.91	0.8608	0.8313	0.7988	0.7638	0.7270	0.6890	0.6508	0.6128
0.94	0.8698	0.8406	0.8084	0.7736	0.7368	0.6989	0.6605	0.6225
0.95	0.8735	0.8445	0.8123	0.7776	0.7410	0.7030	0.6646	0.6265
0.96	0.8778	0.8490	0.8170	0.7824	0.7458	0.7079	0.6694	0.6312

* S.SIZE= 64 " Ramp case" AMU=1.20(i.e. PO= 0.11507) *

* QMIN x100:50.000050.000048.000045.000042.000039.000036.000033.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 12.69 19.35 26.70 34.51 42.42 50.28 57.64 64.30 *

P[Q < T]TEST CRITERION ,T

Table with 9 columns and 17 rows of numerical data for the first 'Ramp case'.

* S.SIZE= 64 " Ramp case" AMU=1.30(i.e. PO= 0.09680) *

* QMIN x100:50.000050.000049.000047.000045.000042.000039.000036.0000 *
* SCALEx100: 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 11.51 17.75 24.78 32.39 40.32 48.25 55.86 62.89 *

P[Q < T]TEST CRITERION ,T

Table with 9 columns and 17 rows of numerical data for the second 'Ramp case'.

* S.SIZE= 64 " Ramp case" AMU=1.40(i.e. PO= 0.08070) *

* QMIN x100:73.000071.000050.000050.000047.000044.000042.000038.0000 *
* SCALEx100: 0.2500 0.2500 0.5000 0.5000 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 10.33 16.12 22.73 30.13 37.96 45.91 53.72 61.07 *

P[Q < T]TEST CRITERION ,T

Table with 9 columns and 17 rows of numerical data for the third 'Ramp case'.

* S.SIZE= 64 " Ramp case" AMU=1.50(i.e. PO= 0.06621) *

* QMIN x100:74.500073.000070.500068.000049.000047.000044.000041.0000 *
* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.5000 0.5000 0.5000 0.5000 *
* P1 x 100: 9.18 14.50 20.74 27.78 35.35 43.32 51.25 58.86 *

P[Q < T]TEST CRITERION ,T

Table with 9 columns and 17 rows of numerical data for the fourth 'Ramp case'.


```
* S.SIZE= 64      " Ramp case"      AMU=1.60(i.e. PD= 0.05487) *
*****
* QMIN x100:75.000074.000072.500070.500067.500065.000064.000064.0000 *
* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 *
* P1 x 100:   8.09  12.93  18.72  25.37  32.73  40.54  48.50  56.31 *
*****
PE[ < T ]      .....TEST CRITERION ,T .....

0.01      0.8251 0.8023 0.7797 0.7475 0.7167 0.6841 0.6503 0.6159
0.02      0.8398 0.8135 0.7914 0.7593 0.7286 0.6961 0.6622 0.6277
0.03      0.8428 0.8205 0.7948 0.7667 0.7361 0.7036 0.6698 0.6352
0.04      0.8479 0.8257 0.8002 0.7722 0.7417 0.7093 0.6754 0.6408
0.05      0.8520 0.8300 0.8046 0.7767 0.7463 0.7139 0.6800 0.6454
0.06      0.8555 0.8335 0.8083 0.7805 0.7501 0.7177 0.6839 0.6492
0.49      0.9104 0.8906 0.8677 0.8418 0.8129 0.7816 0.7483 0.7136
0.50      0.9112 0.8915 0.8687 0.8427 0.8139 0.7826 0.7493 0.7147
0.51      0.9121 0.8924 0.8696 0.8437 0.8149 0.7836 0.7503 0.7157
0.89      0.9490 0.9314 0.9108 0.8870 0.8600 0.8302 0.7979 0.7639
0.90      0.9505 0.9330 0.9126 0.8889 0.8620 0.8322 0.8000 0.7660
0.91      0.9522 0.9348 0.9145 0.8909 0.8641 0.8344 0.8023 0.7683
0.94      0.9582 0.9410 0.9212 0.8980 0.8716 0.8423 0.8104 0.7766
0.95      0.9607 0.9436 0.9239 0.9010 0.8748 0.8455 0.8126 0.7800
0.96      0.9635 0.9465 0.9272 0.9044 0.8784 0.8494 0.8177 0.7841
```

```
* S.SIZE= 64      " Ramp case"      AMU=1.70(i.e. PD= 0.04457) *
*****
* QMIN x100:75.000075.000074.000072.000070.000067.000064.500061.0000 *
* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 *
* P1 x 100:   7.05  11.41  16.73  22.97  30.00  37.62  45.54  53.47 *
*****
PE[ < T ]      .....TEST CRITERION ,T .....

0.01      0.8463 0.8253 0.8017 0.7786 0.7456 0.7143 0.6816 0.6478
0.02      0.8565 0.8398 0.8126 0.7859 0.7570 0.7259 0.6932 0.6593
0.03      0.8629 0.8426 0.8194 0.7930 0.7642 0.7352 0.7005 0.6666
0.04      0.8677 0.8475 0.8245 0.7982 0.7696 0.7386 0.7059 0.6721
0.05      0.8715 0.8515 0.8286 0.8025 0.7739 0.7430 0.7104 0.6765
0.06      0.8747 0.8549 0.8321 0.8061 0.7776 0.7468 0.7141 0.6803
0.49      0.9257 0.9081 0.8876 0.8639 0.8372 0.8078 0.7761 0.7427
0.50      0.9265 0.9090 0.8923 0.8648 0.8381 0.8087 0.7771 0.7437
0.51      0.9273 0.9098 0.8893 0.8657 0.8391 0.8097 0.7780 0.7446
0.89      0.9612 0.9454 0.9273 0.9059 0.8815 0.8537 0.8234 0.7909
0.90      0.9626 0.9469 0.9289 0.9077 0.8832 0.8556 0.8254 0.7929
0.91      0.9641 0.9485 0.9307 0.9095 0.8851 0.8577 0.8275 0.7951
0.94      0.9695 0.9541 0.9368 0.9161 0.8921 0.8651 0.8352 0.8030
0.95      0.9720 0.9565 0.9393 0.9188 0.8950 0.8681 0.8384 0.8063
0.96      0.9748 0.9591 0.9422 0.9220 0.8984 0.8717 0.8421 0.8102
```

```
* S.SIZE= 64      " Ramp case"      AMU=1.80(i.e. PD= 0.03593) *
*****
* QMIN x100:75.000075.000074.500073.500071.500069.500066.500063.5000 *
* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 *
* P1 x 100:   6.09   9.97  14.81  20.60  27.20  34.62  42.42  50.39 *
*****
PE[ < T ]      .....TEST CRITERION ,T .....

0.01      0.8651 0.8464 0.8247 0.8002 0.7720 0.7429 0.7113 0.6784
0.02      0.8748 0.8564 0.8350 0.8108 0.7833 0.7540 0.7226 0.6936
0.03      0.8808 0.8626 0.8414 0.8174 0.7904 0.7610 0.7296 0.6967
0.04      0.8853 0.8711 0.8462 0.8224 0.7955 0.7662 0.7349 0.7021
0.05      0.8889 0.8709 0.8501 0.8264 0.7996 0.7704 0.7392 0.7064
0.06      0.8919 0.8741 0.8534 0.8298 0.8031 0.7740 0.7428 0.7100
0.49      0.9391 0.9235 0.9052 0.8838 0.8594 0.8320 0.8021 0.7701
0.50      0.9398 0.9243 0.9060 0.8847 0.8602 0.8329 0.8030 0.7711
0.51      0.9405 0.9250 0.9068 0.8855 0.8611 0.8338 0.8040 0.7720
0.89      0.9716 0.9575 0.9417 0.9227 0.9005 0.8751 0.8469 0.8162
0.90      0.9733 0.9588 0.9431 0.9243 0.9022 0.8769 0.8488 0.8181
0.91      0.9745 0.9605 0.9447 0.9260 0.9040 0.8788 0.8506 0.8202
0.94      0.9797 0.9653 0.9502 0.9320 0.9104 0.8857 0.8580 0.8277
0.95      0.9816 0.9673 0.9524 0.9344 0.9131 0.8886 0.8610 0.8308
0.96      0.9840 0.9697 0.9550 0.9373 0.9162 0.8919 0.8645 0.8345
```

```
* S.SIZE= 64      " Ramp case"      AMU=1.90(i.e. PD= 0.02872) *
*****
* QMIN x100:75.000075.000075.000074.500073.000071.000069.000066.0000 *
* SCALEx100: 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 *
* P1 x 100:   5.20   8.64  12.99  18.31  24.55  31.59  39.20  47.13 *
*****
PE[ < T ]      .....TEST CRITERION ,T .....

0.01      0.8834 0.8653 0.8458 0.8270 0.7979 0.7697 0.7396 0.7078
0.02      0.8921 0.8747 0.8594 0.8332 0.8082 0.7842 0.7564 0.7225
0.03      0.8975 0.8805 0.8615 0.8395 0.8147 0.7870 0.7571 0.7255
0.04      0.9016 0.8848 0.8660 0.8442 0.8195 0.7920 0.7622 0.7306
0.05      0.9049 0.8883 0.8696 0.8479 0.8234 0.7993 0.7663 0.7348
0.06      0.9076 0.8913 0.8727 0.8511 0.8267 0.7994 0.7698 0.7383
0.49      0.9507 0.9369 0.9208 0.9016 0.8794 0.8542 0.8262 0.7959
0.50      0.9513 0.9376 0.9215 0.9024 0.8802 0.8550 0.8271 0.7968
0.51      0.9519 0.9383 0.9222 0.9032 0.8810 0.8559 0.8280 0.7977
0.89      0.9806 0.9677 0.9539 0.9373 0.9214 0.8945 0.8684 0.8396
0.90      0.9818 0.9689 0.9553 0.9388 0.9190 0.8961 0.8702 0.8415
0.91      0.9830 0.9702 0.9567 0.9442 0.9207 0.8979 0.8721 0.8435
0.94      -0.1060 0.9747 0.9616 0.9457 0.9266 0.9043 0.8788 0.8505
0.95      -0.9894 0.9805 0.9636 0.9479 0.9290 0.9069 0.8816 0.8535
0.96      -0.1060 0.9787 0.9659 0.9505 0.9319 0.9099 0.8849 0.8569
```

* S.SIZE= 64 " Ramp case" AMU=2.00(i.e. PO= 0.02275) *

* QMIN x100:87.500075.000075.000075.000075.000074.500072.500070.0000 *
* SCALEx100: 0.1250 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 *
* P1 x 100: 4.41 7.41 11.29 16.13 21.92 28.58 35.93 43.74 *

PEQ < T]TEST CRITERION ,T

Table with 10 columns of numerical values representing test criteria for AMU=2.00. Values range from approximately -0.1000 to 0.9975.

* S.SIZE= 64 " Ramp case" AMU=2.10(i.e. PO= 0.01786) *

* QMIN x100:87.500087.500075.000075.000075.000074.500072.500070.0000 *
* SCALEx100: 0.1250 0.1250 0.2500 0.2500 0.2500 0.2500 0.2500 0.2500 *
* P1 x 100: 3.69 6.29 9.72 14.08 19.40 25.64 32.67 40.29 *

PEQ < T]TEST CRITERION ,T

Table with 10 columns of numerical values representing test criteria for AMU=2.10. Values range from approximately -0.1000 to 0.9981.

* S.SIZE= 64 " Ramp case" AMU=2.20(i.e. PO= 0.01390) *

* QMIN x100:87.500087.500087.500087.500075.000075.000074.000072.0000 *
* SCALEx100: 0.1250 0.1250 0.1250 0.2500 0.2500 0.2500 0.2500 0.2500 *
* P1 x 100: 3.07 5.29 8.29 12.18 17.02 22.81 29.46 36.82 *

PEQ < T]TEST CRITERION ,T

Table with 10 columns of numerical values representing test criteria for AMU=2.20. Values range from approximately -0.1000 to 0.9977.

* S.SIZE= 64 " Ramp case" AMU=2.30(i.e. PO= 0.01072) *

* QMIN x100:87.500087.500087.500087.500075.000075.000074.500073.5000 *
* SCALEx100: 0.1250 0.1250 0.1250 0.1250 0.2500 0.2500 0.2500 0.2500 *
* P1 x 100: 2.52 4.41 7.00 10.43 14.79 20.11 26.35 33.39 *

PEQ < T]TEST CRITERION ,T

Table with 10 columns of numerical values representing test criteria for AMU=2.30. Values range from approximately -0.1000 to 0.9977.

 * S. SIZE = 64
 ** Ramp case**
 AMU=2.4011.e- PO=0.00063 *

 * GMIN X100:86.875096.875093.750093.750093.750093.750093.750093 *
 * SCALEX100: 0.0310 0.0310 0.0310 0.0310 0.0310 0.0310 0.0310 0.0310 *
 * P1 X 100: 0.15 0.31 0.59 1.04 1.75 2.84 4.42 6.65 *

 PLO < T]TEST CRITERION / T
 0.01 0.9842 0.9842 0.9758 0.9722 0.9670 0.9609 0.9526 0.9425
 0.02 0.9861 0.9842 0.9756 0.9758 0.9708 0.9649 0.9569 0.9472
 0.03 0.9851 0.9819 0.9780 0.9731 0.9673 0.9596 0.9501
 0.04 0.9892 0.9863 0.9836 0.9796 0.9748 0.9671 0.9574
 0.05 0.9905 0.9874 0.9845 0.9809 0.9762 0.9706 0.9632 0.9540
 0.06 0.9917 0.9883 0.9854 0.9820 0.9773 0.9718 0.9645 0.9555
 0.49 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.51 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.55 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.89 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.90 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.91 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.94 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.95 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.96 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998

 * S. SIZE = 64
 ** Ramp case**
 AMU=3.3011.e- PO=0.00063 *

 * GMIN X100:86.875096.875093.750093.750093.750093.750093.750093 *
 * SCALEX100: 0.0310 0.0310 0.0310 0.0310 0.0310 0.0310 0.0310 0.0310 *
 * P1 X 100: 0.21 0.42 0.77 1.34 2.23 3.54 5.43 8.03 *

 PLO < T]TEST CRITERION / T
 0.01 0.9854 0.9838 0.9792 0.9758 0.9718 0.9661 0.9594 0.9504
 0.02 0.9877 0.9854 0.9833 0.9792 0.9748 0.9707 0.9633 0.9547
 0.03 0.9896 0.9870 0.9845 0.9813 0.9770 0.9720 0.9657 0.9574
 0.04 0.9912 0.9883 0.9857 0.9828 0.9786 0.9737 0.9675 0.9593
 0.05 0.9926 0.9894 0.9867 0.9840 0.9799 0.9751 0.9689 0.9609
 0.06 0.9939 0.9904 0.9876 0.9847 0.9809 0.9762 0.9701 0.9622
 0.49 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.51 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.55 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.89 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.90 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.91 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.94 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.95 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.96 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998

 * S. SIZE = 64
 ** Ramp case**
 AMU=5.2011.e- PO=0.00063 *

 * GMIN X100:86.875096.875093.750093.750093.750093.750093.750093 *
 * SCALEX100: 0.0310 0.0310 0.0310 0.0310 0.0310 0.0310 0.0310 0.0310 *
 * P1 X 100: 0.23 0.55 1.00 1.72 2.90 4.39 6.61 9.61 *

 PLO < T]TEST CRITERION / T
 0.01 0.9843 0.9803 0.9760 0.9722 0.9670 0.9609 0.9526 0.9425
 0.02 0.9861 0.9842 0.9756 0.9758 0.9708 0.9649 0.9569 0.9472
 0.03 0.9851 0.9819 0.9780 0.9731 0.9673 0.9596 0.9501
 0.04 0.9892 0.9863 0.9836 0.9796 0.9748 0.9671 0.9574
 0.05 0.9905 0.9874 0.9845 0.9809 0.9762 0.9706 0.9632 0.9540
 0.06 0.9917 0.9883 0.9854 0.9820 0.9773 0.9718 0.9645 0.9555
 0.49 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.51 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.55 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.89 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.90 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.91 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.94 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.95 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998
 0.96 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998 0.9998

Appendix C. C.2-2

Tables to show Equivalence results and robustness under the Uniform Model

The tables below give the parameters for the four equivalent schemes . Each of these four schemes is shown on a row in the tables .The Ramp case is given on the first row where for a given E value the first entry is an integer which indicates that a plan "exists" if the integer value is 1 and "non-existent" if the value is 0 . Of course with "non-existence" there are no reported equivalents and this shows clearly in the tables . The other entries are the Ramp sample size , the E value , the test criterion t , and p0(2) value of the proportion defective of the second equivalence point , in that order .

On the second row we have the parameters for the equivalent two-class attribute case . Its first entry is the n₉₅ (the sample size that satisfies equality in (5.1.) in Chapter (V)) . The second entry is n₅₀ satisfying the equality in the inequality (5.2.) . The last entry on the row is the attribute acceptance number , c .

The third row gives the sample size and the test criterion for the S-plan . The fourth row gives them in the case of G-plan .

For conservation of space the robustness for the Uniform model is also reported on the right side columns of the following tables .

For AQL= 0.01072 (at 95%) :

=====

				Uniform-Robustness	
				Pa	ROB
				----	----
"Ramp":	4	P= 0.50	T= *	*	*
		(" Non-Existent ")			
"Ramp":	4	P= 0.70	T= 0.2498	0.6752	(7.243)
"Attr":	17	73	1 (for p50= 0.0934)		

"S":	4	1.44010		0.7176 (6.124)
"SGMA":	2	1.32009		0.7309 (5.774)
"Ramp":	4	B= 0.90	T= 0.8170	0.6651 (7.508)
"Attr":	18	33	1 (for p50= 0.0897)	
"S":	3	1.53465		0.6394 (8.188)
"SGMA":	2	1.34282		0.7212 (6.031)
"Ramp":	4	B= 1.10	T= 0.7899	0.6588 (7.676)
"Attr":	19	33	1 (for p50= 0.0852)	
"S":	6	1.44298		0.7495 (5.285)
"SGMA":	3	1.37083		0.7359 (5.642)
"Ramp":	4	B= 1.30	T= 0.7635	0.6610 (7.618)
"Attr":	20	33	1 (for p50= 0.0808)	
"S":	5	1.49333		0.6962 (6.690)
"SGMA":	3	1.40000		0.7196 (6.074)
"Ramp":	4	B= 1.50	T= 0.7303	0.6653 (7.504)
"Attr":	19	33	1 (for p50= 0.0865)	
"S":	5	1.45345		0.7260 (5.904)
"SGMA":	3	1.36261		0.7405 (5.522)
"Ramp":	4	B= 1.70	T= 0.6954	0.6624 (7.582)
"Attr":	20	33	1 (for p50= 0.0834)	
"S":	5	1.47500		0.7101 (6.324)
"SGMA":	3	1.38281		0.7293 (5.818)
"Ramp":	4	B= 1.90	T= 0.6627	0.6614 (7.606)
"Attr":	20	33	1 (for p50= 0.0802)	
"S":	5	1.49745		0.6930 (6.773)
"SGMA":	3	1.40386		0.7174 (6.132)

1
For AQL= 0.01390 (at 95%):

					Uniform-Robustness	
					Pa	ROB
					----	----
"Ramp":	4	B= 0.50	T= *		*	*
(" Non-Existent ")						
"Ramp":	4	B= 0.70	T= 0.8275		0.7164 (5.358)	
"Attr":	16	25	1 (for p50= 0.1018)			
"S":	5	1.35609			0.7855 (3.774)	
"SGMA":	3	1.27134			0.7829 (3.833)	
"Ramp":	4	B= 0.90	T= 0.7961		0.7099 (5.507)	
"Attr":	17	25	1 (for p50= 0.0984)			
"S":	5	1.37699			0.7718 (4.089)	
"SGMA":	3	1.29093			0.7729 (4.063)	
"Ramp":	4	B= 1.10	T= 0.7684		0.7106 (5.492)	
"Attr":	17	25	1 (for p50= 0.0943)			
"S":	5	1.40250			0.7544 (4.487)	
"SGMA":	3	1.31484			0.7604 (4.350)	
"Ramp":	4	B= 1.30	T= *		*	*
"Ramp":	4	B= 1.50	T= 0.6976		0.7145 (5.404)	
"Attr":	16	25	1 (for p50= 0.1019)			
"S":	5	1.35560			0.7858 (3.767)	
"SGMA":	3	1.27088			0.7832 (3.827)	
"Ramp":	4	B= 1.70	T= 0.6638		0.7126 (5.445)	
"Attr":	17	25	1 (for p50= 0.0981)			
"S":	5	1.37867			0.7707 (4.115)	
"SGMA":	3	1.29250			0.7721 (4.081)	
"Ramp":	4	B= 1.90	T= 0.6313		0.7135 (5.425)	
"Attr":	17	25	1 (for p50= 0.0945)			
"S":	5	1.40107			0.7554 (4.464)	
"SGMA":	3	1.31351			0.7611 (4.334)	

1
For AQL= 0.01786 (at 95%):

					Uniform-Robustness	
					Pa	ROB
					----	----
"Ramp":	4	B= 0.50	T= *		*	*
(" Non-Existent ")						
"Ramp":	4	B= 0.70	T= 0.8055		0.7563 (3.875)	
"Attr":	15	19	1 (for p50= 0.1104)			
"S":	5	1.30627			0.8080 (2.839)	
"SGMA":	3	1.22463			0.7993 (3.014)	
"Ramp":	4	B= 0.90	T= 0.7745		0.7557 (3.887)	
"Attr":	15	19	1 (for p50= 0.1074)			
"S":	5	1.32341			0.7975 (3.050)	
"SGMA":	3	1.24070			0.7914 (3.172)	
"Ramp":	4	B= 1.10	T= *		*	*
(" Non-Existent ")						
"Ramp":	4	B= 1.30	T= 0.7002		0.7619 (3.761)	
"Attr":	13	19	1 (for p50= 0.1232)			
"S":	5	1.23655			0.8475 (2.049)	
"SGMA":	3	1.15927			0.8295 (2.409)	
"Ramp":	4	B= 1.50	T= 0.6643		0.7599 (3.803)	
"Attr":	14	19	1 (for p50= 0.1190)			
"S":	5	1.25867			0.8356 (2.288)	
"SGMA":	3	1.18000			0.8203 (2.595)	
"Ramp":	4	B= 1.70	T= 0.6312		0.7597 (3.806)	
"Attr":	14	19	1 (for p50= 0.1147)			
"S":	5	1.28207			0.8224 (2.552)	
"SGMA":	3	1.20194			0.8101 (2.797)	
"Ramp":	4	B= 1.90	T= 0.5988		0.7548 (3.904)	
"Attr":	15	19	1 (for p50= 0.1108)			
"S":	5	1.30360			0.8097 (2.807)	
"SGMA":	3	1.22213			0.8005 (2.990)	

For AQL= 0.02275 (at 95%) :

Uniform-Robustness

				Pa	ROB
"Ramp":	4	B= 0.50	T= *	*	*
		(" Non-Existent ")			
"Ramp":	4	B= 0.70	T= *	*	*
		(" Non-Existent ")			
"Ramp":	4	B= 0.90	T= *	*	*
		(" Non-Existent ")			
"Ramp":	4	B= 1.10	T= 0.7036	0.8043	(2.588)
"Attr":	10	15	1 (for p50= 0.1580)		
" S ":	3	1.14584		0.8280	(2.168)
"SGMA":	2	1.00261		0.8351	(2.043)
"Ramp":	4	B= 1.30	T= 0.6645	0.8021	(2.628)
"Attr":	10	15	1 (for p50= 0.1670)		
" S ":	2	1.28808		0.7268	(3.966)
"SGMA":	2	0.96606		0.8470	(1.831)
"Ramp":	4	B= 1.50	T= 0.6303	0.8011	(2.646)
"Attr":	10	15	1 (for p50= 0.1613)		
" S ":	2	1.31911		0.7134	(4.204)
"SGMA":	2	0.98933		0.8394	(1.965)
"Ramp":	4	B= 1.70	T= 0.5977	0.7946	(2.762)
"Attr":	12	15	1 (for p50= 0.1332)		
" S ":	5	1.18544		0.8649	(1.512)
"SGMA":	3	1.11135		0.8428	(1.905)
"Ramp":	4	B= 1.90	T= 0.5652	0.8010	(2.649)
"Attr":	12	15	1 (for p50= 0.1293)		
" S ":	4	1.23228		0.8164	(2.375)
"SGMA":	3	1.12959		0.8351	(2.042)

For AQL= 0.02872 (at 95%) :

Uniform-Robustness

				Pa	ROB
"Ramp":	4	B= 0.50	T= *	*	*
		(" Non-Existent ")			
"Ramp":	4	B= 0.70	T= *	*	*
		(" Non-Existent ")			
"Ramp":	4	B= 0.90	T= *	*	*
		(" Non-Existent ")			
" S ":	2	1.13659		0.7798	(2.705)
"SGMA":	2	0.85244		0.8752	(1.189)
"Ramp":	4	B= 1.30	T= 0.6284	0.8377	(1.785)
"Attr":	8	12	1 (for p50= 0.1907)		
" S ":	2	1.16717		0.7679	(2.894)
"SGMA":	2	0.87538		0.8685	(1.295)
"Ramp":	4	B= 1.50	T= 0.5954	0.8300	(1.908)
"Attr":	10	12	1 (for p50= 0.1587)		
" S ":	4	1.09091		0.8736	(1.214)
"SGMA":	3	1.00000		0.8776	(1.151)
"Ramp":	4	B= 1.70	T= 0.5630	0.8349	(1.830)
"Attr":	9	12	1 (for p50= 0.1794)		
" S ":	2	1.22342		0.7453	(3.254)
"SGMA":	2	0.91757		0.8557	(1.499)
"Ramp":	4	B= 1.90	T= 0.5305	0.8414	(1.726)
"Attr":	9	12	1 (for p50= 0.1750)		
" S ":	2	1.24603		0.7359	(3.404)
"SGMA":	2	0.93452		0.8504	(1.583)

For AQL= 0.03593 (at 95%) :

Uniform-Robustness

				Pa	ROB
"Ramp":	4	B= 0.50	T= *	*	*
		(" Non-Existent ")			
"Ramp":	4	B= 0.70	T= *	*	*
		(" Non-Existent ")			
"Ramp":	4	B= 0.90	T= *	*	*
		(" Non-Existent ")			
"Ramp":	4	B= 1.10	T= 0.6255	0.8695	(1.108)
"Attr":	7	9	1 (for p50= 0.2235)		
" S ":	2	1.01397		0.8156	(1.850)
"SGMA":	2	0.76042		0.8938	(0.774)
"Ramp":	4	B= 1.30	T= 0.5917	0.8611	(1.224)
"Attr":	7	9	1 (for p50= 0.2162)		
" S ":	2	1.04686		0.8039	(2.011)
"SGMA":	2	0.78515		0.8871	(0.866)
"Ramp":	4	B= 1.50	T= 0.5595	0.8643	(1.179)
"Attr":	7	9	1 (for p50= 0.2102)		
" S ":	2	1.07429		0.7939	(2.149)
"SGMA":	2	0.80571		0.8814	(0.944)
"Ramp":	4	B= 1.70	T= 0.5273	0.8696	(1.106)
"Attr":	8	9	1 (for p50= 0.2046)		
" S ":	2	1.10944		0.7846	(2.296)

"SGMA":	2	0.82533		0.8756 (1.021)
"Ramp":	4	B= 1.90	T= 0.4978	0.8715 (1.080)
"Attr":	2	9	1 (for p50= 0.1985)	
"S":	2	1.12937		0.7729 (2.437)
"SGMA":	2	0.84703		0.8695 (1.108)

1

For AQL= 0.04457 (at 95%) :

=====					Uniform-Robustness	
					Pa	ROB
					----	----
"Ramp":	4	B= 0.50	T= *		*	*
	(" Non-Existent ")				
"Ramp":	4	B= 0.70	T= *		*	*
	(" Non-Existent ")				
"Ramp":	4	B= 0.90	T= *		*	*
	(" Non-Existent ")				
"Ramp":	4	B= 1.10	T= 0.5861		0.8885 (0.746)	
"Attr":	6	7	1 (for p50= 0.2514)			
"S":	2	0.89343			0.8460 (1.262)	
"SGMA":	2	0.67007			0.8867 (0.768)	
"Ramp":	4	B= 1.30	T= 0.5542		0.8901 (0.727)	
"Attr":	6	7	1 (for p50= 0.2436)			
"S":	2	0.92657			0.8352 (1.394)	
"SGMA":	2	0.69493			0.8798 (0.852)	
"Ramp":	4	B= 1.50	T= 0.5227		0.8940 (0.680)	
"Attr":	7	7	1 (for p50= 0.2375)			
"S":	2	0.95262			0.8265 (1.500)	
"SGMA":	2	0.71447			0.8980 (0.631)	
"Ramp":	4	B= 1.70	T= 0.4958		0.8928 (0.694)	
"Attr":	7	7	1 (for p50= 0.2282)			
"S":	2	0.99290			0.8125 (1.669)	
"SGMA":	2	0.74468			0.8900 (0.729)	
"Ramp":	4	B= 1.90	T= 0.4605		0.8954 (0.662)	
"Attr":	7	7	1 (for p50= 0.2307)			
"S":	2	0.98199			0.8163 (1.623)	
"SGMA":	2	0.73649			0.8922 (0.702)	

1

For AQL= 0.05480 (at 95%) :

=====					Uniform-Robustness	
					Pa	ROB
					----	----
"Ramp":	4	B= 0.50	T= *		*	*
	(" Non-Existent ")				
"Ramp":	4	B= 0.90	T= *		*	*
	(" Non-Existent ")				
"Ramp":	4	B= 1.10	T= 0.5463		0.9132 (0.413)	
"Attr":	5	6	1 (for p50= 0.2807)			
"S":	2	0.77436			0.8716 (0.881)	
"SGMA":	2	0.58077			0.9010 (0.550)	
"Ramp":	4	B= 1.30	T= 0.5158		0.9157 (0.385)	
"Attr":	6	6	1 (for p50= 0.2735)			
"S":	2	0.80290			0.8632 (0.976)	
"SGMA":	2	0.60217			0.8955 (0.613)	
"Ramp":	4	B= 1.50	T= 0.4941		0.9098 (0.452)	
"Attr":	6	6	1 (for p50= 0.2593)			
"S":	2	0.86055			0.8452 (1.178)	
"SGMA":	2	0.64541			0.8857 (0.745)	
"Ramp":	4	B= 1.70	T= 0.4567		0.9120 (0.427)	
"Attr":	6	6	1 (for p50= 0.2665)			
"S":	2	0.83119			0.8545 (1.074)	
"SGMA":	2	0.62339			0.8898 (0.677)	
"Ramp":	4	B= 1.90	T= 0.4234		0.9147 (0.396)	
"Attr":	6	6	1 (for p50= 0.2611)			
"S":	2	0.85333			0.8475 (1.152)	
"SGMA":	2	0.64000			0.8852 (0.728)	

1

For AQL= 0.06681 (at 95%) :

=====					Uniform-Robustness	
					Pa	ROB
					----	----
"Ramp":	4	B= 0.50	T= *		*	*
	(" Non-Existent ")				
"Ramp":	4	B= 0.70	T= *		*	*
	(" Non-Existent ")				
"Ramp":	4	B= 0.90	T= *		*	*
	(" Non-Existent ")				
"Ramp":	4	B= 1.10	T= 0.5062		0.9355 (0.231)	
"Attr":	8	12	2 (for p50= 0.3111)			
"S":	2	0.65695			0.8929 (0.908)	
"SGMA":	2	0.49272			0.9126 (0.594)	
"Ramp":	4	B= 1.30	T= 0.4928		0.9233 (0.424)	
"Attr":	9	12	2 (for p50= 0.2910)			
"S":	3	0.62924			0.9440 (0.096)	
"SGMA":	3	0.55059			0.9589 (-0.141)	
"Ramp":	4	B= 1.50	T= 0.4528		0.9249 (0.398)	
"Attr":	8	12	2 (for p50= 0.3073)			

" S ":	2	0.67122		0.8890 (0.969)
"SGMA":	2	0.50342		0.9100 (0.636)
"Ramp":	4	B= 1.70	T= 0.4180	0.9273 (0.361)
"Attr":	8	12	2 {for p50= 0.2976}	
" S ":	2	0.70857		0.8786 (1.135)
"SGMA":	2	0.53143		0.9030 (0.747)
"Ramp":	4	B= 1.90	T= 0.3866	0.9302 (0.315)
"Attr":	9	12	2 {for p50= 0.2952}	
" S ":	2	0.71781		0.8760 (1.177)
"SGMA":	2	0.53836		0.9012 (0.775)

For AQL= 0.08076 (at 95%) :

=====					Uniform-Robustness	
					Pa	ROB
					----	----
"Ramp":	4	B= 0.50	T= *		*	*
	(" Non-Existent ")			
"Ramp":	4	B= 0.70	T= *		*	*
	(" Non-Existent ")			
"Ramp":	4	B= 0.90	T= *		*	*
	(" Non-Existent ")			
"Ramp":	4	B= 1.10	T= 0.4928	0.9339 (0.234)		
"Attr":	8	10	2 {for p50= 0.3216}			
" S ":	3	0.52930		0.9541 (-0.059)		
"SGMA":	3	0.46313		0.9652 (-0.220)		
"Ramp":	4	B= 1.30	T= 0.4487	0.9352 (0.215)		
"Attr":	7	10	2 {for p50= 0.3579}			
" S ":	2	0.48551		0.9024 (0.691)		
"SGMA":	2	0.36413		0.9309 (0.277)		
"Ramp":	4	B= 1.50	T= 0.4121	0.9371 (0.187)		
"Attr":	7	10	2 {for p50= 0.3366}			
" S ":	2	0.56245		0.8818 (0.990)		
"SGMA":	2	0.42184		0.9180 (0.465)		
"Ramp":	4	B= 1.70	T= 0.3798	0.9396 (0.151)		
"Attr":	8	10	2 {for p50= 0.3338}			
" S ":	2	0.57274		0.8789 (1.032)		
"SGMA":	2	0.42955		0.9161 (0.491)		
"Ramp":	4	B= 1.90	T= 0.3502	0.9388 (0.163)		
"Attr":	8	10	2 {for p50= 0.3318}			
" S ":	2	0.58002		0.8768 (1.062)		
"SGMA":	2	0.43501		0.9149 (0.510)		

For AQL= 0.09480 (at 95%) :

=====					Uniform-Robustness	
					Pa	ROB
					----	----
"Ramp":	4	B= 0.50	T= *		*	*
	(" Non-Existent ")			
"Ramp":	4	B= 0.70	T= *		*	*
	(" Non-Existent ")			
"Ramp":	4	B= 0.90	T= *		*	*
	(" Non-Existent ")			
"Ramp":	4	B= 1.10	T= 0.4450	0.9433 (0.087)		
"Attr":	7	8	2 {for p50= 0.3446}			
" S ":	4	0.45714		0.9571 (-0.097)		
"SGMA":	2	0.40700		0.9665 (-0.218)		
"Ramp":	4	B= 1.30	T= 0.4157	0.9445 (0.074)		
"Attr":	7	8	2 {for p50= 0.3711}			
" S ":	2	0.41412		0.9164 (0.566)		
"SGMA":	2	0.31159		0.9305 (0.234)		
"Ramp":	4	B= 1.50	T= 0.3722	0.9427 (0.054)		
"Attr":	7	8	2 {for p50= 0.3749}			
" S ":	2	0.42504		0.9036 (1.062)		
"SGMA":	2	0.31978		0.9267 (0.277)		
"Ramp":	4	B= 1.70	T= 0.3421	0.9460 (0.052)		
"Attr":	7	8	2 {for p50= 0.3723}			
" S ":	2	0.43459		0.9012 (1.027)		
"SGMA":	2	0.32595		0.9271 (0.297)		
"Ramp":	4	B= 1.90	T= 0.3143	0.9495 (0.006)		
"Attr":	7	8	2 {for p50= 0.3706}			
" S ":	2	0.44023		0.8990 (1.052)		
"SGMA":	2	0.33017		0.9262 (0.309)		

For AQL= 0.01072 (at 95%) :

=====					Uniform-Robustness	
					Pa	ROB
					----	----
"Ramp":	8	B= 0.50	T= *		*	*
	(" Non-Existent ")			
"Ramp":	8	B= 0.70	T= *		*	*
	(" Non-Existent ")			
"Ramp":	8	B= 0.90	T= 0.8621	0.5637 (10.182)		
"Attr":	25	33	1 {for p50= 0.0668}			
" S ":	8	1.55556		0.6727 (7.309)		
"SGMA":	4	1.50000		0.6772 (7.192)		
"Ramp":	8	B= 1.10	T= 0.8360	0.5386 (10.843)		
"Attr":	26	33	1 {for p50= 0.0635}			

"S":	8	1.52257		0.6451 (6.036)
"SGMA":	4	1.52605		0.6589 (7.673)
"Ramp":	8	B= 1.30	T= 0.8124	0.5081 (11.647)
"Attr":	28	33	1 {for p50= 0.0594}	
"S":	8	1.61740		0.6085 (9.002)
"SGMA":	4	1.55964		0.6348 (8.399)
"Ramp":	8	B= 1.50	T= 0.7881	0.4924 (12.062)
"Attr":	30	33	1 {for p50= 0.0557}	
"S":	11	1.63257		0.5819 (9.702)
"SGMA":	5	1.59175		0.6175 (8.764)
"Ramp":	8	B= 1.70	T= 0.7617	0.4833 (12.301)
"Attr":	31	33	1 {for p50= 0.0526}	
"S":	11	1.66218		0.5432 (10.722)
"SGMA":	5	1.62063		0.5934 (9.400)
"Ramp":	8	B= 1.90	T= 0.7330	0.4795 (10.822)
"Attr":	53	76	2 {for p50= 0.0501}	
"S":	14	1.67585		0.5284 (16.863)
"SGMA":	6	1.64362		0.5759 (14.963)

1

For AQL= 0.01390 (at 95%) :

```

=====
Uniform-Robustness
Pa      ROB
-----  -----
"Ramp":  8      B= 0.50  T= *
( " Non-Existent " )      *      *

"Ramp":  8      B= 0.70  T= 0.8706      0.6481 ( 6.926)
"Attr":  20     25      1 {for p50= 0.0813}
" S ":   7      1.45707
"SGMA":  4      1.39636      0.7432 ( 4.745)
                                           0.7388 ( 4.846)

"Ramp":  8      B= 0.90  T= 0.8393      0.6273 ( 7.404)
"Attr":  21     25      1 {for p50= 0.0784}
" S ":   8      1.46813
"SGMA":  4      1.41569      0.7456 ( 4.690)
                                           0.7264 ( 5.130)

"Ramp":  8      B= 1.10  T= 0.8141      0.6024 ( 7.974)
"Attr":  22     25      1 {for p50= 0.0740}
" S ":   8      1.50003
"SGMA":  4      1.44845      0.7162 ( 5.365)
                                           0.7061 ( 5.594)

"Ramp":  8      B= 1.30  T= 0.7899      0.5767 ( 8.564)
"Attr":  24     25      1 {for p50= 0.0695}
" S ":  10      1.52166
"SGMA":  5      1.47939      0.7123 ( 5.453)
                                           0.6984 ( 5.771)

"Ramp":  8      B= 1.50  T= 0.7640      0.5649 (13.457)
"Attr":  40     58      2 {for p50= 0.0657}
" S ":  10      1.55205
"SGMA":  5      1.50893      0.6791 ( 9.487)
                                           0.6756 ( 9.590)

"Ramp":  8      B= 1.70  T= 0.7357      0.5587 (12.188)
"SGMA":  6      1.53322      0.8882 ( 9.978)
                                           0.5579 (13.703)

"Ramp":  8      B= 1.90  T= 0.7056      0.6369 (10.940)
"Attr":  44     58      2 {for p50= 0.0601}
" S ":  13      1.58676
"SGMA":  6      1.55370      0.6481 (10.549)

```

1

For AQL= 0.01786 (at 95%) :

```

=====
Uniform-Robustness
Pa      ROB
-----  -----
"Ramp":  8      B= 0.50  T= *
( " Non-Existent " )      *      *

"Ramp":  8      B= 0.70  T= 0.8450      0.7071 ( 4.857)
"Attr":  17     19      1 {for p50= 0.0948}
" S ":   7      1.36862
"SGMA":  4      1.31159      0.8021 ( 2.959)
                                           0.7819 ( 3.363)

"Ramp":  8      B= 0.90  T= 0.8163      0.6853 ( 5.294)
"Attr":  18     19      1 {for p50= 0.0906}
" S ":   7      1.39495
"SGMA":  4      1.33682      0.7823 ( 3.355)
                                           0.7670 ( 3.660)

"Ramp":  8      B= 1.10  T= 0.7914      0.6575 ( 5.849)
"Attr":  19     19      1 {for p50= 0.0856}
" S ":   9      1.41267
"SGMA":  5      1.36852      0.7937 ( 3.126)
                                           0.7683 ( 3.635)

"Ramp":  8      B= 1.30  T= 0.7658      0.6436 ( 9.429)
"Attr":  32     45      2 {for p50= 0.0811}
" S ":   9      1.44311
"SGMA":  5      1.39801      0.7669 ( 5.636)
                                           0.7480 ( 6.217)

"Ramp":  8      B= 1.50  T= 0.7378      0.6346 ( 9.707)
"Attr":  34     45      2 {for p50= 0.0775}
" S ":  10      1.46274
"SGMA":  5      1.42211      0.7526 ( 5.892)
                                           0.7308 ( 6.746)

"Ramp":  8      B= 1.70  T= 0.7079      0.6316 ( 9.800)
"Attr":  35     45      2 {for p50= 0.0744}
" S ":  12      1.47761
"SGMA":  6      1.44403      0.7476 ( 6.228)
                                           0.7293 ( 6.793)

"Ramp":  8      B= 1.90  T= 0.6767      0.6335 ( 9.743)
"Attr":  37     45      2 {for p50= 0.0718}
" S ":  12      1.49647
"SGMA":  6      1.46246      0.7263 ( 6.884)
                                           0.7144 ( 7.251)

```

1

For AQL= 0.02275 (at 95%) :

=====

Uniform-Robustness

		B=	T=	Pa	ROB
"Ramp":	8	0.50	*	*	*
(" Non-Existent ")		
"Ramp":	8	0.70	T= 0.8201	0.7571	(3.428)
"Attr":	15	1	{for p50= 0.1087}		
" S ":	7	1.28717		0.8459	(1.849)
"SGMA":	4	1.23354		0.8157	(2.387)
"Ramp":	8	0.90	T= 0.7932	0.7298	(5.977)
"Attr":	25	2	{for p50= 0.1035}		
" S ":	7	1.31674		0.8266	(3.348)
"SGMA":	4	1.26187		0.8004	(4.061)
"Ramp":	8	1.10	T= 0.7674	0.7155	(6.366)
"Attr":	27	2	{for p50= 0.0986}		
" S ":	9	1.33105		0.8444	(2.866)
"SGMA":	5	1.28946		0.8080	(3.855)
"Ramp":	8	1.30	T= 0.7394	0.7054	(6.641)
"Attr":	28	2	{for p50= 0.0950}		
" S ":	9	1.35287		0.8283	(3.304)
"SGMA":	5	1.31060		0.7949	(4.210)
"Ramp":	8	1.50	T= 0.7095	0.6999	(6.789)
"Attr":	29	2	{for p50= 0.0912}		
" S ":	11	1.36773		0.8282	(3.307)
"SGMA":	6	1.33354		0.7987	(4.107)
"Ramp":	8	1.70	T= 0.6785	0.6990	(6.813)
"Attr":	30	2	{for p50= 0.0879}		
" S ":	11	1.38832		0.8102	(3.795)
"SGMA":	6	1.35361		0.7847	(4.486)
"Ramp":	8	1.90	T= 0.6463	0.7050	(6.651)
"Attr":	31	2	{for p50= 0.0854}		
" S ":	11	1.40507		0.7948	(4.214)
"SGMA":	6	1.36994		0.7730	(4.805)

For AQL= 0.02872 (at 95%) :

=====

Uniform-Robustness

		B=	T=	Pa	ROB
"Ramp":	8	0.50	T= 0.8290	0.8127	(3.334)
"Attr":	21	2	{for p50= 0.1266}		
" S ":	6	1.20261		0.8658	(2.045)
"SGMA":	4	1.14248		0.8507	(2.411)
"Ramp":	8	0.70	T= 0.7964	0.7895	(3.896)
"Attr":	21	2	{for p50= 0.1224}		
" S ":	6	1.22403		0.8541	(2.329)
"SGMA":	4	1.16282		0.8410	(2.646)
"Ramp":	8	0.90	T= 0.7683	0.7606	(4.597)
"SGMA":	5	1.18476		0.8349	(2.794)
"Ramp":	8	1.10	T= 0.7410	0.7672	(4.439)
"Attr":	23	2	{for p50= 0.1151}		
" S ":	8	1.24444		0.8742	(1.840)
"SGMA":	5	1.20000		0.8470	(2.501)
"Ramp":	8	1.30	T= 0.7104	0.7606	(4.597)
"Attr":	24	2	{for p50= 0.1108}		
" S ":	8	1.26756		0.8601	(2.183)
"SGMA":	5	1.22229		0.8349	(2.794)
"Ramp":	8	1.50	T= 0.6794	0.7574	(4.677)
"Attr":	25	2	{for p50= 0.1069}		
" S ":	10	1.27889		0.8776	(1.757)
"SGMA":	6	1.24336		0.8429	(2.599)
"Ramp":	8	1.70	T= 0.6475	0.7612	(4.584)
"Attr":	25	2	{for p50= 0.1035}		
" S ":	10	1.29779		0.8650	(2.063)
"SGMA":	6	1.26174		0.8319	(2.869)
"Ramp":	8	1.90	T= 0.6146	0.7674	(4.434)
"Attr":	26	2	{for p50= 0.1009}		
" S ":	10	1.31262		0.8546	(2.317)
"SGMA":	6	1.27616		0.8229	(3.086)

For AQL= 0.03593 (at 95%) :

=====

Uniform-Robustness

		B=	T=	Pa	ROB
"Ramp":	8	0.50	T= 0.8041	0.8337	(2.503)
"Attr":	16	2	{for p50= 0.1643}		
" S ":	4	1.06558		0.8737	(1.641)
"SGMA":	3	0.97678		0.8770	(1.571)
"Ramp":	8	0.70	T= 0.7725	0.8255	(2.679)
"Attr":	16	2	{for p50= 0.1601}		
" S ":	6	1.04626		0.9242	(0.556)
"SGMA":	4	0.99395		0.9016	(1.042)
"Ramp":	8	0.90	T= 0.7433	0.8183	(2.835)
"Attr":	16	2	{for p50= 0.1616}		
" S ":	5	1.05398		0.9027	(1.019)
"SGMA":	4	0.98810		0.9037	(0.997)
"Ramp":	8	1.10	T= 0.7110	0.8117	(2.976)
"Attr":	20	2	{for p50= 0.1332}		
" S ":	8	1.15264		0.9095	(0.872)
"SGMA":	5	1.11147		0.8783	(1.544)
"Ramp":	8	1.30	T= 0.6795	0.8071	(3.075)
"Attr":	28	2	{for p50= 0.1288}		
" S ":	10	1.16463		0.9263	(0.510)

"SGMA":	6	1.13228		0.8865 (1.823)
"Ramp":	8	R= 1.50	T= 0.6479	0.8891 (3.032)
"Attr":	21	22 2	{for p50= 0.1246}	
" S ":	9	1.18958		0.9035 (1.100)
"SGMA":	6	1.15241		0.8786 (1.537)
"Ramp":	8	R= 1.70	T= 0.6152	0.8131 (2.945)
"Attr":	22	22 2	{for p50= 0.1212}	
" S ":	10	1.20223		0.9079 (0.905)
"SGMA":	6	1.16884		0.8704 (1.713)
"Ramp":	8	R= 1.90	T= 0.5817	0.8199 (2.800)
"Attr":	22	22 2	{for p50= 0.1188}	
" S ":	12	1.20837		0.9167 (0.718)
"SGMA":	7	1.18091		0.8210 (1.486)

1

For AQL= 0.04457 (at 95%) :

```

=====
Uniform-Robustness
Pa  ROB
-----
"Ramp": 8 R= 0.50 T= 0.7795 0.8598 (1.757)
"Attr": 14 18 2 {for p50= 0.1809}
" S " : 5 0.97266
"SGMA": 4 0.91187 0.9214 (0.556)
          0.9191 (0.602)

"Ramp": 8 R= 0.70 T= 0.7480 0.8577 (1.796)
"Attr": 15 18 2 {for p50= 0.1779}
" S " : 5 0.98490
"SGMA": 4 0.92334 0.9172 (0.638)
          0.9154 (0.673)

"Ramp": 8 R= 0.90 T= 0.7118 0.8525 (1.898)
"Attr": 13 18 2 {for p50= 0.1919}
" S " : 4 0.95019
"SGMA": 3 0.87100 0.9065 (0.848)
          0.9019 (0.936)

"Ramp": 8 R= 1.10 T= 0.6786 0.8483 (1.981)
"Attr": 14 18 2 {for p50= 0.1798}
" S " : 5 0.97725
"SGMA": 4 0.91618 0.9199 (0.586)
          0.9177 (0.629)

"Ramp": 8 R= 1.30 T= 0.6474 0.8486 (1.973)
"Attr": 15 18 2 {for p50= 0.1737}
" S " : 5 1.00242
"SGMA": 4 0.93977 0.9109 (0.761)
          0.9100 (0.778)

"Ramp": 8 R= 1.50 T= 0.6152 0.8504 (1.938)
"Attr": 15 18 2 {for p50= 0.1686}
" S " : 5 1.02376
"SGMA": 4 0.95977 0.9028 (0.919)
          0.9031 (0.913)

"Ramp": 8 R= 1.70 T= 0.5815 0.8555 (1.839)
"Attr": 16 18 2 {for p50= 0.1652}
" S " : 7 1.01569
"SGMA": 5 0.97337 0.9388 (0.217)
          0.9212 (0.561)

" S " : 7 1.02713 0.9350 (0.293)
"SGMA": 5 0.98433 0.9174 (0.634)

```

1

For AQL= 0.05480 (at 95%) :

```

=====
Uniform-Robustness
Pa  ROB
-----
"Ramp": 8 R= 0.50 T= 0.7556 0.8818 (1.171)
"Attr": 13 14 2 {for p50= 0.1952}
" S " : 5 0.91612
"SGMA": 4 0.85887 0.9284 (0.372)
          0.9244 (0.439)

"Ramp": 8 R= 0.70 T= 0.7142 0.8829 (1.151)
"Attr": 12 14 2 {for p50= 0.2118}
" S " : 5 0.85352
"SGMA": 4 0.80017 0.9463 (0.063)
          0.9405 (0.163)

"Ramp": 8 R= 0.90 T= 0.6765 0.8816 (1.175)
"Attr": 12 14 2 {for p50= 0.2114}
" S " : 5 0.85515
"SGMA": 4 0.80170 0.9459 (0.071)
          0.9401 (0.169)

"Ramp": 8 R= 1.10 T= 0.6458 0.8806 (1.192)
"Attr": 13 14 2 {for p50= 0.2039}
" S " : 5 0.88300
"SGMA": 4 0.82781 0.9383 (0.201)
          0.9333 (0.287)

"Ramp": 8 R= 1.30 T= 0.6146 0.8800 (1.202)
"Attr": 13 14 2 {for p50= 0.1972}
" S " : 5 0.90843
"SGMA": 4 0.85166 0.9308 (0.330)
          0.9266 (0.403)

"Ramp": 8 R= 1.50 T= 0.5807 0.8835 (1.141)
"Attr": 13 14 2 {for p50= 0.1935}
" S " : 7 0.90271
"SGMA": 5 0.86510 0.9607 (-0.183)
          0.9433 (0.116)

"Ramp": 8 R= 1.70 T= 0.5468 0.8884 (1.057)
"Attr": 14 14 2 {for p50= 0.1900}
" S " : 6 0.92404
"SGMA": 5 0.87784 0.9427 (0.126)
          0.9398 (0.176)

"Ramp": 8 R= 1.90 T= 0.5132 0.8952 (0.941)
"Attr": 14 14 2 {for p50= 0.1875}
" S " : 6 0.93373
"SGMA": 5 0.88704 0.9398 (0.175)
          0.9372 (0.220)

```

1

For AQL= 0.06681 (at 95%) :

```

=====
Uniform-Robustness
Pa  ROB

```

"Ramp":	8	B= 0.50	T= 0.7219	0.9032 (0.947)
"Attr":	17	20 3	{for p50= 0.2119}	
" S ":	6	0.84211		0.9536 (-0.074)
"SGMA":	5	0.80000		0.9493 (0.014)
"Ramp":	8	B= 0.70	T= 0.6727	0.9089 (0.654)
"Attr":	10	12 2	{for p50= 0.2448}	
" S ":	4	0.75395		0.9417 (0.133)
"SGMA":	4	0.69112		0.9557 (-0.091)
"Ramp":	8	B= 0.90	T= 0.6425	0.9066 (0.690)
"Attr":	11	12 2	{for p50= 0.2375}	
" S ":	5	0.76195		0.9581 (-0.127)
"SGMA":	4	0.71432		0.9509 (-0.014)
"Ramp":	8	B= 1.10	T= 0.6136	0.9028 (0.751)
"Attr":	11	12 2	{for p50= 0.2283}	
" S ":	5	0.79398		0.9508 (-0.012)
"SGMA":	4	0.74435		0.9440 (0.095)
"Ramp":	8	B= 1.30	T= 0.5792	0.9051 (0.714)
"Attr":	11	12 2	{for p50= 0.2251}	
" S ":	5	0.80541		0.9480 (0.032)
"SGMA":	4	0.75507		0.9414 (0.137)
"Ramp":	8	B= 1.50	T= 0.5451	0.9086 (0.657)
"Attr":	12	12 2	{for p50= 0.2207}	
" S ":	6	0.81024		0.9611 (-0.176)
"SGMA":	5	0.76973		0.9564 (-0.101)
"Ramp":	8	B= 1.70	T= 0.5112	0.9145 (0.728)
"Attr":	16	20 3	{for p50= 0.2175}	
" S ":	6	0.82163		0.9585 (-0.175)
"SGMA":	5	0.78055		0.9539 (-0.081)
"Ramp":	8	B= 1.90	T= 0.4780	0.9200 (0.615)
"Attr":	17	20 3	{for p50= 0.2153}	
" S ":	6	0.82969		0.9566 (-0.136)
"SGMA":	5	0.78820		0.9522 (-0.044)

1

For AQL= 0.08076 (at 95%) :

=====

				Uniform-Robustness	
				Pa	ROB
				-----	-----
"Ramp":	8	B= 0.50	T= 0.6663	0.9328 (0.250)	
"Attr":	9	10 2	{for p50= 0.2825}		
" S ":	3	0.65759		0.9263 (0.344)	
"SGMA":	3	0.57539		0.9451 (0.071)	
"Ramp":	8	B= 0.70	T= 0.6367	0.9289 (0.307)	
"Attr":	9	10 2	{for p50= 0.2743}		
" S ":	4	0.65427		0.9534 (-0.149)	
"SGMA":	4	0.59975		0.9638 (-0.200)	
"Ramp":	8	B= 0.90	T= 0.6125	0.9288 (0.311)	
"SGMA":	4	0.63990		0.9583 (-0.116)	
"Ramp":	8	B= 1.10	T= 0.5770	0.9214 (0.525)	
"Attr":	14	16 3	{for p50= 0.2601}		
" S ":	4	0.70147		0.9427 (0.134)	
"SGMA":	4	0.64301		0.9557 (-0.104)	
"Ramp":	8	B= 1.30	T= 0.5428	0.9237 (0.484)	
"Attr":	14	16 3	{for p50= 0.2543}		
" S ":	4	0.72115		0.9377 (0.225)	
"SGMA":	4	0.66105		0.9519 (-0.036)	
"Ramp":	8	B= 1.50	T= 0.5087	0.9289 (0.387)	
"Attr":	14	16 3	{for p50= 0.2505}		
" S ":	6	0.70849		0.9715 (-0.394)	
"SGMA":	5	0.67307		0.9661 (-0.295)	
"Ramp":	8	B= 1.70	T= 0.4751	0.9336 (0.302)	
"Attr":	14	16 3	{for p50= 0.2476}		
" S ":	6	0.71786		0.9698 (-0.364)	
"SGMA":	5	0.68197		0.9644 (-0.265)	
"Ramp":	8	B= 1.90	T= 0.4425	0.9384 (0.213)	
"Attr":	14	16 3	{for p50= 0.2457}		
" S ":	6	0.72439		0.9686 (-0.342)	
"SGMA":	5	0.68817		0.9632 (-0.243)	

1

For AQL= 0.09680 (at 95%) :

=====

				Uniform-Robustness	
				Pa	ROB
				-----	-----
"Ramp":	8	B= 0.50	T= *	*	*
(" Non-existent ")					
"Ramp":	8	B= 0.70	T= 0.6117	0.9331 (0.291)	
"Attr":	12	14 3	{for p50= 0.2934}		
" S ":	4	0.59285		0.9546 (-0.079)	
"SGMA":	4	0.54845		0.9639 (-0.239)	
"Ramp":	8	B= 0.90	T= 0.5740	0.9337 (0.279)	
"Attr":	12	14 3	{for p50= 0.2994}		
" S ":	4	0.57381		0.9584 (-0.144)	
"SGMA":	4	0.52599		0.9668 (-0.289)	
"Ramp":	8	B= 1.10	T= 0.5396	0.9348 (0.260)	
"Attr":	12	14 3	{for p50= 0.2909}		
" S ":	4	0.60084		0.9529 (-0.090)	
"SGMA":	4	0.55077		0.9626 (-0.217)	
"Ramp":	8	B= 1.30	T= 0.5055	0.9396 (0.179)	
"Attr":	12	14 3	{for p50= 0.2862}		
" S ":	5	0.60232		0.9688 (-0.322)	
"SGMA":	5	0.56468		0.9747 (-0.424)	

"Ramp":	8	B= 1.50	T= 0.4717	0.9453 (1.115)
"Attr":	12	14 3	{for p50= 0.2827}	
" S ":	5	0.61305		0.9669 (-0.270)
"SGMA":	5	0.57473		0.9732 (-0.399)
"Ramp":	8	B= 1.70	T= 0.4386	0.9476 (0.041)
"Attr":	13	14 3	{for p50= 0.2803}	
" S ":	5	0.62071		0.9655 (-0.268)
"SGMA":	5	0.58192		0.9721 (-0.379)
"Ramp":	8	B= 1.90	T= 0.4070	0.9513 (-0.026)
"Attr":	13	14 3	{for p50= 0.2786}	
" S ":	5	0.62602		0.9645 (-0.249)
"SGMA":	5	0.58689		0.9713 (-0.366)

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For AQL= 0.01072 (at 95%) :

=====
Uniform-Robustness
Pa ROE

"Ramp":	16	B= 0.50	T= 0.9263	0.5104 (11.586)
"Attr":	29	73 1	{for p50= 0.0569}	
" S ":	11	1.62229		0.5952 (9.352)
"SGMA":	5	1.58173		0.6258 (8.545)
"Ramp":	16	B= 0.70	T= 0.9052	0.4468 (13.264)
"Attr":	31	73 1	{for p50= 0.0528}	
" S ":	11	1.66004		0.5460 (10.647)
"SGMA":	5	1.61854		0.5951 (9.354)
"Ramp":	16	B= 0.90	T= 0.8893	0.3776 (22.898)
"Attr":	56	76 2	{for p50= 0.0474}	
" S ":	14	1.70329		0.4875 (18.500)
"SGMA":	6	1.67053		0.5506 (15.976)
"Ramp":	16	B= 1.10	T= 0.8726	0.3201 (25.197)
"Attr":	61	76 2	{for p50= 0.0433}	
" S ":	17	1.74093		0.4248 (21.009)
"SGMA":	7	1.71373		0.5061 (17.755)
"Ramp":	16	B= 1.30	T= 0.8531	0.2815 (26.742)
"Attr":	66	76 2	{for p50= 0.0402}	
" S ":	20	1.77152		0.3660 (23.362)
"SGMA":	8	1.74221		0.4650 (19.400)
"Ramp":	16	B= 1.50	T= 0.8308	0.2583 (27.667)
"Attr":	70	76 2	{for p50= 0.0379}	
" S ":	23	1.79582		0.3142 (25.431)
"SGMA":	9	1.77541		0.4283 (20.868)
"Ramp":	16	B= 1.70	T= 0.8063	0.2447 (28.211)
"Attr":	74	76 2	{for p50= 0.0359}	
" S ":	26	1.81818		0.2648 (27.407)
"SGMA":	10	1.80000		0.3923 (22.310)
"Attr":	29	73 1	{for p50= 0.0343}	
" S ":	11	1.83756		0.2212 (37.685)
"SGMA":	11	1.82115		0.3377 (31.659)

1

For AQL= 0.01390 (at 95%) :

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Uniform-Robustness
Pa ROE

"Ramp":	16	B= 0.50	T= 0.9090	0.5966 (8.108)
"Attr":	25	25 1	{for p50= 0.0668}	
" S ":	10	1.54286		0.6893 (5.981)
"SGMA":	5	1.50000		0.6826 (6.136)
"Ramp":	16	B= 0.70	T= 0.8910	0.5176 (15.111)
"Attr":	44	58 2	{for p50= 0.0606}	
" S ":	13	1.58251		0.6427 (10.740)
"SGMA":	6	1.54954		0.6518 (10.420)
"Ramp":	16	B= 0.90	T= 0.8742	0.4482 (17.535)
"Attr":	48	58 2	{for p50= 0.0548}	
" S ":	16	1.62712		0.5898 (12.585)
"SGMA":	7	1.60000		0.6108 (11.853)
"Ramp":	16	B= 1.10	T= 0.8549	0.3968 (19.332)
"Attr":	52	58 2	{for p50= 0.0512}	
" S ":	18	1.65786		0.5440 (14.188)
"SGMA":	8	1.63348		0.5793 (12.954)
"Ramp":	16	B= 1.30	T= 0.8332	0.3629 (20.516)
"Attr":	55	58 2	{for p50= 0.0482}	
" S ":	21	1.68391		0.5000 (15.725)
"SGMA":	9	1.66286		0.5473 (14.072)
"Ramp":	16	B= 1.50	T= 0.8095	0.3409 (21.286)
"Attr":	58	58 2	{for p50= 0.0456}	
" S ":	24	1.70762		0.4537 (17.341)
"SGMA":	10	1.68906		0.5151 (15.197)
"Ramp":	16	B= 1.70	T= 0.7832	0.3302 (28.127)
"Attr":	84	98 3	{for p50= 0.0435}	
" S ":	27	1.72841		0.4085 (24.594)
"SGMA":	11	1.71179		0.4631 (22.114)
"Ramp":	16	B= 1.90	T= 0.7546	0.3296 (28.180)
"Attr":	87	98 3	{for p50= 0.0418}	
" S ":	30	1.74537		0.3682 (26.420)
"SGMA":	12	1.73032		0.4361 (23.341)

1

For AQL= 0.01786 (at 95%) :

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Uniform-Robustness
Pa ROE

"Ramp":	16	B= 0.50	T= 0.8943	0.6519 (9.174)
"Attr":	34	45 2	{for p50= 0.0777}	
" S ":	10	1.46165		0.7596 (5.359)
"SGMA":	5	1.42105		0.7316 (6.728)
"Ramp":	16	B= 0.70	T= 0.8762	0.5831 (11.293)
"Attr":	38	45 2	{for p50= 0.0692}	
" S ":	14	1.51100		0.7243 (6.948)
"SGMA":	7	1.48194		0.7097 (7.396)
"Ramp":	16	B= 0.90	T= 0.8562	0.5254 (15.070)
"Attr":	41	45 2	{for p50= 0.0645}	
" S ":	15	1.54537		0.6856 (8.135)
"SGMA":	7	1.51778		0.6770 (8.404)
"Ramp":	16	B= 1.10	T= 0.8349	0.4813 (14.426)
"Attr":	44	45 2	{for p50= 0.0606}	
" S ":	17	1.57399		0.6542 (9.105)
"SGMA":	8	1.54939		0.6538 (9.116)
"Ramp":	16	B= 1.30	T= 0.8119	0.4504 (19.986)
"Attr":	64	76 3	{for p50= 0.0573}	
" S ":	20	1.59886		0.6251 (12.995)
"SGMA":	9	1.57782		0.6291 (12.837)
"Ramp":	16	B= 1.50	T= 0.7863	0.4334 (20.666)
"Attr":	67	76 3	{for p50= 0.0548}	
" S ":	23	1.61839		0.5981 (14.077)
"SGMA":	10	1.60000		0.6074 (13.703)
"Ramp":	16	B= 1.70	T= 0.7582	0.4284 (20.863)
"Attr":	70	76 3	{for p50= 0.0524}	
" S ":	25	1.63886		0.5622 (15.511)
"SGMA":	11	1.62179		0.5638 (15.450)
"Ramp":	16	B= 1.90	T= 0.7282	0.4311 (20.755)
"Attr":	72	76 3	{for p50= 0.0507}	
" S ":	28	1.65388		0.5344 (16.625)
"SGMA":	12	1.63857		0.5436 (16.256)

1

For AQL= 0.02275 (at 95%) :

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				Uniform-Robustness
				Pa ROE

"Ramp":	16	B= 0.50	T= 0.8796	0.7048 (6.655)
"Attr":	30	35 2	{for p50= 0.0878}	
" S ":	11	1.38920		0.8094 (3.816)
"SGMA":	6	1.35447		0.7841 (4.502)
"Ramp":	16	B= 0.70	T= 0.8577	0.6511 (8.112)
"Attr":	33	35 2	{for p50= 0.0808}	
" S ":	14	1.42745		0.8009 (4.047)
"SGMA":	7	1.40000		0.7649 (5.024)
"Ramp":	16	B= 0.90	T= 0.8337	0.5984 (11.111)
"Attr":	36	45 2	{for p50= 0.0745}	
" S ":	15	1.47000		0.7484 (5.671)
"SGMA":	8	1.43427		0.7484 (5.671)
"Ramp":	16	B= 1.10	T= 0.8136	0.5648 (13.692)
"Attr":	51	60 3	{for p50= 0.0713}	
" S ":	18	1.48793		0.7585 (6.807)
"SGMA":	9	1.46604		0.7291 (7.850)
"Ramp":	16	B= 1.30	T= 0.7885	0.5414 (14.523)
"Attr":	53	60 3	{for p50= 0.0680}	
" S ":	21	1.50946		0.7450 (7.285)
"SGMA":	10	1.49059		0.7127 (8.432)
"Ramp":	16	B= 1.50	T= 0.7611	0.5305 (14.908)
"Attr":	56	60 3	{for p50= 0.0652}	
" S ":	23	1.53006		0.7227 (8.080)
"SGMA":	11	1.51268		0.6795 (9.615)
"Ramp":	16	B= 1.70	T= 0.7316	0.5298 (14.936)
"Attr":	58	60 3	{for p50= 0.0629}	
" S ":	26	1.54667		0.7066 (8.651)
"SGMA":	12	1.53121		0.6638 (10.173)
"Ramp":	16	B= 1.90	T= 0.7000	0.5377 (14.653)
"Attr":	60	60 3	{for p50= 0.0612}	
" S ":	28	1.55939		0.6903 (9.231)
"SGMA":	13	1.54495		0.6519 (10.595)

1

For AQL= 0.02872 (at 95%) :

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				Uniform-Robustness
				Pa ROE

"Ramp":	16	B= 0.50	T= 0.8610	0.7362 (4.706)
"Attr":	26	28 2	{for p50= 0.1008}	
" S ":	10	1.31356		0.8539 (2.333)
"SGMA":	6	1.27708		0.8225 (3.100)
"Ramp":	16	B= 0.70	T= 0.8368	0.7142 (5.725)
"Attr":	28	28 2	{for p50= 0.0939}	
" S ":	13	1.34482		0.8502 (2.422)
"SGMA":	7	1.31680		0.8123 (3.344)
"Ramp":	16	B= 0.90	T= 0.8147	0.6738 (8.689)
"Attr":	41	47 3	{for p50= 0.0879}	
" S ":	17	1.37514		0.8557 (2.965)
"SGMA":	9	1.35365		0.8115 (4.358)
"Ramp":	16	B= 1.10	T= 0.7900	0.6456 (9.575)
"Attr":	43	47 3	{for p50= 0.0839}	
" S ":	17	1.40155		0.8296 (3.788)
"SGMA":	9	1.37966		0.7898 (5.040)
"Ramp":	16	B= 1.30	T= 0.7652	0.6294 (10.086)
"Attr":	45	47 3	{for p50= 0.0804}	
" S ":	20	1.42114		0.8278 (3.844)

"SGMA":	10	1.40244		0.7802 (5.340)
"Ramp":	16	B= 1.50	T= 0.7340	0.6252 (10.218)
"Attr":	47	47 3	{for p50= 0.0775}	
" S ":	22	1.43932		0.8176 (4.164)
"SGMA":	11	1.42219		0.7573 (6.061)
"Ramp":	16	B= 1.70	T= 0.7029	0.6296 (12.124)
"Attr":	62	68 4	{for p50= 0.0752}	
" S ":	24	1.45382		0.8094 (5.320)
"SGMA":	12	1.43802		0.7498 (7.574)
"Ramp":	16	B= 1.90	T= 0.6704	0.6396 (11.745)
"Attr":	63	68 4	{for p50= 0.0734}	
" S ":	26	1.46528		0.8032 (5.556)
"SGMA":	13	1.45062		0.7441 (7.791)

1

For AQL= 0.03593 (at 95%) :

				Uniform-Robustness	
				Pa	ROB
"Ramp":	16	B= 0.50	T= 0.8389	0.8008	(4.221)
"Attr":	31	38 3	{for p50= 0.1166}		
" S ":	11	1.22290		0.8990	(1.443)
"SGMA":	7	1.19233		0.8749	(2.125)
"Ramp":	16	B= 0.70	T= 0.8157	0.7667	(5.124)
"Attr":	34	38 3	{for p50= 0.1072}		
" S ":	14	1.26607		0.8993	(1.433)
"SGMA":	8	1.24172		0.8606	(2.527)
"Ramp":	16	B= 0.90	T= 0.7908	0.7383	(5.989)
"Attr":	35	38 3	{for p50= 0.1023}		
" S ":	16	1.29010		0.8979	(1.472)
"SGMA":	9	1.26860		0.8562	(2.654)
"Ramp":	16	B= 1.10	T= 0.7646	0.7180	(6.563)
"Attr":	37	38 3	{for p50= 0.0981}		
" S ":	18	1.31185		0.8952	(1.550)
"SGMA":	10	1.29256		0.8510	(2.800)
"Ramp":	16	B= 1.30	T= 0.7359	0.7097	(8.102)
"Attr":	49	54 4	{for p50= 0.0946}		
" S ":	20	1.33058		0.8923	(1.946)
"SGMA":	11	1.31307		0.8357	(3.155)
"Ramp":	16	B= 1.50	T= 0.7052	0.7105	(8.077)
"Attr":	50	54 4	{for p50= 0.0917}		
" S ":	22	1.34653		0.8896	(2.036)
"SGMA":	12	1.33050		0.8314	(3.998)
"Ramp":	16	B= 1.70	T= 0.6729	0.7179	(7.825)
"Attr":	52	54 4	{for p50= 0.0894}		
" S ":	25	1.35880		0.8932	(1.914)
"SGMA":	13	1.34465		0.8273	(4.252)
" S ":	24	1.37049		0.8182	(4.443)
"SGMA":	13	1.35559			

1

For AQL= 0.04457 (at 95%) :

				Uniform-Robustness	
				Pa	ROB
"Ramp":	16	B= 0.50	T= 0.8179	0.8356	(2.874)
"Attr":	28	30 3	{for p50= 0.1292}		
" S ":	13	1.15443		0.9365	(0.340)
"SGMA":	8	1.13038		0.9058	(1.110)
"Ramp":	16	B= 0.70	T= 0.7912	0.8133	(3.437)
"Attr":	29	30 3	{for p50= 0.1234}		
" S ":	15	1.17945		0.9385	(0.289)
"SGMA":	9	1.15839		0.9042	(1.151)
"Ramp":	16	B= 0.90	T= 0.7651	0.7924	(4.796)
"Attr":	39	44 4	{for p50= 0.1186}		
" S ":	17	1.20076		0.9399	(0.307)
"SGMA":	10	1.18199		0.9027	(1.439)
"Ramp":	16	B= 1.10	T= 0.7370	0.7810	(5.144)
"Attr":	40	44 4	{for p50= 0.1144}		
" S ":	17	1.22234		0.9285	(0.653)
"SGMA":	10	1.20324		0.8905	(1.210)
"Ramp":	16	B= 1.30	T= 0.7067	0.7784	(5.223)
"Attr":	42	44 4	{for p50= 0.1108}		
" S ":	19	1.23944		0.9298	(0.615)
"SGMA":	11	1.22222		0.8808	(2.107)
"Ramp":	16	B= 1.50	T= 0.6747	0.7827	(5.091)
"Attr":	43	44 4	{for p50= 0.1079}		
" S ":	21	1.25339		0.9314	(0.567)
"SGMA":	12	1.23772		0.8805	(2.115)
"Ramp":	16	B= 1.70	T= 0.6413	0.7922	(4.802)
"Attr":	44	44 4	{for p50= 0.1057}		
" S ":	23	1.26422		0.9336	(0.499)
"SGMA":	13	1.24985		0.8814	(2.088)
"Ramp":	16	B= 1.90	T= 0.6073	0.8042	(5.096)
"Attr":	54	58 5	{for p50= 0.1039}		
" S ":	23	1.27389		0.9274	(0.789)
"SGMA":	13	1.25941		0.8744	(2.642)

1

For AQL= 0.05480 (at 95%) :

				Uniform-Robustness	
				Pa	ROB

"Ramp":	16	B= 0.50	T= 0.7927	0.8668 (1.271)
"Attr":	21	24 3	{for p50= 0.1695}	
" S ":	8	0.99146		0.9468 (-0.071)
"SGMA":	6	0.95605		0.9327 (-0.389)
"Ramp":	16	B= 0.70	T= 0.7653	0.8492 (2.265)
"Attr":	22	24 3	{for p50= 0.1657}	
" S ":	8	1.00746		0.9416 (-0.129)
"SGMA":	6	0.97148		0.9275 (-0.506)
"Ramp":	16	B= 0.90	T= 0.7373	0.8377 (2.525)
"Attr":	22	24 3	{for p50= 0.1605}	
" S ":	10	1.02096		0.9556 (-0.127)
"SGMA":	7	0.99260		0.9347 (-0.345)
"Ramp":	16	B= 1.10	T= 0.7075	0.8322 (3.197)
"Attr":	35	35 4	{for p50= 0.1328}	
" S ":	18	1.12972		0.9599 (-0.270)
"SGMA":	11	1.11311		0.9227 (-0.742)
"Ramp":	16	B= 1.30	T= 0.6758	0.8339 (3.652)
"Attr":	43	47 5	{for p50= 0.1292}	
" S ":	19	1.14601		0.9579 (-0.249)
"SGMA":	12	1.13009		0.9233 (-0.840)
"Ramp":	16	B= 1.50	T= 0.6425	0.8408 (3.434)
"Attr":	44	47 5	{for p50= 0.1264}	
" S ":	19	1.15962		0.9523 (-0.073)
"SGMA":	12	1.14352		0.9164 (-1.058)
"Ramp":	16	B= 1.70	T= 0.6084	0.8506 (3.128)
"Attr":	45	47 5	{for p50= 0.1242}	
" S ":	21	1.16876		0.9565 (-0.204)
"SGMA":	13	1.15415		0.9191 (-0.971)
"Ramp":	16	B= 1.90	T= 0.5741	0.8615 (2.784)
"Attr":	46	47 5	{for p50= 0.1225}	
" S ":	23	1.17579		0.9606 (-0.332)
"SGMA":	14	1.16243		0.9223 (-0.870)

1

For AQL= 0.06681 (at 95%) :

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				Uniform-Robustness	
				Pa	POB
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"Ramp":	16	B= 0.50	T= 0.7662	0.8883 (1.266)	
"Attr":	19	20 3	{for p50= 0.1925}		
" S ":	8	0.90074		0.9607 (-0.220)	
"SGMA":	6	0.86857		0.9466 (-0.069)	
"Ramp":	16	B= 0.70	T= 0.7372	0.8796 (1.445)	
"Attr":	19	20 3	{for p50= 0.1888}		
" S ":	9	0.91078		0.9664 (-0.237)	
"SGMA":	7	0.88232		0.9554 (-0.111)	
"Ramp":	16	B= 0.90	T= 0.7075	0.8730 (1.579)	
"Attr":	7	27 3	{for p50= 0.1605}		
" S ":	7	0.89678		0.9515 (-0.031)	
"SGMA":	7	0.89678		0.9515 (-0.031)	
"Ramp":	16	B= 1.10	T= 0.6762	0.8726 (1.913)	
"Attr":	26	29 4	{for p50= 0.1794}		
" S ":	9	0.94729		0.9570 (-0.173)	
"SGMA":	7	0.91768		0.9455 (-0.112)	
"Ramp":	16	B= 1.30	T= 0.6431	0.8771 (1.802)	
"Attr":	26	29 4	{for p50= 0.1752}		
" S ":	11	0.95757		0.9642 (-0.350)	
"SGMA":	8	0.93363		0.9518 (-0.044)	
"Ramp":	16	B= 1.50	T= 0.6090	0.8847 (1.614)	
"Attr":	27	29 4	{for p50= 0.1718}		
" S ":	11	0.97126		0.9604 (-0.258)	
"SGMA":	8	0.94697		0.9477 (-0.056)	
"Ramp":	16	B= 1.70	T= 0.5744	0.8939 (1.385)	
"Attr":	27	29 4	{for p50= 0.1694}		
" S ":	13	0.97709		0.9705 (-0.506)	
"SGMA":	9	0.95673		0.9543 (-0.106)	
"Ramp":	16	B= 1.90	T= 0.5401	0.9032 (1.155)	
"Attr":	27	29 4	{for p50= 0.1675}		
" S ":	13	0.98468		0.9686 (-0.459)	
"SGMA":	9	0.96416		0.9520 (-0.050)	

1

For AQL= 0.08076 (at 95%) :

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				Uniform-Robustness	
				Pa	POB
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"Ramp":	16	B= 0.50	T= 0.7379	0.9081 (0.769)	
"Attr":	16	16 3	{for p50= 0.2197}		
" S ":	7	0.80670		0.9621 (-0.222)	
"SGMA":	6	0.77309		0.9566 (-0.157)	
"Ramp":	16	B= 0.70	T= 0.7070	0.9022 (1.075)	
"Attr":	21	24 4	{for p50= 0.2134}		
" S ":	9	0.82033		0.9752 (-0.566)	
"SGMA":	7	0.79469		0.9648 (-0.332)	
"Ramp":	16	B= 0.90	T= 0.6758	0.9010 (1.101)	
"Attr":	22	24 4	{for p50= 0.2094}		
" S ":	9	0.83449		0.9725 (-0.505)	
"SGMA":	7	0.80841		0.9617 (-0.283)	
"Ramp":	16	B= 1.10	T= 0.6430	0.9034 (1.047)	
"Attr":	22	24 4	{for p50= 0.2045}		
" S ":	10	0.84909		0.9756 (-0.577)	
"SGMA":	8	0.82551		0.9670 (-0.382)	
"Ramp":	16	B= 1.30	T= 0.6090	0.9092 (0.916)	
"Attr":	23	24 4	{for p50= 0.2004}		
" S ":	10	0.86412		0.9727 (-0.510)	

"SGMA":	8	0.84011		0.9637 (-0.308)
"Ramp":	16	B= 1.50	T= 0.5742	0.9101 (-0.745)
"Attr":	23	24 4	{for p50= 0.1975}	
" S ":	10	0.87486		0.9704 (-0.458)
"SGMA":	8	0.85056		0.9614 (-0.251)
"Ramp":	16	B= 1.70	T= 0.5395	0.9249 (0.565)
"Attr":	23	24 4	{for p50= 0.1951}	
" S ":	12	0.87914		0.9765 (-0.595)
"SGMA":	9	0.85915		0.9672 (-0.587)
"Ramp":	16	B= 1.90	T= 0.5035	0.9324 (0.355)
"Attr":	24	24 4	{for p50= 0.1934}	
" S ":	12	0.88545		0.9752 (-0.567)
"SGMA":	9	0.86533		0.9658 (-0.354)

1

For AQL= 0.09680 (at 95%) :

				Uniform-Robustness	
				Pa	ROB
				-----	-----
"Ramp":	16	B= 0.50	T= 0.7069	0.9213	(0.589)
"Attr":	19	20 4	{for p50= 0.2452}		
" S ":	8	0.71509		0.9774	(-0.582)
"SGMA":	7	0.68955		0.9743	(-0.498)
"Ramp":	16	B= 0.70	T= 0.6749	0.9210	(0.595)
"Attr":	19	20 4	{for p50= 0.2420}		
" S ":	8	0.72593		0.9756	(-0.525)
"SGMA":	7	0.70000		0.9725	(-0.461)
"Ramp":	16	B= 0.90	T= 0.6421	0.9221	(0.572)
"Attr":	19	20 4	{for p50= 0.2370}		
" S ":	8	0.74257		0.9726	(-0.463)
"SGMA":	7	0.71605		0.9695	(-0.400)
"Ramp":	16	B= 1.10	T= 0.6083	0.9264	(0.485)
"Attr":	20	20 4	{for p50= 0.2322}		
" S ":	10	0.75266		0.9824	(-0.666)
"SGMA":	8	0.73175		0.9745	(-0.504)
"Ramp":	16	B= 1.30	T= 0.5735	0.9326	(0.408)
"Attr":	24	26 5	{for p50= 0.2284}		
" S ":	10	0.76549		0.9805	(-0.714)
"SGMA":	8	0.74423		0.9725	(-0.521)
"Ramp":	16	B= 1.50	T= 0.5385	0.9395	(0.246)
"Attr":	25	26 5	{for p50= 0.2255}		
" S ":	11	0.77289		0.9807	(-0.719)
"SGMA":	9	0.75357		0.9772	(-0.636)
"Ramp":	16	B= 1.70	T= 0.5040	0.9462	(0.088)
"Attr":	25	26 5	{for p50= 0.2233}		
" S ":	11	0.78063		0.9795	(-0.690)
"SGMA":	9	0.76111		0.9755	(-0.605)

"Ramp":	16	B= 1.90	T= 0.4718	0.9542 (0.000)
"Attr":	25	26 5	{for p50= 0.2218}	
" S ":	11	0.78584		0.9786 (-0.670)
"SGMA":	9	0.76619		0.9749 (-0.583)

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For AQL= 0.01072 (at 95%) :

				Uniform-Robustness	
				Pa	ROB
				-----	-----
"Ramp":	32	B= 0.50	T= 0.9387	0.3360	(24.560)
"Attr":	67	76 2	{for p50= 0.0392}		
" S ":	23	1.77259		0.3542	(23.810)
"SGMA":	9	1.75245		0.4550	(19.799)
"Ramp":	32	B= 0.70	T= 0.9252	0.2273	(28.907)
"Attr":	72	76 2	{for p50= 0.0368}		
" S ":	26	1.80724		0.2834	(26.664)
"SGMA":	10	1.78917		0.4053	(21.788)
"Ramp":	32	B= 0.90	T= 0.9125	0.1471	(41.514)
"Attr":	109	127 3	{for p50= 0.0337}		
" S ":	32	1.84436		0.1989	(38.835)
"SGMA":	12	1.82949		0.3205	(32.548)
"Ramp":	32	B= 1.10	T= 0.8976	0.1007	(43.914)
"Attr":	117	127 3	{for p50= 0.0312}		
" S ":	32	1.87616		0.1319	(42.300)
"SGMA":	14	1.86348		0.2641	(35.466)
"Ramp":	32	B= 1.30	T= 0.8802	0.0739	(45.300)
"Attr":	125	127 3	{for p50= 0.0292}		
" S ":	44	1.90310		0.0836	(44.797)
"SGMA":	16	1.89204		0.2152	(37.995)
"Ramp":	32	B= 1.50	T= 0.8595	0.0597	(55.262)
"Attr":	168	183 4	{for p50= 0.0277}		
" S ":	51	1.92497		0.0502	(55.850)
"SGMA":	18	1.91535		0.1748	(48.114)
"Ramp":	32	B= 1.70	T= 0.8364	0.0518	(55.751)
"Attr":	176	183 4	{for p50= 0.0264}		
" S ":	57	1.94517		0.0294	(57.140)
"SGMA":	20	1.93649		0.1400	(50.277)
"Ramp":	32	B= 1.90	T= 0.8107	0.0492	(64.432)
"Attr":	223	243 5	{for p50= 0.0254}		
" S ":	64	1.96131		0.0165	(66.766)
"SGMA":	22	1.95353		0.1126	(59.897)

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For AQL= 0.01390 (at 95%) :

Uniform-Robustness
Pa ROB

"Ramp":	32	R= 0.50	T= 0.9264	0.4275 (12.257)
"Attr":	56	58 2	{for p50= 0.0475}	
" S ":	21	1.69114		0.4862 (13.167)
"SGMA":	9	1.67000		0.5325 (14.564)
"Ramp":	32	R= 0.70	T= 0.9133	0.2991 (29.567)
"Attr":	84	98 3	{for p50= 0.0433}	
" S ":	27	1.73001		0.4052 (24.740)
"SGMA":	11	1.71332		0.4611 (22.295)
"Ramp":	32	R= 0.90	T= 0.8990	0.2113 (33.553)
"Attr":	91	98 3	{for p50= 0.0401}	
" S ":	33	1.76349		0.3232 (28.445)
"SGMA":	13	1.74972		0.4062 (24.700)
"Ramp":	32	R= 1.10	T= 0.8824	0.1566 (36.027)
"Attr":	97	98 3	{for p50= 0.0375}	
" S ":	39	1.79229		0.2492 (31.330)
"SGMA":	15	1.78050		0.3542 (27.065)
"Ramp":	32	R= 1.30	T= 0.8625	0.1264 (44.871)
"Attr":	131	141 4	{for p50= 0.0356}	
" S ":	44	1.81453		0.1931 (41.258)
"SGMA":	17	1.80398		0.3103 (34.855)
"Ramp":	32	R= 1.50	T= 0.8402	0.1080 (45.176)
"Attr":	137	141 4	{for p50= 0.0332}	
" S ":	51	1.83621		0.1384 (44.221)
"SGMA":	19	1.82703		0.2663 (37.247)
"Ramp":	32	R= 1.70	T= 0.8152	0.1000 (53.333)
"Attr":	174	187 5	{for p50= 0.0325}	
" S ":	57	1.85415		0.0993 (53.374)
"SGMA":	21	1.84587		0.2290 (43.240)
"Ramp":	32	R= 1.90	T= 0.7877	0.0996 (53.360)
"Attr":	180	187 5	{for p50= 0.0314}	
" S ":	63	1.86839		0.0715 (55.119)
"SGMA":	23	1.86085		0.1980 (47.181)

For AQL= 0.01786 (at 95%) :

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				Uniform-Robustness
				Pa ROB

"Ramp":	32	R= 0.50	T= 0.9143	0.5057 (17.773)
"Attr":	64	76 3	{for p50= 0.0554}	
" S ":	22	1.61422		0.6035 (13.859)
"SGMA":	10	1.59500		0.6134 (13.464)
"Ramp":	32	R= 0.70	T= 0.8999	0.3804 (22.782)
"Attr":	72	76 3	{for p50= 0.0509}	
" S ":	28	1.65108		0.5403 (16.590)
"SGMA":	12	1.63580		0.5474 (16.104)

"Ramp":	32	R= 0.90	T= 0.8839	0.2905 (31.737)
"Attr":	98	110 4	{for p50= 0.0476}	
" S ":	33	1.68148		0.4741 (22.509)
"SGMA":	14	1.66834		0.5027 (21.523)
"Ramp":	32	R= 1.10	T= 0.8648	0.2357 (34.873)
"Attr":	103	110 4	{for p50= 0.0452}	
" S ":	39	1.70443		0.4153 (25.731)
"SGMA":	16	1.69321		0.4633 (23.421)
"Ramp":	32	R= 1.30	T= 0.8433	0.2004 (36.074)
"Attr":	108	110 4	{for p50= 0.0430}	
" S ":	44	1.72716		0.3527 (28.742)
"SGMA":	18	1.71712		0.4211 (25.453)
"Ramp":	32	R= 1.50	T= 0.8191	0.1816 (42.602)
"Attr":	137	146 5	{for p50= 0.0411}	
" S ":	50	1.74677		0.2941 (36.366)
"SGMA":	20	1.73786		0.3811 (31.542)
"Ramp":	32	R= 1.70	T= 0.7922	0.1766 (42.875)
"Attr":	142	146 5	{for p50= 0.0397}	
" S ":	56	1.76224		0.2454 (39.061)
"SGMA":	22	1.75423		0.3467 (33.447)
"Ramp":	32	R= 1.90	T= 0.7631	0.1808 (47.747)
"Attr":	172	183 6	{for p50= 0.0386}	
" S ":	61	1.77503		0.2864 (46.153)
"SGMA":	24	1.76764		0.3165 (39.320)

For AQL= 0.02275 (at 95%) :

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				Uniform-Robustness
				Pa ROB

"Ramp":	32	R= 0.50	T= 0.9009	0.5810 (13.115)
"Attr":	57	60 3	{for p50= 0.0642}	
" S ":	23	1.53803		0.7097 (8.540)
"SGMA":	11	1.52056		0.6701 (9.950)
"Ramp":	32	R= 0.70	T= 0.8848	0.4674 (20.536)
"Attr":	78	86 4	{for p50= 0.0599}	
" S ":	29	1.56979		0.6734 (11.788)
"SGMA":	13	1.55578		0.6374 (13.303)
"Ramp":	32	R= 0.90	T= 0.8663	0.3872 (23.947)
"Attr":	82	86 4	{for p50= 0.0568}	
" S ":	34	1.59298		0.6352 (13.396)
"SGMA":	15	1.58190		0.6088 (14.516)
"Ramp":	32	R= 1.10	T= 0.8457	0.3305 (26.361)
"Attr":	86	86 4	{for p50= 0.0540}	
" S ":	39	1.61743		0.5885 (15.373)
"SGMA":	17	1.60679		0.5759 (15.916)
"Ramp":	32	R= 1.30	T= 0.8222	0.2970 (31.989)

"Attr":	109	114	5	(for p50= 0.0517)	
" S ":	44	1.63933			0.5394 (20.119)
"SGMA":	19	1.62881			0.5424 (19.967)
"Ramp":	32	B= 1.50		T= 0.7960	0.2827 (32.290)
"Attr":	113	114	5	(for p50= 0.0498)	
" S ":	49	1.65557			0.4935 (22.324)
"SGMA":	21	1.64695			0.5115 (21.422)
"Ramp":	32	B= 1.70		T= 0.7674	0.2832 (36.714)
"Attr":	138	144	6	(for p50= 0.0483)	
" S ":	55	1.66938			0.4524 (27.399)
"SGMA":	23	1.66165			0.4839 (25.662)
"Ramp":	32	B= 1.90		T= 0.7365	0.2962 (35.997)
"Attr":	141	144	6	(for p50= 0.0472)	
" S ":	60	1.67963			0.4190 (29.236)
"SGMA":	25	1.67251			0.4616 (26.890)

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For AQL= 0.02872 (at 95%) :

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Uniform-Robustness
Pa ROE

"Ramp":	32	B= 0.50		T= 0.8854	0.6533 (11.226)
"Attr":	62	68	4	(for p50= 0.0747)	
" S ":	24	1.45743			0.8045 (5.503)
"SGMA":	12	1.44158			0.7459 (7.723)
"Ramp":	32	B= 0.70		T= 0.8671	0.5609 (14.721)
"Attr":	66	68	4	(for p50= 0.0708)	
" S ":	29	1.48338			0.7891 (6.087)
"SGMA":	14	1.47014			0.7283 (8.388)
"Ramp":	32	B= 0.90		T= 0.8472	0.4872 (20.144)
"Attr":	84	90	5	(for p50= 0.0673)	
" S ":	34	1.50732			0.7674 (7.949)
"SGMA":	16	1.49590			0.7077 (10.547)
"Ramp":	32	B= 1.10		T= 0.8245	0.4384 (22.268)
"Attr":	88	90	5	(for p50= 0.0643)	
" S ":	39	1.52932			0.7405 (9.121)
"SGMA":	18	1.51926			0.6846 (11.551)
"Ramp":	32	B= 1.30		T= 0.7991	0.4113 (26.309)
"Attr":	107	114	6	(for p50= 0.0619)	
" S ":	43	1.54823			0.7099 (11.764)
"SGMA":	20	1.53902			0.6621 (14.102)
"Ramp":	32	B= 1.50		T= 0.7708	0.4060 (26.648)
"Attr":	111	114	6	(for p50= 0.0601)	
" S ":	48	1.56257			0.6861 (12.927)
"SGMA":	22	1.55426			0.6433 (15.026)
"Ramp":	32	B= 1.70		T= 0.7405	0.4147 (26.224)
"Attr":	113	114	6	(for p50= 0.0585)	
" S ":	53	1.57469			0.6632 (14.648)

"SGMA":	22	1.55426			0.6632 (14.648)
"Ramp":	32	B= 1.90		T= 0.7085	0.4340 (27.813)
"Attr":	133	138	7	(for p50= 0.0573)	
" S ":	56	1.58458			0.6402 (16.697)
"SGMA":	25	1.57738			0.6087 (18.397)

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For AQL= 0.03593 (at 95%) :

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Uniform-Robustness
Pa ROE

"Ramp":	32	B= 0.50		T= 0.8676	0.7216 (7.299)
"Attr":	53	54	4	(for p50= 0.0873)	
" S ":	24	1.37258			0.8752 (2.522)
"SGMA":	13	1.35766			0.8162 (4.510)
"Ramp":	32	B= 0.70		T= 0.8480	0.6446 (11.890)
"Attr":	68	72	5	(for p50= 0.0830)	
" S ":	29	1.39779			0.8707 (3.087)
"SGMA":	15	1.38531			0.8053 (5.632)
"Ramp":	32	B= 0.90		T= 0.8261	0.5861 (14.169)
"Attr":	71	72	5	(for p50= 0.0794)	
" S ":	34	1.42019			0.8627 (3.397)
"SGMA":	17	1.40943			0.7930 (6.111)
"Ramp":	32	B= 1.10		T= 0.8014	0.5489 (17.557)
"Attr":	87	91	6	(for p50= 0.0763)	
" S ":	38	1.44030			0.8480 (4.430)
"SGMA":	19	1.43057			0.7798 (7.449)
"Ramp":	32	B= 1.30		T= 0.7738	0.5337 (18.220)
"Attr":	90	91	6	(for p50= 0.0739)	
" S ":	43	1.45585			0.8401 (4.809)
"SGMA":	21	1.44718			0.7689 (7.929)
"Ramp":	32	B= 1.50		T= 0.7439	0.5362 (19.911)
"Attr":	106	110	7	(for p50= 0.0720)	
" S ":	47	1.46919			0.8286 (5.340)
"SGMA":	23	1.46120			0.7587 (9.207)
"Ramp":	32	B= 1.70		T= 0.7122	0.5516 (19.172)
"Attr":	108	110	7	(for p50= 0.0704)	
" S ":	52	1.47992			0.8214 (6.190)
"SGMA":	25	1.47267			0.7500 (9.623)
"Ramp":	32	B= 1.90		T= 0.6790	0.5767 (17.964)
"Attr":	110	110	7	(for p50= 0.0692)	
" S ":	54	1.48847			0.8093 (6.771)
"SGMA":	26	1.48145			0.7399 (10.109)

1

For AQL= 0.04457 (at 95%) :

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Uniform-Robustness

				Pa	ROB
"Ramp":	32	B= 0.50	T= 0.8483	0.7763	(6.071)
"Attr":	55	58 5	{for p50= 0.1014}		
" S ":	25	1.28709		0.9269	(0.708)
"SGMA":	14	1.27368		0.8723	(2.719)
"Ramp":	32	B= 0.70	T= 0.8268	0.7191	(2.069)
"Attr":	58	58 5	{for p50= 0.0968}		
" S ":	29	1.31171		0.9240	(0.910)
"SGMA":	16	1.30000		0.8666	(2.513)
"Ramp":	32	B= 0.90	T= 0.8029	0.6770	(10.702)
"Attr":	71	73 6	{for p50= 0.0932}		
" S ":	33	1.33183		0.9210	(1.135)
"SGMA":	18	1.32143		0.8615	(3.470)
"Ramp":	32	B= 1.10	T= 0.7759	0.6549	(12.772)
"Attr":	85	89 7	{for p50= 0.0902}		
" S ":	38	1.34848		0.9211	(1.250)
"SGMA":	20	1.33937		0.8567	(4.038)
"Ramp":	32	B= 1.30	T= 0.7466	0.6493	(13.016)
"Attr":	87	89 7	{for p50= 0.0878}		
" S ":	42	1.36292		0.9180	(1.386)
"SGMA":	22	1.35461		0.8523	(4.231)
"Ramp":	32	B= 1.50	T= 0.7152	0.6587	(13.697)
"Attr":	101	105 8	{for p50= 0.0858}		
" S ":	46	1.37483		0.9155	(1.621)
"SGMA":	24	1.36719		0.8487	(4.761)
"Ramp":	32	B= 1.70	T= 0.6822	0.6786	(12.759)
"Attr":	102	105 8	{for p50= 0.0842}		
" S ":	48	1.38460		0.9095	(1.905)
"SGMA":	25	1.37723		0.8419	(5.084)
"Ramp":	32	B= 1.90	T= 0.6482	0.7046	(11.540)
"Attr":	104	105 8	{for p50= 0.0830}		
" S ":	53	1.39180		0.9120	(1.788)
"SGMA":	27	1.38511		0.8415	(5.103)

For AQL= 0.05480 (at 95%) :

Uniform-Robustness

				Pa	ROB
"Ramp":	32	B= 0.50	T= 0.8269	0.8212	(4.539)
"Attr":	56	59 6	{for p50= 0.1174}		
" S ":	25	1.20065		0.9562	(-0.217)
"SGMA":	15	1.18815		0.9149	(1.238)
"Ramp":	32	B= 0.70	T= 0.8036	0.7815	(5.539)
"Attr":	59	59 6	{for p50= 0.1128}		
" S ":	29	1.22290		0.9572	(-0.255)
"SGMA":	17	1.21199		0.9133	(1.292)

"Ramp":	32	B= 0.90	T= 0.7773	0.7565	(7.535)
"Attr":	70	72 7	{for p50= 0.1091}		
" S ":	33	1.24084		0.9583	(-0.323)
"SGMA":	19	1.23114		0.9124	(1.462)
"Ramp":	32	B= 1.10	T= 0.7486	0.7451	(7.977)
"Attr":	72	72 7	{for p50= 0.1061}		
" S ":	37	1.25644		0.9589	(-0.347)
"SGMA":	21	1.24771		0.9114	(1.502)
"Ramp":	32	B= 1.30	T= 0.7176	0.7478	(8.551)
"Attr":	83	85 8	{for p50= 0.1036}		
" S ":	41	1.26930		0.9597	(-0.411)
"SGMA":	23	1.26137		0.9110	(1.650)
"Ramp":	32	B= 1.50	T= 0.6848	0.7617	(7.965)
"Attr":	85	85 8	{for p50= 0.1016}		
" S ":	45	1.27978		0.9608	(-0.458)
"SGMA":	25	1.27251		0.9113	(1.639)
"Ramp":	32	B= 1.70	T= 0.6508	0.7823	(7.616)
"Attr":	96	98 9	{for p50= 0.1000}		
" S ":	47	1.28831		0.9591	(-0.415)
"SGMA":	26	1.28131		0.9083	(1.894)
"Ramp":	32	B= 1.90	T= 0.6162	0.8059	(6.547)
"Attr":	97	98 9	{for p50= 0.0988}		
" S ":	49	1.29487		0.9583	(-0.378)
"SGMA":	27	1.28813		0.9066	(1.970)

For AQL= 0.06681 (at 95%) :

Uniform-Robustness

				Pa	ROB
"Ramp":	32	B= 0.50	T= 0.8036	0.8570	(2.986)
"Attr":	49	49 6	{for p50= 0.1357}		
" S ":	25	1.11158		0.9741	(-0.775)
"SGMA":	16	1.10000		0.9455	(0.145)
"Ramp":	32	B= 0.70	T= 0.7778	0.8336	(4.103)
"Attr":	58	59 7	{for p50= 0.1309}		
" S ":	29	1.13245		0.9763	(-0.927)
"SGMA":	18	1.12234		0.9457	(0.150)
"Ramp":	32	B= 0.90	T= 0.7497	0.8200	(4.990)
"Attr":	68	70 8	{for p50= 0.1272}		
" S ":	33	1.14878		0.9784	(-1.089)
"SGMA":	20	1.13981		0.9467	(0.127)
"Ramp":	32	B= 1.10	T= 0.7192	0.8177	(5.080)
"Attr":	69	70 8	{for p50= 0.1241}		
" S ":	36	1.16291		0.9786	(-1.099)
"SGMA":	22	1.15460		0.9477	(0.088)
"Ramp":	32	B= 1.30	T= 0.6867	0.8255	(5.140)

"Attr":	79	81	9	(for p50= 0.1217)	
" S ":	40				0.9805 (-1.259)
"SGMA":	24				0.9490 (0.040)
"Ramp":	32	B=	1.50	T= 0.6526	0.8412 (4.495)
"Attr":	80	81	9	(for p50= 0.1198)	
" S ":	42				0.9801 (-1.243)
"SGMA":	25				0.9476 (0.098)
"Ramp":	32	B=	1.70	T= 0.6179	0.8595 (3.975)
"Attr":	90	92	10	(for p50= 0.1182)	
" S ":	46				0.9822 (-1.418)
"SGMA":	27				0.9500 (0.000)
"Ramp":	32	B=	1.90	T= 0.5830	0.8785 (3.149)
"Attr":	91	92	10	(for p50= 0.1171)	
" S ":	48				0.9825 (-1.432)
"SGMA":	28				0.9500 (0.001)

1

For AQL= 0.08076 (at 95%) :

```

=====
Uniform-Robustness
Pa   ROB
-----
"Ramp": 32  B= 0.50  T= 0.7776  0.8866 (1.646)
"Attr": 31  32  5  (for p50= 0.1826)
" S " : 15  0.92202  0.9800 (-0.779)
"SGMA": 11  0.90556  0.9651 (-0.392)

"Ramp": 32  B= 0.70  T= 0.7501  0.8731 (1.996)
"Attr": 32  32  5  (for p50= 0.1769)
" S " : 17  0.94186  0.9823 (-0.839)
"SGMA": 12  0.92715  0.9656 (-0.404)

"Ramp": 32  B= 0.90  T= 0.7202  0.8682 (2.375)
"Attr": 38  40  6  (for p50= 0.1725)
" S " : 18  0.95843  0.9819 (-0.926)
"SGMA": 13  0.94434  0.9665 (-0.478)

"Ramp": 32  B= 1.10  T= 0.6881  0.8715 (2.278)
"Attr": 39  40  6  (for p50= 0.1687)
" S " : 18  0.97352  0.9789 (-0.838)
"SGMA": 13  0.95920  0.9623 (-0.357)

"Ramp": 32  B= 1.30  T= 0.6541  0.8822 (1.967)
"Attr": 40  40  6  (for p50= 0.1660)
" S " : 20  0.98296  0.9821 (-0.931)
"SGMA": 14  0.97003  0.9644 (-0.418)

"Ramp": 32  B= 1.50  T= 0.6192  0.8964 (1.721)
"Attr": 46  49  7  (for p50= 0.1638)
" S " : 22  0.99087  0.9848 (-1.117)
"SGMA": 15  0.97907  0.9666 (-0.533)

"Ramp": 32  B= 1.70  T= 0.5840  0.9115 (1.237)
"Attr": 47  49  7  (for p50= 0.1621)
" S " : 22  0.99767  0.9835 (-1.076)

```

```

"SGMA": 15  0.98580  0.9828 (-0.469)
"Ramp": 32  B= 1.90  T= 0.5491  0.9256 (0.784)
"Attr": 47  49  7  (for p50= 0.1608)
" S " : 24  1.00185  0.9863 (-1.167)
"SGMA": 16  0.99096  0.9675 (-0.562)

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For AQL= 0.09680 (at 95%) :

```

=====
Uniform-Robustness
Pa   ROB
-----
"Ramp": 32  B= 0.50  T= 0.7497  0.9087 (1.028)
"Attr": 32  33  6  (for p50= 0.2069)
" S " : 14  0.83315
"SGMA": 11  0.81712  0.9825 (-0.857)
                                0.9727 (-0.599)

"Ramp": 32  B= 0.70  T= 0.7202  0.9033 (1.231)
"Attr": 33  33  6  (for p50= 0.2017)
" S " : 16  0.84986  0.9856 (-0.940)
"SGMA": 12  0.83569  0.9740 (-0.633)

"Ramp": 32  B= 0.90  T= 0.6885  0.9043 (1.205)
"Attr": 33  33  6  (for p50= 0.1973)
" S " : 17  0.86488  0.9858 (-0.945)
"SGMA": 13  0.85137  0.9754 (-0.669)

"Ramp": 32  B= 1.10  T= 0.6549  0.9108 (1.150)
"Attr": 39  41  7  (for p50= 0.1938)
" S " : 19  0.87620  0.9864 (-1.127)
"SGMA": 14  0.86404  0.9769 (-0.790)

"Ramp": 32  B= 1.30  T= 0.6201  0.9211 (0.850)
"Attr": 40  41  7  (for p50= 0.1911)
" S " : 19  0.88631  0.9870 (-1.086)
"SGMA": 14  0.87400  0.9748 (-0.727)

"Ramp": 32  B= 1.50  T= 0.5846  0.9331 (0.497)
"Attr": 40  41  7  (for p50= 0.1890)
" S " : 20  0.89334  0.9878 (-1.111)
"SGMA": 15  0.88159  0.9770 (-0.793)

"Ramp": 32  B= 1.70  T= 0.5493  0.9445 (0.162)
"Attr": 40  41  7  (for p50= 0.1873)
" S " : 20  0.89966  0.9869 (-1.084)
"SGMA": 15  0.88782  0.9756 (-0.753)

"Ramp": 32  B= 1.90  T= 0.5147  0.9545 (-0.142)
"Attr": 46  48  8  (for p50= 0.1861)
" S " : 22  0.90299  0.9897 (-1.263)
"SGMA": 16  0.89224  0.9782 (-0.896)

```

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For AQL= 0.01072 (at 95%) :

=====					Uniform-Robustness	
					Pa	ROB
"Ramp":	64	R= 0.50	T= 0.9502		0.1247	(42.674)
"Attr":	125	127 3	{for p50= 0.0293}			
" S ":	44	1.90149			0.0853	(44.711)
"SGMA":	16	1.89843			0.2171	(37.897)
"Ramp":	64	R= 0.70	T= 0.9398		0.0467	(56.661)
"Attr":	169	183 4	{for p50= 0.0275}			
" S ":	51	1.92861			0.0476	(56.614)
"SGMA":	18	1.91897			0.1709	(48.358)
"Ramp":	64	R= 0.90	T= 0.9285		0.0170	(57.912)
"Attr":	183	183 4	{for p50= 0.0255}			
" S ":	64	1.95963			0.0171	(57.905)
"SGMA":	22	1.95185			0.1141	(51.885)
"Ramp":	64	R= 1.10	T= 0.9148		0.0072	(67.437)
"Attr":	237	243 5	{for p50= 0.0239}			
" S ":	77	1.98551			0.0054	(67.563)
"SGMA":	26	1.97898			0.0737	(62.674)
"Ramp":	64	R= 1.30	T= 0.8985		0.0037	(75.554)
"Attr":	293	306 6	{for p50= 0.0228}			
" S ":	90	2.00563			0.0016	(76.121)
"SGMA":	30	2.00000			0.0474	(72.448)
"Ramp":	64	R= 1.50	T= 0.8789		0.0024	(83.744)
"Attr":	353	371 7	{for p50= 0.0217}			
" S ":	103	2.02541			0.0004	(83.923)
"SGMA":	34	2.02044			0.0288	(81.409)
"Ramp":	64	R= 1.70	T= 0.8568		0.0019	(83.793)
"Attr":	363	371 7	{for p50= 0.0211}			
" S ":	113	2.03566			0.0001	(83.945)
"SGMA":	37	2.03112			0.0204	(82.153)
"Ramp":	64	R= 1.90	T= 0.8320		0.0017	(90.957)
"Attr":	430	437 8	{for p50= 0.0202}			
" S ":	133	2.05434			0.0000	(91.119)
"SGMA":	43	2.05045			0.0099	(90.174)

1
For AQL= 0.01390 (at 95%) :

=====					Uniform-Robustness	
					Pa	ROB
"Ramp":	64	R= 0.50	T= 0.9403		0.1951	(41.131)
"Attr":	129	141 4	{for p50= 0.0359}			
" S ":	41	1.81132			0.2073	(40.466)
"SGMA":	16	1.80000			0.3212	(34.260)
"Ramp":	64	R= 0.70	T= 0.9294		0.0829	(47.241)
"Attr":	141	141 4	{for p50= 0.0330}			
" S ":	20	1.82705			0.2449	(38.418)
"SGMA":	20	1.83235				
"Ramp":	64	R= 0.90	T= 0.9165		0.0367	(57.304)
"Attr":	183	187 5	{for p50= 0.0309}			
" S ":	66	1.87495			0.0603	(55.822)
"SGMA":	24	1.86774			0.1839	(48.069)
"Ramp":	64	R= 1.10	T= 0.9011		0.0187	(65.642)
"Attr":	228	236 6	{for p50= 0.0292}			
" S ":	78	1.89882			0.0288	(64.950)
"SGMA":	28	1.89266			0.1347	(57.471)
"Ramp":	64	R= 1.30	T= 0.8823		0.0120	(72.784)
"Attr":	274	286 7	{for p50= 0.0280}			
" S ":	90	1.91705			0.0135	(72.669)
"SGMA":	32	1.91167			0.0988	(66.056)
"Ramp":	64	R= 1.50	T= 0.8610		0.0089	(73.022)
"Attr":	285	286 7	{for p50= 0.0268}			
" S ":	106	1.93431			0.0050	(73.330)
"SGMA":	37	1.92970			0.0674	(68.483)
"Ramp":	64	R= 1.70	T= 0.8370		0.0078	(79.365)
"Attr":	334	337 8	{for p50= 0.0259}			
" S ":	118	1.94876			0.0020	(79.850)
"SGMA":	41	1.94459			0.0475	(76.015)
"Ramp":	64	R= 1.90	T= 0.8103		0.0078	(85.375)
"Attr":	383	390 9	{for p50= 0.0252}			
" S ":	131	1.96002			0.0008	(86.010)
"SGMA":	45	1.95625			0.0339	(83.014)

1
For AQL= 0.01786 (at 95%) :

=====					Uniform-Robustness	
					Pa	ROB
"Ramp":	64	R= 0.50	T= 0.9299		0.2740	(37.478)
"Attr":	134	146 5	{for p50= 0.0422}			
" S ":	47	1.73499			0.3284	(34.461)
"SGMA":	19	1.72556			0.4046	(30.236)
"Ramp":	64	R= 0.70	T= 0.9177		0.1371	(45.066)
"Attr":	143	146 5	{for p50= 0.0395}			
" S ":	56	1.76488			0.2393	(39.403)
"SGMA":	22	1.75686			0.3422	(33.699)
"Ramp":	64	R= 0.90	T= 0.9030		0.0732	(59.940)
"Attr":	213	222 7	{for p50= 0.0360}			
" S ":	76	1.80562			0.1189	(56.821)
"SGMA":	29	1.79960			0.2429	(48.339)
"Ramp":	64	R= 1.10	T= 0.8850		0.0463	(61.769)
"Attr":	213	222 7	{for p50= 0.0359}			
" S ":	78	1.80586			0.1154	(57.057)
"SGMA":	30	1.80000			0.2385	(48.639)

"Ramp":	64	B= 1.30	T= 0.8646	0.0325 (88.278)
"Attr":	253	242 8	{for p50= 0.0342}	
" S ":	93	1.82696		0.0653 (65.707)
"SGMA":	35	1.82200		0.1843 (56.749)
"Ramp":	64	B= 1.50	T= 0.8414	0.0275 (68.484)
"Attr":	262	262 8	{for p50= 0.0330}	
" S ":	105	1.84289		0.0284 (67.704)
"SGMA":	39	1.83846		0.1467 (59.663)
"Ramp":	64	B= 1.70	T= 0.8153	0.0269 (73.730)
"Attr":	301	303 9	{for p50= 0.0321}	
" S ":	116	1.85507		0.0232 (74.020)
"SGMA":	43	1.85104		0.1178 (66.469)
"Ramp":	64	B= 1.90	T= 0.7870	0.0284 (78.545)
"Attr":	340	345 10	{for p50= 0.0313}	
" S ":	128	1.86554		0.0135 (79.209)
"SGMA":	47	1.86187		0.0944 (72.518)

1
For AQL= 0.02275 (at 95%) :

				Uniform-Robustness	
				pa	ROB
				----	----
"Ramp":	64	B= 0.50	T= 0.9182	0.3626	(22.776)
"Attr":	113	114 5	{for p50= 0.0499}		
" S ":	49	1.65437		0.4969	(22.200)
"SGMA":	21	1.64575		0.5137	(21.374)
"Ramp":	64	B= 0.70	T= 0.9043	0.2134	(40.558)
"Attr":	141	144 6	{for p50= 0.0471}		
" S ":	60	1.68026		0.4171	(29.340)
"SGMA":	25	1.67314		0.4604	(26.959)
"Ramp":	64	B= 0.90	T= 0.8871	0.1383	(75.047)
"Attr":	405	476 14	{for p50= 0.0361}		
" S ":	170	1.80016		0.0277	(65.268)
"SGMA":	65	1.79749		0.1224	(76.511)
"Ramp":	64	B= 1.10	T= 0.8675	0.0990	(56.044)
"Attr":	200	206 8	{for p50= 0.0433}		
" S ":	78	1.71915		0.2803	(44.106)
"SGMA":	32	1.71357		0.3663	(38.429)
"Ramp":	64	B= 1.30	T= 0.8451	0.0801	(61.573)
"Attr":	232	238 9	{for p50= 0.0417}		
" S ":	92	1.73644		0.2124	(52.209)
"SGMA":	37	1.73167		0.3167	(44.831)
"Ramp":	64	B= 1.50	T= 0.8197	0.0740	(66.166)
"Attr":	263	271 10	{for p50= 0.0405}		
" S ":	103	1.74974		0.1637	(59.391)
"SGMA":	41	1.74545		0.2775	(50.799)
"Ramp":	64	B= 1.70	T= 0.7919	0.0752	(66.079)

"Attr":	270	277 10	{for p50= 0.0397}		
" S ":	114	1.76104		0.1249	(62.324)
"SGMA":	45	1.75714		0.2429	(53.409)
"Ramp":	64	B= 1.90	T= 0.7616	0.0837	(69.307)
"Attr":	301	304 11	{for p50= 0.0387}		
" S ":	125	1.76589		0.0980	(68.159)
"SGMA":	49	1.76533		0.2163	(58.693)

1
For AQL= 0.02872 (at 95%) :

				Uniform-Robustness	
				pa	ROB
				----	----
"Ramp":	64	B= 0.50	T= 0.9049	0.4569	(24.158)
"Attr":	113	114 6	{for p50= 0.0590}		
" S ":	51	1.57144		0.6689	(13.775)
"SGMA":	23	1.56358		0.6296	(15.696)
"Ramp":	64	B= 0.70	T= 0.8883	0.3184	(34.043)
"Attr":	135	138 7	{for p50= 0.0566}		
" S ":	61	1.59038		0.6291	(17.297)
"SGMA":	27	1.58376		0.6001	(18.860)
"Ramp":	64	B= 0.90	T= 0.8696	0.2319	(42.069)
"Attr":	159	163 8	{for p50= 0.0363}		
" S ":	68	1.60982		0.5744	(22.004)
"SGMA":	30	1.60381		0.5626	(22.696)
"Ramp":	64	B= 1.10	T= 0.8479	0.1868	(48.016)
"Attr":	185	188 9	{for p50= 0.0522}		
" S ":	81	1.62862		0.5142	(27.420)
"SGMA":	35	1.62353		0.5213	(26.970)
"Ramp":	64	B= 1.30	T= 0.8234	0.1662	(52.607)
"Attr":	210	214 10	{for p50= 0.0506}		
" S ":	91	1.64382		0.4572	(33.075)
"SGMA":	39	1.63926		0.4833	(31.324)
"Ramp":	64	B= 1.50	T= 0.7990	0.1460	(60.277)
"Attr":	262	267 12	{for p50= 0.0493}		
" S ":	104	1.65613		0.4050	(40.858)
"SGMA":	44	1.65211		0.4484	(37.606)
"Ramp":	64	B= 1.70	T= 0.7663	0.1735	(58.215)
"Attr":	262	267 12	{for p50= 0.0483}		
" S ":	112	1.66490		0.3661	(43.778)
"SGMA":	47	1.66115		0.4223	(39.563)
"Ramp":	64	B= 1.90	T= 0.7348	0.1928	(56.773)
"Attr":	266	267 12	{for p50= 0.0479}		
" S ":	119	1.67285		0.3302	(46.472)
"SGMA":	50	1.66931		0.3975	(41.424)

1
For AQL= 0.03593 (at 95%) :

				Uniform-Robustness	
				Pa	ROE
"Ramp":	64	B= 0.50	T= 0.8889	0.5612	(12.712)
"Attr":	109	110 7	{for p50= 0.0702}		
" S ":	52	1.48175		0.8179	(6.357)
"SGMA":	25	1.47449		0.7471	(9.763)
"Ramp":	64	B= 0.70	T= 0.8709	0.4321	(27.095)
"Attr":	128	130 8	{for p50= 0.0673}		
" S ":	61	1.50215		0.7949	(8.115)
"SGMA":	29	1.49589		0.7262	(11.706)
"Ramp":	64	B= 0.90	T= 0.8501	0.3512	(33.246)
"Attr":	149	150 9	{for p50= 0.0648}		
" S ":	71	1.52127		0.7665	(10.313)
"SGMA":	33	1.51584		0.7009	(13.997)
"Ramp":	64	B= 1.10	T= 0.8264	0.3084	(38.494)
"Attr":	170	171 10	{for p50= 0.0627}		
" S ":	80	1.53751		0.7346	(12.924)
"SGMA":	37	1.53264		0.6758	(16.454)
"Ramp":	64	B= 1.30	T= 0.7996	0.2956	(41.806)
"Attr":	190	192 11	{for p50= 0.0611}		
" S ":	90	1.54998		0.7076	(15.409)
"SGMA":	41	1.54563		0.6542	(18.800)
"Ramp":	64	B= 1.50	T= 0.7704	0.3020	(43.391)
"Attr":	211	213 12	{for p50= 0.0598}		
" S ":	99	1.56056		0.6801	(18.076)
"SGMA":	45	1.55658		0.6339	(21.169)
"Ramp":	64	B= 1.70	T= 0.7392	0.3235	(44.064)
"Attr":	232	235 13	{for p50= 0.0587}		
" S ":	109	1.56928		0.6554	(20.722)
"SGMA":	49	1.56565		0.6154	(23.532)
"Ramp":	64	B= 1.90	T= 0.7064	0.3574	(43.592)
"Attr":	253	257 14	{for p50= 0.0579}		
" S ":	116	1.57621		0.6323	(23.370)
"SGMA":	52	1.57279		0.5991	(25.814)

For AQL= 0.04457 (at 95%) :

				Uniform-Robustness	
				Pa	ROE
"Ramp":	64	B= 0.50	T= 0.8715	0.6510	(14.060)
"Attr":	104	105 8	{for p50= 0.0827}		
" S ":	52	1.39411		0.9072	(2.013)
"SGMA":	27	1.38727		0.8387	(5.231)
"Ramp":	64	B= 0.70	T= 0.8515	0.5474	(20.319)
"Attr":	121	121 9	{for p50= 0.0797}		
" S ":	67	1.41317		0.8285	(6.130)
"SGMA":	31	1.40731			
"Ramp":	64	B= 0.90	T= 0.8286	0.4827	(26.695)
"Attr":	151	155 11	{for p50= 0.0770}		
" S ":	70	1.43080		0.8904	(3.404)
"SGMA":	35	1.42562		0.8158	(7.666)
"Ramp":	64	B= 1.10	T= 0.8025	0.4550	(29.787)
"Attr":	168	172 12	{for p50= 0.0750}		
" S ":	79	1.44425		0.8821	(4.084)
"SGMA":	39	1.43962		0.8057	(8.685)
"Ramp":	64	B= 1.30	T= 0.7739	0.4524	(31.388)
"Attr":	186	189 13	{for p50= 0.0733}		
" S ":	88	1.45577		0.8736	(4.822)
"SGMA":	43	1.45159		0.7958	(9.722)
"Ramp":	64	B= 1.50	T= 0.7430	0.4707	(31.643)
"Attr":	203	207 14	{for p50= 0.0719}		
" S ":	97	1.46523		0.8659	(5.551)
"SGMA":	47	1.46141		0.7873	(10.743)
"Ramp":	64	B= 1.70	T= 0.7104	0.5035	(29.473)
"Attr":	206	207 14	{for p50= 0.0709}		
" S ":	104	1.47293		0.8572	(6.124)
"SGMA":	50	1.46935		0.7781	(11.347)
"Ramp":	64	B= 1.90	T= 0.6765	0.5473	(27.715)
"Attr":	223	225 15	{for p50= 0.0700}		
" S ":	110	1.47903		0.8495	(6.915)
"SGMA":	53	1.47563		0.7712	(12.307)

For AQL= 0.05480 (at 95%) :

				Uniform-Robustness	
				Pa	ROE
"Ramp":	64	B= 0.50	T= 0.8520	0.7290	(10.731)
"Attr":	110	112 10	{for p50= 0.0968}		
" S ":	55	1.30605		0.9601	(-0.489)
"SGMA":	30	1.30000		0.9077	(2.054)
"Ramp":	64	B= 0.70	T= 0.8300	0.6538	(15.256)
"Attr":	124	126 11	{for p50= 0.0937}		
" S ":	63	1.32344		0.9588	(-0.451)
"SGMA":	34	1.31811		0.9044	(2.351)
"Ramp":	64	B= 0.90	T= 0.8046	0.6141	(18.236)
"Attr":	138	140 12	{for p50= 0.0912}		
" S ":	70	1.33793		0.9563	(-0.342)
"SGMA":	37	1.33308		0.8983	(2.805)
"Ramp":	64	B= 1.10	T= 0.7767	0.6003	(19.910)
"Attr":	153	154 13	{for p50= 0.0891}		
" S ":	80	1.35059		0.9567	(-0.383)
"SGMA":	42	1.34632		0.8979	(2.968)

"Ramp":	64	B= 1.30	T= 0.7463	0.6100 (20.223)
"Attr":	167	168 14	{for p50= 0.0874}	
" S ":	86	1.36096		0.9530 (-0.215)
"SGMA":	45	1.35695		0.8930 (3.368)
"Ramp":	64	B= 1.50	T= 0.7139	0.6368 (18.437)
"Attr":	182	183 15	{for p50= 0.0860}	
" S ":	94	1.36940		0.9531 (-0.191)
"SGMA":	49	1.36571		0.8917 (3.619)
"Ramp":	64	B= 1.70	T= 0.6800	0.6752 (17.096)
"Attr":	196	197 16	{for p50= 0.0850}	
" S ":	101	1.37597		0.9526 (-0.169)
"SGMA":	52	1.37253		0.8895 (3.899)
"Ramp":	64	B= 1.90	T= 0.6454	0.7176 (15.524)
"Attr":	210	212 17	{for p50= 0.0841}	
" S ":	105	1.38137		0.9503 (-0.023)
"SGMA":	54	1.37805		0.8862 (4.265)

1
 For AQL= 0.06681 (at 95%) :
 =====

				Uniform-Robustness	
				Pa	ROB
				-----	-----
"Ramp":	64	B= 0.50	T= 0.8305	0.7918	(7.365)
"Attr":	103	103 11	{for p50= 0.1131}		
" S ":	55	1.21592		0.9826	(-1.519)
"SGMA":	32	1.21029		0.9497	(0.912)
"Ramp":	64	B= 0.70	T= 0.8059	0.7471	(10.451)
"Attr":	124	126 13	{for p50= 0.1101}		
" S ":	63	1.23118		0.9838	(-1.739)
"SGMA":	36	1.22622		0.9502	(-0.008)
"Ramp":	64	B= 0.90	T= 0.7787	0.7253	(12.110)
"Attr":	136	138 14	{for p50= 0.1074}		
" S ":	70	1.24493		0.9838	(-1.821)
"SGMA":	40	1.24042		0.9501	(-0.004)
"Ramp":	64	B= 1.10	T= 0.7488	0.7265	(12.561)
"Attr":	148	150 15	{for p50= 0.1053}		
" S ":	76	1.25599		0.9835	(-1.884)
"SGMA":	43	1.25180		0.9486	(0.078)
"Ramp":	64	B= 1.30	T= 0.7168	0.7440	(12.029)
"Attr":	160	162 16	{for p50= 0.1036}		
" S ":	84	1.26537		0.9845	(-2.012)
"SGMA":	47	1.26156		0.9494	(0.036)
"Ramp":	64	B= 1.50	T= 0.6828	0.7750	(10.592)
"Attr":	172	174 17	{for p50= 0.1023}		
" S ":	90	1.27206		0.9849	(-2.114)
"SGMA":	50	1.26848		0.9496	(0.021)
"Ramp":	64	B= 1.70	T= 0.6480	0.8093	(8.803)

"Attr":	184	186 18	{for p50= 0.1012}	0.9854	(-2.216)
" S ":	96	1.27799		0.9500	(-0.002)
"SGMA":	53	1.27463			
"Ramp":	64	B= 1.90	T= 0.6129	0.8431	(6.692)
"Attr":	185	186 18	{for p50= 0.1004}		
" S ":	100	1.28270		0.9853	(-2.211)
"SGMA":	55	1.27946		0.9495	(0.931)

1
 For AQL= 0.08076 (at 95%) :
 =====

				Uniform-Robustness	
				Pa	ROB
				-----	-----
"Ramp":	64	B= 0.50	T= 0.8064	0.8435	(4.983)
"Attr":	103	104 13	{for p50= 0.1315}		
" S ":	55	1.12431		0.9925	(-1.989)
"SGMA":	34	1.11910		0.9740	(-1.122)
"Ramp":	64	B= 0.70	T= 0.7799	0.8183	(6.451)
"Attr":	114	114 14	{for p50= 0.1284}		
" S ":	62	1.13869		0.9932	(-2.118)
"SGMA":	38	1.13403		0.9751	(-1.230)
"Ramp":	64	B= 0.90	T= 0.7506	0.8127	(7.293)
"Attr":	132	134 16	{for p50= 0.1258}		
" S ":	69	1.15066		0.9939	(-2.331)
"SGMA":	42	1.14643		0.9763	(-1.395)
"Ramp":	64	B= 1.10	T= 0.7191	0.8218	(7.058)
"Attr":	142	144 17	{for p50= 0.1236}		
" S ":	75	1.16102		0.9942	(-2.432)
"SGMA":	45	1.15710		0.9762	(-1.440)
"Ramp":	64	B= 1.30	T= 0.6853	0.8438	(6.045)
"Attr":	152	154 18	{for p50= 0.1220}		
" S ":	80	1.16858		0.9944	(-2.529)
"SGMA":	48	1.16488		0.9768	(-1.524)
"Ramp":	64	B= 1.50	T= 0.6504	0.8699	(4.706)
"Attr":	162	164 19	{for p50= 0.1207}		
" S ":	86	1.17488		0.9950	(-2.641)
"SGMA":	51	1.17143		0.9776	(-1.619)
"Ramp":	64	B= 1.70	T= 0.6150	0.8959	(3.277)
"Attr":	172	174 20	{for p50= 0.1196}		
" S ":	91	1.18009		0.9953	(-2.741)
"SGMA":	54	1.17681		0.9785	(-1.727)
"Ramp":	64	B= 1.90	T= 0.5796	0.9191	(1.870)
"Attr":	173	174 20	{for p50= 0.1189}		
" S ":	95	1.18385		0.9956	(-2.757)
"SGMA":	56	1.18070		0.9789	(-1.752)

1
 For AQL= 0.09680 (at 95%) :

Uniform-Robustness
Pa RCB

"Ramp":	64	B= 0.50	T= 0.7802	0.8820 (2.336)
"Attr":	54	56 9	{for p50= 0.1785}	
" S ":	25	0.93067		0.9901 (-1.377)
"SGMA":	18	0.92097		0.9782 (-0.969)
"Ramp":	64	B= 0.70	T= 0.7517	0.8714 (2.700)
"Attr":	55	56 9	{for p50= 0.1746}	
" S ":	28	0.94486		0.9916 (-1.420)
"SGMA":	20	0.93611		0.9803 (-1.040)
"Ramp":	64	B= 0.90	T= 0.7204	0.8758 (2.702)
"Attr":	62	63 10	{for p50= 0.1715}	
" S ":	30	0.95662		0.9920 (-1.511)
"SGMA":	21	0.94838		0.9800 (-1.094)
"Ramp":	64	B= 1.10	T= 0.6872	0.8893 (2.211)
"Attr":	63	63 10	{for p50= 0.1689}	
" S ":	33	0.96619		0.9933 (-1.577)
"SGMA":	23	0.95864		0.9822 (-1.172)
"Ramp":	64	B= 1.30	T= 0.6524	0.9082 (1.615)
"Attr":	69	71 11	{for p50= 0.1668}	
" S ":	35	0.97413		0.9938 (-1.893)
"SGMA":	24	0.96696		0.9824 (-1.252)
"Ramp":	64	B= 1.50	T= 0.6167	0.9282 (0.844)
"Attr":	70	71 11	{for p50= 0.1652}	
" S ":	37	0.97998		0.9944 (-1.716)
"SGMA":	25	0.97318		0.9829 (-1.272)
"Ramp":	64	B= 1.70	T= 0.5809	0.9458 (0.162)
"Attr":	71	71 11	{for p50= 0.1640}	
" S ":	38	0.98462		0.9945 (-1.719)
"SGMA":	26	0.97797		0.9836 (-1.300)
"Ramp":	64	B= 1.90	T= 0.5456	0.9600 (-0.385)
"Attr":	71	71 11	{for p50= 0.1632}	
" S ":	38	0.98796		0.9941 (-1.706)
"SGMA":	26	0.98129		0.9829 (-1.273)

Appendix (C.4.)

Performance of the Sample Sizes under Equivalence of Different Schemes

Description of the tables :

The tables are composed of a number of sub-tables each representing a level of AQL shown at the right top corner . The B values are shown on the top of each set of parameters , while the values for the Ramp sample size are shown on the left of each sub-table .

For any B on this table there are three columns of sample size . The first column is for equivalent two-class plan , the second for the S-plan and the third one for G-plan .

Each row has a ramp n that is equivalent to each n in each subset of three. But it should be remembered that between the subsets the background O.C. curves are different . Also note that the "equivalence" values of n for the attribute case are chosen such that the O.C. at the 95% point is as close as possible to (ARL,95%) .

We should also note that the values of the 50% indifference point on the O.C. curve behind the "equivalences" in these tables have a proportion defective, p0(2), which is decreasing with B . In a way this is responsible for the higher sample sizes as B increases . This is due to the general rule that a smaller p0(2) implies more stringency of the O.C. discrimination and hence a larger sample size . These values of p0(2) are shown in parantheses beneath their relevant subset of sample sizes .

Behaviour of Sample Size in the Different "Equivalent" Schemes

AQL= 0.0107 (at 95 %) :																											
Ramp n	B = 0.5			B = 0.7			B = 0.9			B = 1.1			B = 1.3			B = 1.5			B = 1.7			B = 1.9					
8	0	0	0	0	0	0	33	8	4	33	8	4	33	8	4	33	11	5	33	11	5	76	14	6			
	(-)	(-)	(0.0868)	(0.0635)	(0.0594)	(0.0557)	(0.0526)	(0.0501)			
16	33	11	5	33	11	5	76	14	6	76	17	7	76	20	8	76	23	9	76	26	10	127	29	11			

	(0.0569)	(0.0528)	(0.0474)	(0.0433)	(0.0402)	(0.0379)	(0.0359)	(0.0343)
32	76 23 9 (0.0390)	76 26 10 (0.0368)	127 32 12 (0.0337)	127 36 14 (0.0312)	127 44 16 (0.0292)	183 51 18 (0.0277)	183 57 20 (0.0264)	243 64 22 (0.0254)
64	127 44 16 (0.0293)	183 51 18 (0.0275)	183 64 22 (0.0255)	243 77 26 (0.0239)	306 90 30 (0.0223)	371 103 34 (0.0217)	371 113 37 (0.0211)	437 133 43 (0.0202)
128	306 90 30 (0.0228)	306 100 35 (0.0219)	437 127 41 (0.0204)	505 153 49 (0.0194)	575 184 58 (0.0186)	716 215 67 (0.0179)	789 239 74 (0.0174)	935 273 84 (0.0170)
256	575 170 54 (0.0189)	645 197 62 (0.0182)	789 245 76 (0.0173)	1009 311 95 (0.0165)	1235 375 112 (0.0159)	1465 432 130 (0.0156)	1698 495 148 (0.0152)	1855 554 165 (0.0149)

AQL= 0.0139 (at 95%) :

Ramp n	B = 0.5	B = 0.7	B = 0.9	B = 1.1	B = 1.3	B = 1.5	B = 1.7	B = 1.9
8	0 0 0 (-)	25 7 4 (0.0813)	25 8 4 (0.0784)	25 8 4 (0.0740)	25 10 5 (0.0695)	58 10 5 (0.0657)	58 13 6 (0.0626)	58 13 6 (0.0601)
16	25 10 5 (0.0668)	58 13 6 (0.0606)	58 16 7 (0.0542)	58 18 8 (0.0512)	58 21 9 (0.0482)	58 24 10 (0.0456)	98 27 11 (0.0435)	98 30 12 (0.0418)
32	58 21 9 (0.0475)	98 27 11 (0.0433)	98 33 13 (0.0401)	98 39 15 (0.0375)	141 44 17 (0.0356)	141 51 19 (0.0338)	187 57 21 (0.0325)	187 63 23 (0.0314)
64	141 41 16 (0.0359)	141 54 20 (0.0330)	187 63 24 (0.0309)	236 78 28 (0.0292)	286 90 32 (0.0280)	286 106 37 (0.0268)	337 118 41 (0.0259)	390 131 45 (0.0252)
128	236 84 30 (0.0287)	337 109 38 (0.0266)	390 134 46 (0.0251)	497 159 54 (0.0240)	553 182 61 (0.0232)	608 210 70 (0.0225)	721 242 80 (0.0219)	779 268 88 (0.0214)
256	497 172 58 (0.0236)	608 201 67 (0.0228)	779 265 87 (0.0215)	953 323 105 (0.0207)	1150 372 120 (0.0202)	1310 434 139 (0.0197)	1492 495 157 (0.0193)	1675 545 173 (0.0190)

AQL= 0.0179 (at 95%) :

Ramp n	B = 0.5	B = 0.7	B = 0.9	B = 1.1	B = 1.3	B = 1.5	B = 1.7	B = 1.9
8	0 0 0 (-)	19 7 4 (0.0943)	19 7 4 (0.0906)	19 9 5 (0.0856)	45 9 5 (0.0811)	45 10 5 (0.0775)	45 12 6 (0.0744)	45 12 6 (0.0718)
16	45 10 5 (0.0777)	45 14 7 (0.0692)	45 15 7 (0.0645)	45 17 8 (0.0606)	76 20 9 (0.0575)	76 23 10 (0.0548)	76 25 11 (0.0524)	76 28 12 (0.0507)
32	76 22 10 (0.0554)	76 28 12 (0.0509)	110 33 14 (0.0476)	110 39 16 (0.0452)	110 44 18 (0.0430)	146 50 20 (0.0411)	146 56 22 (0.0397)	185 61 24 (0.0386)
64	146 47 19 (0.0422)	146 56 22 (0.0395)	222 76 29 (0.0360)	222 78 30 (0.0359)	262 90 35 (0.0342)	262 105 39 (0.0330)	303 116 43 (0.0321)	345 128 47 (0.0313)
128	262 93 35 (0.0341)	303 114 42 (0.0322)	387 140 51 (0.0308)	430 161 58 (0.0298)	517 188 67 (0.0287)	581 215 76 (0.0280)	651 239 84 (0.0274)	696 266 93 (0.0268)
256	517 187 67 (0.0287)	606 230 81 (0.0276)	741 281 98 (0.0266)	879 327 113 (0.0259)	1019 382 131 (0.0252)	1208 437 149 (0.0247)	1351 489 166 (0.0243)	1496 541 183 (0.0239)

AQL= 0.0228 (at 95%) :

Ramp n	B = 0.5	B = 0.7	B = 0.9	B = 1.1	B = 1.3	B = 1.5	B = 1.7	B = 1.9
8	0 0 0 (-)	15 7 4 (0.1087)	35 7 4 (0.1035)	35 9 5 (0.0986)	35 9 5 (0.0950)	35 11 6 (0.0912)	35 11 6 (0.0879)	35 11 6 (0.0854)
16	35 11 6 (0.0878)	35 14 7 (0.0808)	35 16 8 (0.0757)	60 18 9 (0.0713)	60 21 10 (0.0680)	60 23 11 (0.0652)	60 26 12 (0.0629)	60 28 13 (0.0612)
32	60 23 11 (0.0642)	86 29 13 (0.0599)	86 34 15 (0.0568)	86 39 17 (0.0540)	114 44 19 (0.0517)	114 49 21 (0.0493)	144 55 23 (0.0483)	144 60 25 (0.0472)
64	114 49 21 (0.0499)	144 60 25 (0.0471)	406 170 65 (0.0361)	206 78 32 (0.0433)	238 92 37 (0.0417)	271 103 41 (0.0405)	271 114 45 (0.0395)	304 125 49 (0.0387)
128	238 98 39 (0.0410)	304 120 47 (0.0390)	337 139 54 (0.0377)	406 161 62 (0.0365)	476 187 71 (0.0355)	511 212 80 (0.0346)	582 237 89 (0.0339)	618 257 96 (0.0334)
256	476 195 74 (0.0352)	582 243 91 (0.0338)	690 282 105 (0.0329)	800 331 122 (0.0321)	949 388 142 (0.0313)	1061 434 158 (0.0308)	1212 486 176 (0.0303)	1289 523 189 (0.0300)

AQL= 0.0287 (at 95%) :

Ramp n	B = 0.5	B = 0.7	B = 0.9	B = 1.1	B = 1.3	B = 1.5	B = 1.7	B = 1.9
8	28 6 4 (0.1266)	28 6 4 (0.1224)	28 8 5 (0.1181)	28 8 5 (0.1151)	28 8 5 (0.1102)	28 10 6 (0.1069)	28 10 6 (0.1035)	28 10 6 (0.1009)
16	28 10 6 (0.1008)	28 13 7 (0.0939)	47 17 9 (0.0879)	47 17 9 (0.0839)	47 20 10 (0.0804)	47 22 11 (0.0775)	68 24 12 (0.0752)	68 26 13 (0.0734)
32	68 24 12 (0.0747)	68 29 14 (0.0708)	90 34 16 (0.0673)	90 39 18 (0.0643)	114 45 20 (0.0619)	114 48 22 (0.0601)	144 53 24 (0.0585)	144 56 25 (0.0572)
64	114 49 21 (0.0590)	138 61 27 (0.0566)	163 68 30 (0.0563)	188 81 35 (0.0522)	214 91 39 (0.0506)	267 104 44 (0.0493)	267 112 47 (0.0483)	304 125 49 (0.0475)
128	241 104 44 (0.0491)	267 122 51 (0.0474)	321 143 59 (0.0459)	377 164 67 (0.0446)	433 187 76 (0.0434)	489 208 84 (0.0426)	518 229 92 (0.0419)	576 250 100 (0.0413)
256	461 208 84 (0.0427)	547 243 97 (0.0415)	663 290 115 (0.0403)	781 336 132 (0.0394)	870 384 152 (0.0387)	990 427 166 (0.0381)	1081 470 182 (0.0377)	1173 510 197 (0.0373)

AQL= 0.0359 (at 95%) :

Ramp n	B = 0.5	B = 0.7	B = 0.9	B = 1.1	B = 1.3	B = 1.5	B = 1.7	B = 1.9
8	22 4 3 (0.1643)	22 6 4 (0.1601)	22 5 4 (0.1616)	22 8 5 (0.1332)	22 10 6 (0.1288)	22 9 6 (0.1246)	22 10 6 (0.1212)	22 12 7 (0.1188)
16	38 11 7 (0.1166)	38 14 8 (0.1072)	38 16 9 (0.1023)	38 18 10 (0.0981)	54 20 11 (0.0946)	54 22 12 (0.0917)	54 25 13 (0.0894)	54 24 13 (0.0876)
32	54 24 13 (0.0873)	72 29 15 (0.0830)	72 34 17 (0.0794)	91 38 19 (0.0763)	91 43 21 (0.0739)	110 47 23 (0.0720)	110 52 25 (0.0704)	110 54 26 (0.0692)
64	110 52 25 (0.0702)	130 61 29 (0.0673)	150 71 33 (0.0648)	171 80 37 (0.0627)	192 90 41 (0.0611)	213 99 45 (0.0598)	235 109 49 (0.0587)	257 116 52 (0.0579)
128	235 104 47 (0.0591)	257 123 55 (0.0571)	301 143 63 (0.0555)	346 165 72 (0.0540)	391 184 80 (0.0524)	437 206 89 (0.0520)	483 224 96 (0.0513)	507 241 103 (0.0507)
256	460 211 91 (0.0517)	530 251 107 (0.0504)	624 296 125 (0.0492)	719 338 142 (0.0482)	816 380 159 (0.0475)	888 418 174 (0.0469)	986 458 190 (0.0464)	1059 491 203 (0.0460)

AQL= 0.0446 (at 95%) :

Ramp n	B = 0.5	B = 0.7	B = 0.9	B = 1.1	B = 1.3	B = 1.5	B = 1.7	B = 1.9
8	18 5 4 (0.1809)	18 5 4 (0.1779)	18 4 3 (0.1919)	18 5 4 (0.1798)	18 5 4 (0.1737)	18 5 4 (0.1686)	18 7 5 (0.1652)	18 7 5 (0.1625)
16	30 13 8 (0.1292)	30 15 9 (0.1234)	44 17 10 (0.1186)	44 17 10 (0.1144)	44 19 11 (0.1108)	44 21 12 (0.1079)	44 23 13 (0.1057)	44 23 13 (0.1039)
32	58 25 14 (0.1014)	58 29 16 (0.0968)	73 33 18 (0.0932)	89 36 20 (0.0902)	89 42 22 (0.0878)	105 46 24 (0.0858)	105 48 25 (0.0842)	105 53 27 (0.0830)
64	105 52 27 (0.0827)	121 61 31 (0.0797)	155 70 35 (0.0770)	172 79 39 (0.0750)	189 88 43 (0.0733)	207 97 47 (0.0719)	207 104 50 (0.0709)	225 110 53 (0.0700)
128	225 108 52 (0.0704)	261 126 60 (0.0684)	297 142 67 (0.0668)	334 163 76 (0.0652)	371 183 85 (0.0640)	408 202 93 (0.0631)	446 218 100 (0.0623)	465 232 106 (0.0617)
256	446 217 100 (0.0623)	522 257 117 (0.0608)	599 299 135 (0.0596)	677 336 151 (0.0586)	755 373 167 (0.0579)	834 411 183 (0.0572)	894 446 198 (0.0567)	953 472 209 (0.0563)

AQL= 0.0548 (at 95%) :

Ramp n	B = 0.5	B = 0.7	B = 0.9	B = 1.1	B = 1.3	B = 1.5	B = 1.7	B = 1.9
8	14 5 4 (0.1952)	14 5 4 (0.2118)	14 5 4 (0.2114)	14 5 4 (0.2039)	14 5 4 (0.1972)	14 7 5 (0.1935)	14 6 5 (0.1900)	14 6 5 (0.1875)
16	24 8 6 (0.1695)	24 8 6 (0.1657)	24 10 7 (0.1605)	35 12 11 (0.1528)	47 15 12 (0.1292)	47 19 12 (0.1264)	47 21 13 (0.1242)	47 23 14 (0.1225)

32	59 25 15	59 29 17	72 33 19	72 37 21	85 41 23	85 45 25	98 47 26	98 49 27
	(0.1174)	(0.1128)	(0.1051)	(0.1081)	(0.1035)	(0.1016)	(0.1000)	(0.0988)
64	112 55 30	126 63 34	140 70 37	154 80 42	168 88 45	183 94 49	197 101 52	212 105 54
	(0.0968)	(0.0937)	(0.0891)	(0.0891)	(0.0874)	(0.0860)	(0.0850)	(0.0841)
128	212 109 56	256 128 65	286 143 72	317 162 81	347 179 89	378 196 97	409 209 103	425 220 108
	(0.0835)	(0.0813)	(0.0797)	(0.0781)	(0.0769)	(0.0759)	(0.0752)	(0.0746)
256	440 224 110	503 263 128	566 296 143	646 333 160	711 368 176	775 400 191	824 424 202	873 451 214
	(0.0745)	(0.0729)	(0.0713)	(0.0705)	(0.0699)	(0.0693)	(0.0688)	(0.0684)

AQL= 0.0668 (at 95 %) :

Ramp n	B = 0.5	B = 0.7	B = 0.9	B = 1.1	B = 1.3	B = 1.5	B = 1.7	B = 1.9
8	20 6 5	12 4 4	12 5 4	12 5 4	12 5 4	12 6 5	20 6 5	20 6 5
	(0.2119)	(0.2448)	(0.2375)	(0.2293)	(0.2251)	(0.2207)	(0.2175)	(0.2153)
16	20 8 6	20 9 7	20 9 7	29 9 7	29 11 8	29 11 8	29 13 9	29 13 9
	(0.1925)	(0.1888)	(0.1849)	(0.1794)	(0.1752)	(0.1718)	(0.1694)	(0.1675)
32	49 25 16	59 29 18	70 33 20	70 36 22	81 41 24	81 42 25	92 46 27	92 48 28
	(0.1357)	(0.1309)	(0.1272)	(0.1241)	(0.1217)	(0.1196)	(0.1182)	(0.1171)
64	103 55 32	126 63 36	138 70 40	150 78 43	162 84 47	174 90 50	186 96 53	186 100 55
	(0.1131)	(0.1101)	(0.1074)	(0.1053)	(0.1036)	(0.1023)	(0.1012)	(0.1004)
128	210 111 61	235 123 67	272 143 77	297 159 85	323 175 93	348 187 99	374 199 105	387 209 110
	(0.0985)	(0.0968)	(0.0946)	(0.0930)	(0.0919)	(0.0909)	(0.0901)	(0.0896)
256	425 229 120	491 261 136	543 294 152	609 328 169	662 355 182	716 383 196	756 408 208	796 428 218
	(0.0885)	(0.0871)	(0.0859)	(0.0848)	(0.0840)	(0.0834)	(0.0829)	(0.0825)

AQL= 0.0808 (at 95 %) :

Ramp n	B = 0.5	B = 0.7	B = 0.9	B = 1.1	B = 1.3	B = 1.5	B = 1.7	B = 1.9
8	10 3 3	10 4 4	16 4 4	16 4 4	16 4 4	16 6 5	16 6 5	16 6 5
	(0.2825)	(0.2743)	(0.2611)	(0.2601)	(0.2543)	(0.2505)	(0.2476)	(0.2457)
16	16 7 6	24 9 7	24 9 7	24 10 8	24 10 8	24 10 8	24 12 9	24 12 9
	(0.2197)	(0.2134)	(0.2094)	(0.2045)	(0.2004)	(0.1975)	(0.1951)	(0.1934)
32	32 15 11	32 17 12	40 18 13	40 18 13	40 20 14	49 22 15	49 22 15	49 24 16
	(0.1826)	(0.1769)	(0.1725)	(0.1687)	(0.1660)	(0.1638)	(0.1621)	(0.1608)
64	104 55 34	114 62 38	134 69 42	144 75 43	154 80 48	164 86 51	174 91 54	174 95 56
	(0.1315)	(0.1284)	(0.1258)	(0.1236)	(0.1220)	(0.1207)	(0.1196)	(0.1189)
128	204 111 65	235 126 73	267 141 81	292 156 89	309 168 96	330 180 102	352 189 107	363 197 111
	(0.1157)	(0.1134)	(0.1116)	(0.1100)	(0.1089)	(0.1080)	(0.1072)	(0.1067)
256	417 228 128	471 259 144	526 289 160	581 319 176	625 344 189	670 366 201	703 387 212	737 404 221
	(0.1047)	(0.1032)	(0.1020)	(0.1010)	(0.1002)	(0.0995)	(0.0990)	(0.0986)

AQL= 0.0968 (at 95 %) :

Ramp n	B = 0.5	B = 0.7	B = 0.9	B = 1.1	B = 1.3	B = 1.5	B = 1.7	B = 1.9
8	0 0 0	14 4 4	14 4 4	14 4 4	14 5 5	14 5 5	14 5 5	14 5 5
	(0.0000)	(0.2934)	(0.2994)	(0.2909)	(0.2862)	(0.2827)	(0.2803)	(0.2786)
16	20 8 7	20 8 7	20 8 7	20 10 8	26 10 8	26 11 9	26 11 9	26 11 9
	(0.2452)	(0.2420)	(0.2370)	(0.2322)	(0.2284)	(0.2255)	(0.2233)	(0.2218)
32	33 14 11	33 16 12	33 17 13	41 19 14	41 19 14	41 20 15	41 20 15	41 22 16
	(0.2069)	(0.2017)	(0.1973)	(0.1938)	(0.1911)	(0.1890)	(0.1873)	(0.1861)
64	56 25 18	56 28 20	63 30 21	63 33 23	71 35 24	71 37 25	71 38 26	71 38 26
	(0.1785)	(0.1746)	(0.1715)	(0.1689)	(0.1668)	(0.1652)	(0.1640)	(0.1632)
128	205 110 69	231 126 78	249 138 85	276 150 92	293 161 98	311 171 104	329 178 108	338 185 112
	(0.1350)	(0.1327)	(0.1310)	(0.1295)	(0.1283)	(0.1273)	(0.1266)	(0.1261)
256	420 229 137	466 257 153	512 283 168	559 308 182	596 331 195	633 350 206	671 370 217	689 381 223
	(0.1231)	(0.1215)	(0.1203)	(0.1193)	(0.1185)	(0.1179)	(0.1173)	(0.1170)

AQL= 0.1151 (at 95 %) :

Ramp n	B = 0.5	B = 0.7	B = 0.9	B = 1.1	B = 1.3	B = 1.5	B = 1.7	B = 1.9
8	11 4 4	11 4 4	11 4 4	11 4 4	11 5 5	11 5 5	11 5 5	11 5 5
	(0.3219)	(0.3464)	(0.3502)	(0.3243)	(0.3207)	(0.3175)	(0.3155)	(0.3141)
16	17 8 7	22 8 7	22 9 8	22 9 8	22 9 8	22 11 9	22 10 9	22 10 9
	(0.2757)	(0.2726)	(0.2665)	(0.2621)	(0.2586)	(0.2561)	(0.2542)	(0.2528)
32	34 15 12	34 15 12	34 16 13	40 18 14	40 18 14	40 19 15	40 19 15	40 21 16
	(0.2336)	(0.2285)	(0.2243)	(0.2211)	(0.2186)	(0.2165)	(0.2151)	(0.2141)
64	53 25 19	53 28 21	60 30 22	60 31 23	66 32 24	66 34 25	66 36 26	73 36 26
	(0.2034)	(0.1997)	(0.1966)	(0.1942)	(0.1923)	(0.1908)	(0.1897)	(0.1889)
128	80 42 30	87 45 32	94 48 34	101 51 36	101 54 38	108 56 39	108 57 40	115 59 41
	(0.1839)	(0.1809)	(0.1786)	(0.1765)	(0.1751)	(0.1739)	(0.1730)	(0.1723)
256	129 68 47	136 73 50	143 76 53	151 81 55	158 84 57	165 87 59	165 89 61	172 91 61
	(0.1683)	(0.1665)	(0.1650)	(0.1637)	(0.1627)	(0.1620)	(0.1614)	(0.1609)

n.b. :

- (1) The values in the brackets show $P_0(2)$, the proportion defective for the 50 % indifference point of the equivalence O-C curve.
- (2) Some of these results are reflected graphically in Chapter (IV).

Appendix (F.1.)

Robustness Results for Lognormal and Contaminated Normal processes

The Performance of the Schemes under Lognormal and Contaminated Normal Processes is given below in terms of the Probability of Acceptance for the equivalent sets of plans :

for AQL= 0.01390 (at 95%) :

=====

	Lognormal	Contaminated-Normal Robustness											
		D = 1				D > 1							
		Y= 0.0	0.02	0.06	0.10	0.02		0.06		0.10			
				D=1.2	D=2.0	D=1.2	D=2.0	D=1.2	D=2.0				
"Ramp":	8	B= 0.50	T= *	*	*								
	(" Non-Existent ")										
"Ramp":	8	B= 0.90	T= 0.8393	0.68	0.90	0.97	-	-	0.97	0.97	-	-	-
"Attr":	21	25	1 {for p50= 0.0784}	0.96	0.96	0.96	-	-	0.95	0.95	-	-	-
" S ":	8	1.46813		0.50	0.97	0.99	-	-	0.99	0.99	-	-	-
"SGMA":	4	1.41569		0.51	0.94	0.97	-	-	0.97	0.96	-	-	-
"Ramp":	8	B= 1.30	T= 0.7899	0.53	0.95	0.98	-	-	0.98	0.98	-	-	-
"Attr":	24	25	1 {for p50= 0.0695}	0.96	0.96	0.95	-	-	0.95	0.95	-	-	-
" S ":	10	1.52166		0.44	0.97	0.99	-	-	1.00	0.99	-	-	-
"SGMA":	5	1.47939		0.47	0.93	0.98	-	-	0.98	0.97	-	-	-
"Ramp":	8	B= 1.70	T= 0.7357	0.41	0.94	0.98	-	-	0.98	0.98	-	-	-
"Attr":	42	58	2 {for p50= 0.0626}	0.95	0.95	0.96	-	-	0.95	0.95	-	-	-
" S ":	13	1.56584		0.39	0.97	0.99	-	-	0.99	0.99	-	-	-
"SGMA":	6	1.53322		0.44	0.94	0.98	-	-	0.98	0.97	-	-	-

For AQL= 0.02872 (at 95%) :

=====

	Lognormal	Contaminated-Normal				Robustness									
		D = 1				D > 1									
		Y= 0.0	0.02	0.06	0.10	0.02		0.06		0.10					
					D=1.2	D=2.0	D=1.2	D=2.0	D=1.2	D=2.0					
"Ramp":	8	B= 0.50	T= 0.8290	0.81	0.93	0.94	-	-	0.94	0.94	-	-	-	-	
"Attr":	21	28	2	{for p50= 0.1266}	0.96	0.96	0.96	-	-	0.96	0.96	-	-	-	-
" S ":	6	1.20261			0.61	0.95	0.95	-	-	0.95	0.94	-	-	-	-
"SGMA":	4	1.14248			0.63	0.93	0.94	-	-	0.94	0.93	-	-	-	-
"Ramp":	8	B= 0.90	T= 0.7693	0.72	0.94	0.95	-	-	0.95	0.95	-	-	-	-	
"Attr":	22	28	2	{for p50= 0.1181}	0.96	0.96	0.95	-	-	0.95	0.95	-	-	-	-
" S ":	8	1.22864			0.60	0.96	0.98	-	-	0.97	0.96	-	-	-	-
"SGMA":	5	1.18476			0.61	0.94	0.95	-	-	0.95	0.94	-	-	-	-
"Ramp":	8	B= 1.30	T= 0.7104	0.59	0.94	0.95	-	-	0.95	0.95	-	-	-	-	
"Attr":	24	28	2	{for p50= 0.1108}	0.96	0.96	0.96	-	-	0.96	0.96	-	-	-	-
" S ":	8	1.26756			0.56	0.95	0.96	-	-	0.96	0.95	-	-	-	-
"SGMA":	5	1.22229			0.58	0.93	0.95	-	-	0.94	0.94	-	-	-	-
"Ramp":	8	B= 1.70	T= 0.6475	0.50	0.94	0.96	-	-	0.96	0.95	-	-	-	-	
"Attr":	25	28	2	{for p50= 0.1035}	0.96	0.96	0.96	-	-	0.96	0.96	-	-	-	-
" S ":	10	1.29779			0.53	0.96	0.97	-	-	0.97	0.96	-	-	-	-
"SGMA":	6	1.26174			0.55	0.93	0.95	-	-	0.94	0.93	-	-	-	-

For AQL= 0.05480 (at 95%) :

=====

	Lognormal	Contaminated-Normal				Robustness								
		D = 1				D > 1								
		Y= 0.0	0.02	0.06	0.10	0.02		0.06		0.10				
					D=1.2	D=2.0	D=1.2	D=2.0	D=1.2	D=2.0				
"Ramp":	8	B= 0.50	T= 0.7556	0.81	0.93	0.90	0.91	0.91	0.90	0.90	0.91	0.91	0.91	0.91
"Attr":	13	14	2	{for p50= 0.1952}	0.97	0.97	0.97	0.97	0.96	0.97	0.97	0.97	0.96	0.96
" S ":	5	0.91612			0.69	0.92	0.92	0.94	0.96	0.92	0.91	0.93	0.90	0.96
"SGMA":	4	0.85887			0.72	0.92	0.92	0.93	0.95	0.92	0.91	0.92	0.90	0.95
"Ramp":	8	B= 0.90	T= 0.6765	0.76	0.94	0.95	0.95	0.97	0.95	0.95	0.95	0.95	0.97	0.97
"Attr":	12	14	2	{for p50= 0.2114}	0.97	0.97	0.96	0.97	0.96	0.96	0.96	0.97	0.97	0.96
" S ":	5	0.85515			0.75	0.94	0.94	0.95	0.97	0.94	0.93	0.94	0.92	0.97
"SGMA":	4	0.80170			0.77	0.93	0.94	0.94	0.96	0.94	0.93	0.94	0.92	0.95
"Ramp":	8	B= 1.30	T= 0.6146	0.67	0.94	0.95	0.96	0.98	0.95	0.95	0.96	0.96	0.98	0.98
"Attr":	13	14	2	{for p50= 0.1972}	0.97	0.97	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
" S ":	5	0.90843			0.75	0.94	0.94	0.95	0.97	0.94	0.93	0.94	0.92	0.97
"SGMA":	4	0.85166			0.77	0.93	0.94	0.94	0.96	0.94	0.93	0.94	0.92	0.95
"Ramp":	8	B= 1.70	T= 0.5468	0.61	0.94	0.95	0.96	0.98	0.94	0.94	0.96	0.96	0.98	0.98
"Attr":	14	14	2	{for p50= 0.1900}	0.97	0.97	0.96	0.96	0.95	0.96	0.96	0.96	0.96	0.95
" S ":	6	0.92404			0.72	0.93	0.94	0.94	0.97	0.94	0.93	0.95	0.92	0.97
"SGMA":	5	0.87784			0.73	0.93	0.94	0.93	0.97	0.94	0.93	0.95	0.93	0.97

For AQL= 0.09680 (at 95%) :

=====

		Lognormal		Contaminated-Normal				Robustness					
				D = 1				D > 1					
				Y= 0.0	0.02	0.06	0.10	0.02		0.06		0.10	
								D=1.2	D=2.0	D=1.2	D=2.0	D=1.2	D=2.0
"Ramp":	8	B= 0.50	T= *	*	*								
	(" Non-Existent ")										
"Ramp":	8	B= 0.90	T= 0.5740	0.81	0.95	0.94	0.94	0.94	0.94	0.94	0.93	0.95	0.94
"Attr":	12	14	3 (for p50= 0.2994)	0.96	0.96	0.96	0.97	0.97	0.96	0.96	0.97	0.97	0.97
" S ":	4	0.57381		0.81	0.92	0.91	0.91	0.91	0.91	0.90	0.87	0.91	0.87
"SGMA":	4	0.52599		0.85	0.93	0.93	0.92	0.93	0.93	0.92	0.90	0.92	0.89
"Ramp":	8	B= 1.30	T= 0.5055	0.75	0.94	0.94	0.94	0.95	0.94	0.94	0.94	0.95	0.94
"Attr":	12	14	3 (for p50= 0.2862)	0.96	0.96	0.96	0.96	0.97	0.96	0.96	0.96	0.97	0.97
" S ":	5	0.60232		0.83	0.93	0.93	0.93	0.93	0.93	0.92	0.93	0.90	0.92
"SGMA":	5	0.56468		0.86	0.94	0.94	0.94	0.94	0.94	0.93	0.94	0.92	0.91
"Ramp":	8	B= 1.70	T= 0.4386	0.73	0.95	0.95	0.95	0.96	0.95	0.95	0.95	0.94	0.96
"Attr":	13	14	3 (for p50= 0.2803)	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
" S ":	5	0.62071		0.82	0.93	0.93	0.93	0.93	0.93	0.93	0.92	0.89	0.93
"SGMA":	5	0.58192		0.85	0.94	0.94	0.94	0.94	0.94	0.93	0.93	0.91	0.90

For AQL= 0.01390 (at 95%) :

=====

		Lognormal		Contaminated-Normal				Robustness					
				D = 1				D > 1					
				Y= 0.0	0.02	0.06	0.10	0.02		0.06		0.10	
								D=1.2	D=2.0	D=1.2	D=2.0	D=1.2	D=2.0
"Ramp":	16	B= 0.50	T= 0.9090	0.75	0.93	0.95	-	-	0.95	0.95	-	-	-
"Attr":	25	25	1 (for p50= 0.0668)	0.96	0.95	0.95	-	-	0.95	0.95	-	-	-
" S ":	10	1.54286		0.42	0.99	0.99	-	-	0.99	0.99	-	-	-
"SGMA":	5	1.50000		0.45	0.97	0.97	-	-	0.97	0.96	-	-	-
"Ramp":	16	B= 0.90	T= 0.8742	0.53	0.94	0.97	-	-	0.98	0.98	-	-	-
"Attr":	48	58	2 (for p50= 0.0548)	0.95	0.95	0.95	-	-	0.95	0.95	-	-	-
" S ":	16	1.62712		0.30	0.98	0.99	-	-	1.00	0.99	-	-	-
"SGMA":	7	1.60000		0.37	0.94	0.98	-	-	0.98	0.97	-	-	-
"Ramp":	16	B= 1.30	T= 0.8332	0.30	0.94	0.99	-	-	0.99	0.99	-	-	-
"Attr":	55	58	2 (for p50= 0.0482)	0.95	0.95	0.94	-	-	0.94	0.94	-	-	-
" S ":	21	1.68391		0.20	0.98	1.00	-	-	1.00	1.00	-	-	-
"SGMA":	9	1.66286		0.30	0.94	0.99	-	-	0.99	0.98	-	-	-
"Ramp":	16	B= 1.70	T= 0.7832	0.15	0.94	0.99	-	-	0.99	0.99	-	-	-
"Attr":	84	98	3 (for p50= 0.0435)	0.96	0.96	0.94	-	-	0.94	0.94	-	-	-
" S ":	27	1.72841		0.12	0.98	1.00	-	-	1.00	1.00	-	-	-
"SGMA":	11	1.71179		0.23	0.94	0.99	-	-	1.00	0.99	-	-	-

For AQL= 0.02872 (at 95%) :

=====

				Lognormal	Contaminated-Normal				Robustness					
					D = 1				D > 1					
					$\gamma = 0.0$	0.02	0.06	0.10	0.02		0.06		0.10	
									D=1.2	D=2.0	D=1.2	D=2.0	D=1.2	D=2.0
"Ramp":	16	B= 0.50	T= 0.8610	0.78	0.95	0.95	-	-	0.95	0.95	-	-	-	-
"Attr":	26	28 2	{for p50= 0.1008}	0.96	0.96	0.96	-	-	0.96	0.96	-	-	-	-
" S ":	10	1.31356		0.51	0.96	0.97	-	-	0.97	0.95	-	-	-	-
"SGMA":	6	1.27708		0.53	0.93	0.94	-	-	0.93	0.92	-	-	-	-
"Ramp":	16	B= 0.90	T= 0.8147	0.57	0.94	0.96	-	-	0.96	0.96	-	-	-	-
"Attr":	41	47 3	{for p50= 0.0879}	0.96	0.96	0.96	-	-	0.96	0.96	-	-	-	-
" S ":	17	1.37514		0.43	0.97	0.99	-	-	0.99	0.98	-	-	-	-
"SGMA":	9	1.35365		0.46	0.94	0.95	-	-	0.95	0.94	-	-	-	-
"Ramp":	16	B= 1.30	T= 0.7632	0.37	0.94	0.96	-	-	0.96	0.96	-	-	-	-
"Attr":	45	47 3	{for p50= 0.0804}	0.96	0.96	0.96	-	-	0.96	0.96	-	-	-	-
" S ":	20	1.42114		0.35	0.97	0.98	-	-	0.98	0.97	-	-	-	-
"SGMA":	10	1.40244		0.40	0.93	0.94	-	-	0.94	0.92	-	-	-	-
"Ramp":	16	B= 1.70	T= 0.7029	0.24	0.94	0.96	-	-	0.96	0.96	-	-	-	-
"Attr":	62	68 4	{for p50= 0.0752}	0.95	0.95	0.96	-	-	0.96	0.96	-	-	-	-
" S ":	24	1.45382		0.29	0.97	0.98	-	-	0.98	0.97	-	-	-	-
"SGMA":	12	1.43802		0.36	0.95	0.95	-	-	0.94	0.93	-	-	-	-

For AQL= 0.05480 (at 95%) :

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				Lognormal	Contaminated-Normal				Robustness					
					D = 1				D > 1					
					$\gamma = 0.0$	0.02	0.06	0.10	0.02		0.06		0.10	
									D=1.2	D=2.0	D=1.2	D=2.0	D=1.2	D=2.0
"Ramp":	16	B= 0.50	T= 0.7927	0.79	0.93	0.93	0.95	0.96	0.93	0.93	0.95	0.95	0.97	0.97
"Attr":	21	24 3	{for p50= 0.1695}	0.97	0.97	0.97	0.96	0.96	0.97	0.97	0.96	0.96	0.96	0.96
" S ":	8	0.99146		0.69	0.94	0.94	0.95	0.98	0.94	0.93	0.95	0.92	0.97	0.95
"SGMA":	6	0.95605		0.68	0.92	0.93	0.94	0.97	0.92	0.91	0.93	0.91	0.96	0.94
"Ramp":	16	B= 0.90	T= 0.7373	0.61	0.93	0.94	0.95	0.97	0.94	0.94	0.95	0.95	0.98	0.98
"Attr":	22	24 3	{for p50= 0.1605}	0.97	0.97	0.96	0.97	0.96	0.96	0.96	0.97	0.97	0.96	0.96
" S ":	10	1.02096		0.67	0.95	0.96	0.96	0.98	0.95	0.95	0.95	0.93	0.98	0.95
"SGMA":	7	0.99260		0.66	0.92	0.93	0.94	0.97	0.93	0.92	0.94	0.91	0.97	0.94
"Ramp":	16	B= 1.30	T= 0.6758	0.47	0.94	0.95	0.96	0.97	0.95	0.94	0.97	0.96	0.97	0.97
"Attr":	43	47 5	{for p50= 0.1292}	0.96	0.96	0.96	0.96	0.97	0.96	0.96	0.96	0.96	0.97	0.97
" S ":	19	1.14601		0.56	0.97	0.97	0.97	0.98	0.97	0.95	0.97	0.95	0.98	0.96
"SGMA":	12	1.13009		0.56	0.94	0.94	0.96	0.97	0.94	0.92	0.96	0.91	0.96	0.95
"Ramp":	16	B= 1.70	T= 0.6084	0.38	0.94	0.95	0.97	0.99	0.94	0.95	0.97	0.96	0.99	0.99
"Attr":	45	47 5	{for p50= 0.1242}	0.96	0.96	0.95	0.95	0.95	0.96	0.95	0.95	0.95	0.95	0.95
" S ":	21	1.16876		0.53	0.97	0.97	0.98	0.99	0.93	0.95	0.97	0.95	0.99	0.98
"SGMA":	13	1.15415		0.52	0.94	0.94	0.95	0.98	0.93	0.93	0.95	0.91	0.98	0.95

For AQL= 0.09680 (at 95%) :

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				Lognormal	Contaminated-Normal				Robustness						
					D = 1				D > 1						
					Y= 0.0	0.02	0.06	0.10	0.02		0.06		0.10		
									D=1.2	D=2.0	D=1.2	D=2.0	D=1.2	D=2.0	
"Ramp":	16	B= 0.50	T= 0.7069	0.82	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
"Attr":	19	20 4	{for p50= 0.2452}	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
" S ":	8	0.71509		0.81	0.94	0.93	0.94	0.94	0.93	0.92	0.94	0.91	0.94	0.89	0.89
"SGMA":	7	0.68955		0.82	0.93	0.93	0.94	0.94	0.93	0.92	0.93	0.91	0.93	0.90	0.90
"Ramp":	16	B= 0.90	T= 0.6421	0.68	0.94	0.95	0.95	0.95	0.95	0.94	0.95	0.94	0.94	0.94	0.95
"Attr":	19	20 4	{for p50= 0.2370}	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
" S ":	8	0.74257		0.78	0.93	0.93	0.93	0.93	0.92	0.91	0.92	0.89	0.93	0.88	0.88
"SGMA":	7	0.71605		0.79	0.92	0.92	0.93	0.94	0.92	0.91	0.92	0.89	0.93	0.88	0.88
"Ramp":	16	B= 1.30	T= 0.5735	0.58	0.93	0.93	0.94	0.94	0.93	0.93	0.94	0.93	0.94	0.94	0.93
"Attr":	24	26 5	{for p50= 0.2284}	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97	0.97
" S ":	10	0.76549		0.79	0.94	0.93	0.94	0.93	0.93	0.92	0.93	0.90	0.93	0.88	0.88
"SGMA":	8	0.74423		0.78	0.92	0.92	0.93	0.93	0.92	0.91	0.92	0.89	0.92	0.87	0.87
"Ramp":	16	B= 1.70	T= 0.5040	0.53	0.94	0.94	0.94	0.95	0.94	0.93	0.94	0.92	0.95	0.93	0.93
"Attr":	25	26 5	{for p50= 0.2233}	0.97	0.97	0.96	0.97	0.97	0.96	0.96	0.96	0.97	0.97	0.97	0.97
" S ":	11	0.78063		0.78	0.94	0.94	0.94	0.94	0.94	0.93	0.93	0.90	0.93	0.89	0.89
"SGMA":	9	0.76111		0.78	0.93	0.93	0.93	0.93	0.93	0.91	0.92	0.89	0.93	0.93	0.93

For AQL= 0.01390 (at 95%) :

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				Lognormal	Contaminated-Normal				Robustness						
					D = 1				D > 1						
					Y= 0.0	0.02	0.06	0.10	0.02		0.06		0.10		
									D=1.2	D=2.0	D=1.2	D=2.0	D=1.2	D=2.0	
"Ramp":	32	B= 0.50	T= 0.9264	0.69	0.94	0.97	-	-	0.97	0.97	-	-	-	-	-
"Attr":	56	58 2	{for p50= 0.0475}	0.95	0.95	0.95	-	-	0.95	0.95	-	-	-	-	-
" S ":	21	1.69114		0.19	0.92	1.00	-	-	1.00	1.00	-	-	-	-	-
"SGMA":	9	1.67000		0.29	0.94	0.98	-	-	0.98	0.97	-	-	-	-	-
"Ramp":	32	B= 0.90	T= 0.8990	0.30	0.95	0.98	-	-	0.98	0.98	-	-	-	-	-
"Attr":	91	93 3	{for p50= 0.0401}	0.96	0.96	0.95	-	-	0.95	0.95	-	-	-	-	-
" S ":	33	1.76349		0.07	0.99	1.00	-	-	1.00	1.00	-	-	-	-	-
"SGMA":	13	1.74972		1.17	0.93	0.99	-	-	0.99	0.98	-	-	-	-	-
"Ramp":	32	B= 1.30	T= 0.8625	0.08	0.95	0.99	-	-	0.99	0.99	-	-	-	-	-
"Attr":	131	141 4	{for p50= 0.0356}	0.95	0.95	0.95	-	-	0.95	0.95	-	-	-	-	-
" S ":	44	1.81453		0.02	0.98	1.00	-	-	1.00	1.00	-	-	-	-	-
"SGMA":	17	1.80398		0.11	0.94	1.00	-	-	1.00	0.99	-	-	-	-	-
"Ramp":	32	B= 1.70	T= 0.8152	0.02	0.95	0.99	-	-	0.99	0.99	-	-	-	-	-
"Attr":	174	187 5	{for p50= 0.0325}	0.95	0.95	0.95	-	-	0.95	0.95	-	-	-	-	-
" S ":	57	1.85415		0.01	0.99	0.99	-	-	1.00	1.00	-	-	-	-	-
"SGMA":	21	1.84587		0.07	0.97	0.99	-	-	0.99	0.99	-	-	-	-	-

For AQL= 0.02872 (at 95%) :

=====

				Lognormal	Contaminated-Normal				Robustness					
					D = 1				D > 1					
					Y= 0.0	0.02	0.06	0.10	0.02		0.06		0.10	
									D=1.2	D=2.0	D=1.2	D=2.0	D=1.2	D=2.0
"Ramp":	32	B= 0.50	T= 0.8854	0.70	0.94	0.95	-	-	0.95	0.95	-	-	-	-
"Attr":	62	68 4	{for p50= 0.0747}	0.95	0.95	0.96	-	-	0.96	0.96	-	-	-	-
" S ":	24	1.45743		0.29	0.97	0.98	-	-	0.98	0.97	-	-	-	-
"SGMA":	12	1.44158		0.35	0.94	0.95	-	-	0.95	0.94	-	-	-	-
"Ramp":	32	B= 0.90	T= 0.8472	0.34	0.95	0.96	-	-	0.96	0.96	-	-	-	-
"Attr":	84	90 5	{for p50= 0.0673}	0.96	0.96	0.96	-	-	0.96	0.96	-	-	-	-
" S ":	34	1.50732		0.18	0.98	0.99	-	-	0.98	0.98	-	-	-	-
"SGMA":	16	1.49590		0.28	0.94	0.95	-	-	0.94	0.93	-	-	-	-
"Ramp":	32	B= 1.30	T= 0.7991	0.12	0.95	0.97	-	-	0.97	0.97	-	-	-	-
"Attr":	107	114 6	{for p50= 0.0619}	0.95	0.95	0.95	-	-	0.95	0.95	-	-	-	-
" S ":	43	1.54823		0.10	0.97	0.99	-	-	0.99	0.99	-	-	-	-
"SGMA":	20	1.53902		0.21	0.95	0.97	-	-	0.96	0.94	-	-	-	-
"Ramp":	32	B= 1.70	T= 0.7405	0.05	0.95	0.97	-	-	0.97	0.97	-	-	-	-
"Attr":	113	114 6	{for p50= 0.0585}	0.95	0.95	0.95	-	-	0.95	0.95	-	-	-	-
" S ":	53	1.57469		0.05	0.98	1.00	-	-	1.00	0.99	-	-	-	-
"SGMA":	24	1.56712		0.15	0.95	0.97	-	-	0.97	0.95	-	-	-	-

For AQL= 0.05480 (at 95%) :

=====

				Lognormal	Contaminated-Normal				Robustness					
					D = 1				D > 1					
					Y= 0.0	0.02	0.06	0.10	0.02		0.06		0.10	
									D=1.2	D=2.0	D=1.2	D=2.0	D=1.2	D=2.0
"Ramp":	32	B= 0.50	T= 0.8269	0.71	0.94	0.95	0.96	0.97	0.94	0.94	0.96	0.96	0.97	0.98
"Attr":	56	59 6	{for p50= 0.1174}	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
" S ":	25	1.20065		0.46	0.97	0.97	0.97	0.99	0.97	0.95	0.97	0.94	0.99	0.98
"SGMA":	15	1.18815		0.48	0.94	0.94	0.95	0.98	0.93	0.91	0.94	0.89	0.98	0.95
"Ramp":	32	B= 0.90	T= 0.7773	0.41	0.94	0.94	0.96	0.98	0.94	0.94	0.97	0.97	0.98	0.98
"Attr":	70	72 7	{for p50= 0.1091}	0.95	0.95	0.96	0.95	0.96	0.96	0.96	0.95	0.95	0.96	0.96
" S ":	33	1.24084		0.38	0.97	0.97	0.99	0.99	0.97	0.96	0.98	0.95	0.99	0.98
"SGMA":	19	1.23114		0.41	0.94	0.94	0.96	0.99	0.94	0.92	0.95	0.90	0.98	0.95
"Ramp":	32	B= 1.30	T= 0.7176	0.21	0.94	0.96	0.97	0.99	0.96	0.95	0.97	0.96	0.99	1.00
"Attr":	83	85 8	{for p50= 0.1036}	0.96	0.96	0.95	0.96	0.95	0.95	0.95	0.96	0.96	0.95	0.95
" S ":	41	1.26930		0.30	0.99	0.98	0.98	1.00	0.98	0.96	0.98	0.94	1.00	0.99
"SGMA":	23	1.26137		0.35	0.93	0.95	0.96	0.99	0.94	0.93	0.95	0.88	0.99	0.96
"Ramp":	32	B= 1.70	T= 0.6508	0.12	0.94	0.95	0.97	0.99	0.95	0.95	0.97	0.96	0.99	0.99
"Attr":	96	98 9	{for p50= 0.1000}	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
" S ":	47	1.28831		0.26	0.98	0.98	0.98	0.99	0.98	0.96	0.98	0.93	0.99	0.99
"SGMA":	26	1.28131		0.31	0.93	0.94	0.96	0.99	0.94	0.92	0.95	0.90	0.98	0.97

For AQL= 0.09680 (at 95%) :

=====

Lognormal

Contaminated-Normal

Robustness

D = 1

D > 1

Y= 0.0 0.02 0.06 0.10

0.02 0.06 0.10
D=1.2 D=2.0 D=1.2 D=2.0 D=1.2 D=2.0

"Ramp":	32	B= 0.50	T= 0.7497	0.73	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94	0.94
"Attr":	32	33 6	{for p50= 0.2069}	0.96	0.96	0.96	0.97	0.97	0.96	0.96	0.97	0.97	0.97	0.97
" S ":	14	0.83315		0.76	0.95	0.94	0.94	0.97	0.94	0.93	0.94	0.90	0.93	0.88
"SGMA":	11	0.81712		0.74	0.94	0.93	0.93	0.96	0.93	0.92	0.92	0.88	0.93	0.87
"Ramp":	32	B= 0.90	T= 0.6885	0.50	0.94	0.94	0.95	0.96	0.94	0.94	0.95	0.94	0.96	0.95
"Attr":	33	33 6	{for p50= 0.1973}	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
" S ":	17	0.86428		0.74	0.95	0.95	0.96	0.96	0.95	0.93	0.95	0.92	0.95	0.90
"SGMA":	13	0.85137		0.73	0.94	0.93	0.94	0.95	0.93	0.92	0.94	0.90	0.94	0.89
"Ramp":	32	B= 1.30	T= 0.6201	0.36	0.85	0.86	0.87	0.89	0.86	0.93	0.87	0.84	0.89	0.85
"Attr":	40	41 7	{for p50= 0.1911}	0.96	0.96	0.95	0.96	0.96	0.95	0.95	0.96	0.96	0.96	0.96
" S ":	19	0.88631		0.74	0.96	0.96	0.95	0.96	0.96	0.95	0.95	0.92	0.95	0.90
"SGMA":	14	0.87400		0.71	0.93	0.93	0.93	0.93	0.93	0.92	0.92	0.88	0.92	0.86
"Ramp":	32	B= 1.70	T= 0.5493	0.27	0.93	0.93	0.94	0.96	0.93	0.93	0.94	0.92	0.96	0.93
"Attr":	40	41 7	{for p50= 0.1873}	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
" S ":	20	0.89966		0.72	0.95	0.95	0.96	0.96	0.95	0.94	0.95	0.91	0.96	0.89
"SGMA":	15	0.88782		0.69	0.93	0.93	0.93	0.94	0.93	0.91	0.93	0.88	0.93	0.86

For AQL= 0.01390 (at 95%) :

=====

Lognormal

Contaminated-Normal

Robustness

D = 1

D > 1

Y= 0.0 0.02 0.06 0.10

0.02 0.06 0.10
D=1.2 D=2.0 D=1.2 D=2.0 D=1.2 D=2.0

"Ramp":	64	B= 0.50	T= 0.9403	0.55	0.94	0.97	-	-	0.97	0.97	-	-	-	-
"Attr":	129	141 4	{for p50= 0.0359}	0.95	0.95	0.96	-	-	0.96	0.96	-	-	-	-
" S ":	41	1.81132		0.03	0.99	0.99	-	-	0.99	0.99	-	-	-	-
"SGMA":	16	1.80000		0.13	0.94	0.99	-	-	0.99	0.98	-	-	-	-
"Ramp":	64	B= 0.90	T= 0.9165	0.09	0.95	0.99	-	-	0.99	0.94	-	-	-	-
"Attr":	183	187 5	{for p50= 0.0309}	0.95	0.95	0.95	-	-	0.95	0.96	-	-	-	-
" S ":	66	1.87495		0.01	1.00	1.00	-	-	1.00	0.93	-	-	-	-
"SGMA":	24	1.86774		0.05	0.96	1.00	-	-	1.00	0.92	-	-	-	-
"Ramp":	64	B= 1.30	T= 0.8823	0.01	0.95	1.00	-	-	1.00	0.85	-	-	-	-
"Attr":	274	286 7	{for p50= 0.0280}	0.95	0.95	0.95	-	-	0.95	0.95	-	-	-	-
" S ":	90	1.91705		0.00	1.00	1.00	-	-	1.00	0.95	-	-	-	-
"SGMA":	32	1.91167		0.01	0.94	1.00	-	-	1.00	0.92	-	-	-	-
"Ramp":	64	B= 1.70	T= 0.8370	0.00	0.95	1.00	-	-	1.00	1.00	-	-	-	-
"Attr":	334	337 8	{for p50= 0.0259}	0.95	0.95	0.95	-	-	0.95	0.95	-	-	-	-
" S ":	118	1.94876		0.00	1.00	1.00	-	-	1.00	1.00	-	-	-	-
"SGMA":	41	1.94459		0.00	0.95	1.00	-	-	1.00	1.00	-	-	-	-

For AQL= 0.02872 (at 95%) :

=====

	Lognormal			Contaminated-Normal				Robustness						
				D = 1				D > 1						
				Y= 0.0	0.02	0.06	0.10	0.02		0.06		0.10		
				D=1.2	D=2.0	D=1.2	D=2.0	D=1.2	D=2.0					
"Ramp":	64	B= 0.50	T= 0.9049	0.53	0.94	0.96	-	-	0.96	0.96	-	-	-	-
"Attr":	113	114 6	{for p50= 0.0590}	0.95	0.95	0.95	-	-	0.95	0.95	-	-	-	-
" S ":	51	1.57144		0.06	0.98	1.00	-	-	1.00	0.99	-	-	-	-
"SGMA":	23	1.56358		0.15	0.95	0.97	-	-	0.97	0.94	-	-	-	-
"Ramp":	64	B= 0.90	T= 0.8696	0.11	0.95	0.97	-	-	0.97	0.97	-	-	-	-
"Attr":	159	163 8	{for p50= 0.0363}	0.95	0.95	0.96	-	-	0.96	0.96	-	-	-	-
" S ":	68	1.60982		0.02	0.98	0.99	-	-	0.99	0.98	-	-	-	-
"SGMA":	30	1.60381		0.08	0.94	0.95	-	-	0.95	0.93	-	-	-	-
"Ramp":	64	B= 1.30	T= 0.8234	0.01	0.95	0.97	-	-	0.97	0.97	-	-	-	-
"Attr":	210	214 10	{for p50= 0.0506}	0.95	0.95	0.96	-	-	0.96	0.96	-	-	-	-
" S ":	91	1.64382		0.00	0.98	0.99	-	-	0.99	0.99	-	-	-	-
"SGMA":	39	1.63926		0.04	0.95	0.97	-	-	0.97	0.94	-	-	-	-
"Ramp":	64	B= 1.70	T= 0.7663	0.00	0.95	0.98	-	-	0.98	0.97	-	-	-	-
"Attr":	262	267 12	{for p50= 0.0483}	0.95	0.95	0.95	-	-	0.95	0.95	-	-	-	-
" S ":	112	1.66490		0.00	0.98	1.00	-	-	1.00	0.99	-	-	-	-
"SGMA":	47	1.66115		0.02	0.94	0.97	-	-	0.95	0.94	-	-	-	-

For AQL= 0.05480 (at 95%) :

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	Lognormal			Contaminated-Normal				Robustness						
				D = 1				D > 1						
				Y= 0.0	0.02	0.06	0.10	0.02		0.06		0.10		
				D=1.2	D=2.0	D=1.2	D=2.0	D=1.2	D=2.0					
"Ramp":	64	B= 0.50	T= 0.8520	0.55	0.95	0.96	0.97	0.97	0.96	0.96	0.97	0.97	0.98	0.98
"Attr":	110	112 10	{for p50= 0.0968}	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
" S ":	55	1.30605		0.19	0.98	0.98	0.99	0.99	0.98	0.96	0.99	0.95	0.99	0.99
"SGMA":	30	1.30000		0.28	0.95	0.96	0.97	0.99	0.95	0.93	0.96	0.91	0.98	0.97
"Ramp":	64	B= 0.90	T= 0.8046	0.15	0.95	0.95	0.98	1.00	0.95	0.94	0.98	0.98	1.00	1.00
"Attr":	138	140 12	{for p50= 0.0912}	0.96	0.96	0.96	0.95	0.95	0.96	0.96	0.95	0.95	0.95	0.95
" S ":	70	1.33793		0.11	0.98	0.98	1.00	1.00	0.98	0.96	0.99	0.95	1.00	1.00
"SGMA":	37	1.33308		0.20	0.94	0.94	0.97	1.00	0.94	0.91	0.96	0.91	1.00	0.97
"Ramp":	64	B= 1.30	T= 0.7463	0.02	0.94	0.96	0.97	0.99	0.96	0.96	0.97	0.97	0.99	0.99
"Attr":	167	168 14	{for p50= 0.0874}	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
" S ":	86	1.36096		0.05	0.97	0.98	0.98	0.99	0.98	0.96	0.98	0.94	0.99	0.99
"SGMA":	45	1.35695		0.12	0.93	0.94	0.96	0.99	0.93	0.90	0.96	0.88	0.99	0.97
"Ramp":	64	B= 1.70	T= 0.6800	0.00	0.94	0.96	0.98	0.99	0.95	0.96	0.98	0.97	0.99	0.99
"Attr":	196	197 16	{for p50= 0.0850}	0.96	0.96	0.96	0.96	0.96	0.96	0.94	0.96	0.96	0.96	0.96
" S ":	101	1.37597		0.02	0.97	0.98	0.99	0.99	0.98	0.96	0.99	0.94	0.99	0.99
"SGMA":	52	1.37253		0.09	0.94	0.95	0.97	0.99	0.94	0.90	0.96	0.88	0.99	0.98

For AQL= 0.09680 (at 95%) :

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			Lognormal	Contaminated-Normal				Robustness						
				D = 1				D > 1						
				Y= 0.0	0.02	0.06	0.10	0.02		0.06		0.10		
								D=1.2	D=2.0	D=1.2	D=2.0	D=1.2	D=2.0	
"Ramp":	64	B= 0.50	T= 0.7802	0.58	0.92	0.94	0.94	0.95	0.93	0.92	0.94	0.92	0.94	0.90
"Attr":	54	54 9	{for p50= 0.1785}	0.96	0.96	0.96	0.97	0.96	0.96	0.96	0.97	0.97	0.96	0.96
" S ":	25	0.93067		0.68	0.96	0.96	0.95	0.96	0.95	0.94	0.95	0.90	0.95	0.88
"SGMA":	18	0.92097		0.66	0.94	0.94	0.94	0.95	0.94	0.92	0.93	0.88	0.93	0.85
"Ramp":	64	B= 0.90	T= 0.7204	0.26	0.95	0.95	0.94	0.96	0.95	0.94	0.95	0.94	0.97	0.95
"Attr":	62	63 10	{for p50= 0.1715}	0.95	0.95	0.96	0.96	0.95	0.95	0.95	0.96	0.96	0.95	0.95
" S ":	30	0.95662		0.64	0.94	0.94	0.94	0.95	0.94	0.92	0.93	0.88	0.94	0.86
"SGMA":	21	0.94838		0.63	0.94	0.94	0.94	0.95	0.94	0.92	0.93	0.88	0.94	0.86
"Ramp":	64	B= 1.30	T= 0.6524	0.10	0.93	0.95	0.95	0.96	0.93	0.92	0.95	0.96	0.96	0.94
"Attr":	69	71 11	{for p50= 0.1668}	0.96	0.96	0.95	0.96	0.96	0.97	0.97	0.96	0.93	0.96	0.94
" S ":	35	0.97413		0.60	0.96	0.97	0.97	0.96	0.95	0.94	0.96	0.90	0.95	0.87
"SGMA":	24	0.96696		0.59	0.94	0.94	0.94	0.94	0.93	0.91	0.94	0.88	0.93	0.84
"Ramp":	64	B= 1.70	T= 0.5809	0.05	0.93	0.95	0.95	0.96	0.94	0.93	0.95	0.91	0.96	0.91
"Attr":	71	71 11	{for p50= 0.1640}	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96
" S ":	38	0.98462		0.59	0.96	0.97	0.97	0.96	0.96	0.95	0.96	0.90	0.96	0.87
"SGMA":	26	0.97797		0.58	0.93	0.94	0.94	0.95	0.94	0.92	0.93	0.87	0.93	0.84

Appendix (F.2.)

Table (5.4.2) : Results of The Variance-Effect Acceptance Probability
for "Ramp" and " &-plan" at the given AQL

Note :

1. In this table for each value of B there are two rows .The first row shows the "pa" resulting from variance changes for RAMP while the second row shows that for &-plan for which "n" is given at the end of its row.
2. The value of the changed variance does not appear on the table for space saving since it is easy to evaluate .For each double entry it is equal to the quotient of the bracketed B (on the left) over the top column B value . Such values of & are given in the subsidiary table annexed to this table.
3. The value of the specific AQL is given below as p0 .
4. The second column in each sub-table gives the value of the test criterion which is t for the Ramp and K for the &-plan . If a value of -1.0000 is given for t this indicates "Non-existence" problem and hence the label "NE" shown below .("Non-existence" is defined and discussed elsewhere) .

* S. Size= 4 ARU=2.20 (i.e. p0= 0.0139) *

(P)	Test Criter.	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma
(0.5)	-1.0000	NE	NE	NE	NE	NE	NE	NE	NE	
(0.7)	0.8275	0.97	0.95	0.93	0.90	0.86	0.81	0.75	0.67	
	1.2713	0.99	0.95	0.84	0.64	0.39	0.18	0.06	0.02	3
(0.9)	0.7961	0.98	0.97	0.95	0.93	0.90	0.86	0.81	0.74	
	1.2909	0.99	0.98	0.94	0.86	0.72	0.53	0.34	0.18	3

(1.1)	0.7684	0.99	0.98	0.97	0.95	0.94	0.90	0.85	0.80	
	1.3148	1.00	0.99	0.97	0.94	0.93	0.70	0.61	0.45	3
(1.3)	-1.0000	NE	NE	NE	NE	NE	NE	NE	NE	
(1.5)	0.4976	1.00	0.99	0.99	0.98	0.97	0.95	0.93	0.90	
	1.2709	1.00	1.00	0.99	0.99	0.97	0.95	0.91	0.85	3
(1.7)	0.4638	1.00	0.99	0.99	0.99	0.98	0.97	0.95	0.93	
	1.2925	1.00	1.00	1.00	0.99	0.98	0.97	0.94	0.90	7
(1.9)	0.6313	1.00	1.00	0.99	0.99	0.98	0.98	0.97	0.95	
	1.3135	1.00	1.00	1.00	0.99	0.99	0.98	0.96	0.94	3

* s. size= 4 AMU=2.00 (i.e. p0= 0.0287) *

(B)	Test Criter.	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma
(0.5)	-1.0000	NE	NE	NE	NE	NE	NE	NE	NE	
(0.7)	-1.0000	NE	NE	NE	NE	NE	NE	NE	NE	
(0.9)	-1.0000	NE	NE	NE	NE	NE	NE	NE	NE	
(1.1)	0.4646	0.99	0.98	0.97	0.95	0.93	0.90	0.87	0.82	
	0.8524	0.98	0.97	0.96	0.93	0.90	0.85	0.80	0.73	2
(1.3)	0.4284	0.99	0.99	0.98	0.97	0.95	0.93	0.90	0.87	
	0.8754	0.99	0.98	0.97	0.95	0.93	0.90	0.86	0.81	2
(1.5)	0.5954	0.99	0.99	0.98	0.98	0.97	0.95	0.93	0.90	
	1.0000	1.00	0.99	0.99	0.98	0.96	0.94	0.91	0.86	3
(1.7)	0.5630	1.00	0.99	0.99	0.98	0.98	0.97	0.95	0.93	
	0.9176	0.99	0.98	0.98	0.97	0.95	0.94	0.92	0.89	2
(1.9)	0.5305	1.00	1.00	0.99	0.99	0.99	0.98	0.97	0.95	
	0.9345	0.99	0.99	0.98	0.97	0.96	0.95	0.93	0.91	2

* s. size= 4 AMU=1.60 (i.e. p0= 0.0548) *

(B)	Test Criter.	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma
(0.5)	-1.0000	NE	NE	NE	NE	NE	NE	NE	NE	
(0.7)	-1.0000	NE	NE	NE	NE	NE	NE	NE	NE	
(0.9)	-1.0000	NE	NE	NE	NE	NE	NE	NE	NE	
(1.1)	0.5463	0.99	0.98	0.97	0.96	0.94	0.92	0.88	0.84	
	0.5808	0.97	0.96	0.94	0.93	0.90	0.87	0.84	0.80	2
(1.3)	0.5158	0.99	0.99	0.98	0.97	0.96	0.94	0.91	0.88	
	0.4022	0.97	0.96	0.95	0.94	0.92	0.90	0.87	0.85	2
(1.5)	0.4941	1.00	0.99	0.99	0.98	0.97	0.95	0.93	0.90	
	0.4454	0.97	0.97	0.96	0.94	0.93	0.91	0.89	0.87	2
(1.7)	0.4567	1.00	0.99	0.99	0.98	0.98	0.97	0.95	0.93	
	0.4234	0.98	0.97	0.96	0.95	0.94	0.93	0.92	0.90	2
(1.9)	0.4234	1.00	1.00	0.99	0.99	0.98	0.98	0.96	0.95	
	0.4400	0.98	0.97	0.97	0.96	0.95	0.94	0.93	0.91	2

* s. size= 4 AMU=1.30 (i.e. p0= 0.0960) *

(B)	Test Criter.	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma
(0.5)	-1.0000	NE	NE	NE	NE	NE	NE	NE	NE	
(0.7)	-1.0000	NE	NE	NE	NE	NE	NE	NE	NE	
(0.9)	-1.0000	NE	NE	NE	NE	NE	NE	NE	NE	
(1.1)	0.4450	0.98	0.98	0.96	0.95	0.93	0.90	0.87	0.83	
	0.4600	0.97	0.96	0.95	0.94	0.92	0.90	0.88	0.85	3
(1.3)	0.4057	0.99	0.98	0.98	0.97	0.95	0.93	0.91	0.88	
	0.3106	0.95	0.95	0.94	0.93	0.92	0.91	0.90	0.88	2
(1.5)	0.3722	0.99	0.99	0.98	0.98	0.97	0.95	0.93	0.91	
	0.3188	0.95	0.95	0.94	0.93	0.93	0.92	0.91	0.90	2
(1.7)	0.3421	1.00	0.99	0.99	0.98	0.97	0.96	0.95	0.93	
	0.3260	0.96	0.95	0.94	0.94	0.93	0.92	0.92	0.91	2
(1.9)	0.3143	1.00	0.99	0.99	0.99	0.98	0.97	0.96	0.95	
	0.3362	0.96	0.95	0.95	0.94	0.94	0.93	0.92	0.91	2

* s. size= 8 AMU=2.20 (i.e. p0= 0.0139) *

(B)	Test Criter.	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma
(0.5)	-1.0000	NE	NE	NE	NE	NE	NE	NE	NE	
(0.7)	0.2706	0.97	0.95	0.92	0.87	0.81	0.73	0.63	0.51	
	1.3964	0.99	0.95	0.79	0.50	0.22	0.06	0.01	0.00	4
(0.9)	0.2393	0.98	0.97	0.95	0.92	0.88	0.82	0.74	0.64	
	1.4157	1.00	0.99	0.94	0.83	0.62	0.37	0.17	0.06	4
(1.1)	0.2141	0.99	0.98	0.97	0.95	0.92	0.88	0.82	0.73	
	1.4464	1.00	0.99	0.98	0.93	0.84	0.68	0.47	0.28	4
(1.3)	0.2899	0.99	0.99	0.98	0.97	0.95	0.92	0.87	0.81	
	1.4794	1.00	1.00	1.00	0.98	0.95	0.86	0.72	0.53	5
(1.5)	0.2640	1.00	0.99	0.99	0.98	0.97	0.95	0.92	0.87	
	1.5089	1.00	1.00	1.00	0.99	0.98	0.94	0.86	0.74	5
(1.7)	0.2357	1.00	1.00	1.00	0.99	0.98	0.97	0.95	0.92	
	1.5332	1.00	1.00	1.00	1.00	0.99	0.98	0.95	0.88	6
(1.9)	0.2056	1.00	1.00	1.00	1.00	0.99	0.98	0.97	0.95	
	1.5537	1.00	1.00	1.00	1.00	1.00	0.99	0.98	0.94	6

* S. Size= 8 AMU=1.90 (i.e. p0= 0.0207) *

(B)	Test Criter.	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma
(0.5)		0.8290	0.95	0.92	0.87	0.81	0.74	0.64	0.53	0.40
		1.1425	0.94	0.73	0.38	0.11	0.02	0.00	0.00	0.00
(0.7)		0.7964	0.97	0.95	0.92	0.88	0.82	0.75	0.65	0.53
		1.1628	0.98	0.93	0.79	0.56	0.30	0.12	0.03	0.01
(0.9)		0.7693	0.98	0.97	0.95	0.92	0.88	0.82	0.73	0.63
		1.1848	1.00	0.99	0.95	0.84	0.66	0.43	0.22	0.09
(1.1)		0.7410	0.99	0.98	0.97	0.95	0.92	0.87	0.81	0.72
		1.2000	1.00	0.99	0.98	0.94	0.86	0.72	0.54	0.35
(1.3)		0.7104	1.00	0.99	0.98	0.97	0.95	0.92	0.87	0.80
		1.2223	1.00	1.00	0.99	0.97	0.94	0.86	0.75	0.60
(1.5)		0.6794	1.00	0.99	0.99	0.98	0.97	0.95	0.92	0.87
		1.2434	1.00	1.00	1.00	0.99	0.98	0.95	0.89	0.79
(1.7)		0.6475	1.00	1.00	0.99	0.99	0.98	0.97	0.95	0.92
		1.2617	1.00	1.00	1.00	1.00	0.99	0.97	0.94	0.88
(1.9)		0.6146	1.00	1.00	1.00	1.00	0.99	0.98	0.97	0.95
		1.2762	1.00	1.00	1.00	1.00	0.99	0.99	0.97	0.94

* S. Size= 8 AMU=1.60 (i.e. p0= 0.0548) *

(B)	Test Criter.	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma
(0.5)		0.7556	0.95	0.91	0.85	0.79	0.71	0.61	0.50	0.38
		0.8589	0.93	0.79	0.54	0.28	0.10	0.03	0.00	0.00
(0.7)		0.7142	0.97	0.95	0.92	0.88	0.82	0.74	0.64	0.52
		0.7002	0.98	0.95	0.87	0.75	0.59	0.41	0.25	0.13
(0.9)		0.6765	0.98	0.97	0.95	0.92	0.88	0.82	0.74	0.64
		0.8017	0.99	0.97	0.94	0.89	0.81	0.70	0.57	0.43
(1.1)		0.6458	0.99	0.98	0.97	0.95	0.92	0.88	0.81	0.73
		0.8278	0.99	0.98	0.97	0.94	0.89	0.83	0.74	0.62
(1.3)		0.6146	1.00	0.99	0.98	0.97	0.95	0.92	0.87	0.80
		0.8517	0.99	0.99	0.98	0.96	0.93	0.89	0.83	0.76
(1.5)		0.5807	1.00	0.99	0.99	0.98	0.97	0.95	0.92	0.87
		0.8651	1.00	1.00	0.99	0.98	0.97	0.95	0.92	0.87
(1.7)		0.5468	1.00	1.00	0.99	0.99	0.98	0.97	0.95	0.92
		0.8778	1.00	1.00	0.99	0.99	0.98	0.97	0.95	0.92
(1.9)		0.5132	1.00	1.00	1.00	1.00	0.99	0.98	0.97	0.95
		0.8870	1.00	1.00	1.00	0.99	0.99	0.98	0.96	0.94

* S. Size= 8 AMU=1.30 (i.e. p0= 0.0968) *

(B)	Test Criter.	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma
(0.5)		-1.0000	NE	NE	NE	NE	NE	NE	NE	
(0.7)		0.6117	0.97	0.95	0.92	0.88	0.82	0.74	0.65	0.53
		0.5434	0.97	0.93	0.89	0.81	0.72	0.61	0.48	0.36
(0.9)		0.5740	0.98	0.97	0.95	0.92	0.88	0.82	0.74	0.65
		0.5260	0.98	0.96	0.94	0.91	0.86	0.80	0.73	0.65
(1.1)		0.5396	0.99	0.98	0.97	0.95	0.92	0.88	0.82	0.74
		0.5508	0.98	0.97	0.96	0.93	0.90	0.86	0.82	0.76
(1.3)		0.5055	0.99	0.99	0.98	0.97	0.95	0.92	0.88	0.82
		0.5647	0.99	0.99	0.98	0.97	0.95	0.93	0.90	0.86
(1.5)		0.4717	1.00	0.99	0.99	0.98	0.97	0.95	0.92	0.87
		0.5747	0.99	0.99	0.98	0.98	0.96	0.95	0.93	0.90
(1.7)		0.4386	1.00	1.00	0.99	0.99	0.98	0.97	0.95	0.92
		0.5819	0.99	0.99	0.99	0.98	0.97	0.96	0.95	0.93
(1.9)		0.4070	1.00	1.00	1.00	0.99	0.99	0.98	0.97	0.95
		0.5869	0.99	0.99	0.99	0.98	0.98	0.97	0.96	0.94

* S. Size= 16 AMU=2.20 (i.e. p0= 0.0139) *

(B)	Test Criter.	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma
(0.5)		0.8090	0.95	0.91	0.86	0.78	0.68	0.54	0.38	0.23
		1.5000	0.94	0.59	0.13	0.01	0.00	0.00	0.00	0.00
(0.7)		0.8910	0.97	0.95	0.92	0.86	0.78	0.66	0.51	0.34
		1.5495	1.00	0.94	0.69	0.28	0.05	0.00	0.00	0.00
(0.9)		0.8742	0.99	0.97	0.95	0.91	0.85	0.75	0.62	0.45
		1.6000	1.00	0.99	0.94	0.74	0.38	0.11	0.01	0.00
(1.1)		0.8549	0.99	0.99	0.97	0.95	0.91	0.84	0.73	0.58
		1.6335	1.00	1.00	0.99	0.95	0.78	0.47	0.18	0.04
(1.3)		0.8332	1.00	0.99	0.99	0.98	0.95	0.90	0.83	0.70
		1.6629	1.00	1.00	1.00	0.99	0.95	0.80	0.53	0.24
(1.5)		0.8095	1.00	1.00	1.00	0.99	0.98	0.95	0.90	0.81
		1.6891	1.00	1.00	1.00	1.00	0.99	0.95	0.82	0.58
(1.7)		0.7832	1.00	1.00	1.00	1.00	0.99	0.98	0.95	0.90
		1.7118	1.00	1.00	1.00	1.00	1.00	0.99	0.95	0.83
(1.9)		0.7546	1.00	1.00	1.00	1.00	1.00	0.99	0.98	0.95
		1.7303	1.00	1.00	1.00	1.00	1.00	1.00	0.99	0.95

* S. Size= 16 AMU=1.90 (i.e. p0= 0.0287) *

(B)	Test Criter.	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma
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Criter.		B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma
(0.5)	0.8610 1.2771	0.95 0.94	0.91 0.61	0.85 0.16	0.76 0.01	0.64 0.00	0.49 0.00	0.34 0.00	0.19 0.00	6
(0.7)	0.8368 1.3168	0.97 0.99	0.95 0.94	0.91 0.71	0.85 0.33	0.76 0.07	0.63 0.01	0.47 0.00	0.20 0.00	7
(0.9)	0.8147 1.3537	0.99 1.00	0.97 0.99	0.95 0.95	0.91 0.77	0.84 0.43	0.73 0.14	0.59 0.02	0.42 0.00	9
(1.1)	0.7900 1.3797	0.99 1.00	0.99 1.00	0.97 0.99	0.95 0.94	0.91 0.79	0.83 0.52	0.71 0.24	0.55 0.07	9
(1.3)	0.7632 1.4024	1.00 1.00	0.99 1.00	0.99 1.00	0.98 0.99	0.95 0.94	0.90 0.81	0.82 0.58	0.69 0.32	10
(1.5)	0.7340 1.4222	1.00 1.00	1.00 1.00	1.00 1.00	0.99 1.00	0.98 0.99	0.95 0.94	0.90 0.73	0.81 0.63	11
(1.7)	0.7029 1.4380	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	0.99 1.00	0.98 0.99	0.95 0.95	0.89 0.84	12
(1.9)	0.6704 1.4506	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	0.99 1.00	0.98 0.99	0.95 0.95	13

* S. Size= 16 AMU=1.60 (i.e. p0= 0.0548) *

Criter.		B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma
(0.5)	0.7927 0.9561	0.95 0.94	0.91 0.74	0.85 0.38	0.75 0.11	0.62 0.02	0.47 0.00	0.31 0.00	0.17 0.00	6
(0.7)	0.7653 0.9715	0.97 0.99	0.95 0.94	0.91 0.81	0.84 0.57	0.74 0.31	0.60 0.12	0.44 0.03	0.27 0.01	6
(0.9)	0.7373 0.9926	0.99 1.00	0.97 0.99	0.95 0.95	0.91 0.85	0.83 0.67	0.72 0.44	0.57 0.23	0.40 0.09	7
(1.1)	0.7075 1.1131	0.99 1.00	0.99 1.00	0.98 0.99	0.95 0.95	0.90 0.83	0.82 0.61	0.70 0.34	0.55 0.14	11
(1.3)	0.6758 1.1301	1.00 1.00	1.00 1.00	0.99 1.00	0.98 0.99	0.95 0.95	0.90 0.85	0.81 0.86	0.69 0.43	12
(1.5)	0.6425 1.1435	1.00 1.00	1.00 1.00	1.00 1.00	0.99 1.00	0.98 0.98	0.95 0.94	0.90 0.85	0.81 0.70	12
(1.7)	0.6084 1.1541	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	0.99 1.00	0.98 0.98	0.95 0.95	0.90 0.87	13
(1.9)	0.5741 1.1624	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	0.99 0.99	0.98 0.98	0.95 0.95	14

* S. Size= 16 AMU=1.30 (i.e. p0= 0.0964) *

Criter.		B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma
(0.5)	0.7069 0.8295	0.95 0.95	0.91 0.81	0.84 0.58	0.74 0.28	0.61 0.10	0.45 0.02	0.29 0.00	0.16 0.00	7
(0.7)	0.6749 0.7000	0.97 0.98	0.95 0.94	0.91 0.86	0.84 0.70	0.73 0.50	0.59 0.30	0.43 0.14	0.27 0.06	7
(0.9)	0.6421 0.7160	0.99 0.99	0.98 0.98	0.95 0.94	0.90 0.87	0.83 0.76	0.72 0.61	0.57 0.44	0.41 0.29	7
(1.1)	0.6083 0.7317	1.00 1.00	0.99 0.99	0.98 0.98	0.95 0.95	0.90 0.89	0.82 0.80	0.71 0.68	0.56 0.54	8
(1.3)	0.5735 0.7442	1.00 1.00	1.00 0.99	0.99 0.99	0.98 0.97	0.95 0.94	0.90 0.89	0.82 0.82	0.70 0.73	8
(1.5)	0.5385 0.7536	1.00 1.00	1.00 1.00	1.00 0.99	0.99 0.99	0.98 0.97	0.95 0.95	0.90 0.91	0.82 0.85	9
(1.7)	0.5040 0.7611	1.00 1.00	1.00 1.00	1.00 1.00	1.00 0.99	0.99 0.98	0.98 0.97	0.95 0.95	0.90 0.91	9
(1.9)	0.4705 0.7662	1.00 1.00	1.00 1.00	1.00 1.00	1.00 0.99	1.00 0.99	0.99 0.98	0.98 0.97	0.95 0.95	9

* S. Size= 32 AMU=2.20 (i.e. p0= 0.0139) *

Criter.		B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma
(0.5)	0.9264 1.6700	0.95 0.94	0.91 0.34	0.83 0.01	0.71 0.00	0.54 0.00	0.34 0.00	0.16 0.00	0.06 0.00	9
(0.7)	0.9133 1.7134	0.98 1.00	0.95 0.95	0.90 0.50	0.81 0.05	0.67 0.00	0.48 0.00	0.27 0.00	0.11 0.00	11
(0.9)	0.8990 1.7497	0.99 1.00	0.98 1.00	0.95 0.95	0.89 0.59	0.79 0.12	0.62 0.00	0.40 0.00	0.20 0.00	13
(1.1)	0.8824 1.7805	1.00 1.00	0.99 1.00	0.98 1.00	0.95 0.95	0.88 0.84	0.76 0.19	0.57 0.02	0.34 0.00	15
(1.3)	0.8625 1.8040	1.00 1.00	1.00 1.00	0.99 1.00	0.98 1.00	0.95 0.95	0.88 0.69	0.74 0.26	0.52 0.04	17
(1.5)	0.8402 1.8270	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	0.98 1.00	0.95 0.95	0.87 0.71	0.71 0.31	19
(1.7)	0.8152 1.8459	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	0.98 1.00	0.95 0.95	0.86 0.73	21
(1.9)	0.7877 1.8609	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00	0.99 0.99	0.95 0.95	23

* S. Size= 32 AMU=1.90 (i.e. p0= 0.0287) *

Criter.		B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma
(0.5)	0.8854 1.4416	0.95 0.94	0.90 0.34	0.81 0.01	0.66 0.00	0.47 0.00	0.27 0.00	0.11 0.00	0.03 0.00	12
(0.7)	0.8671 1.4701	0.98 1.00	0.95 0.95	0.89 0.51	0.79 0.06	0.62 0.00	0.41 0.00	0.21 0.00	0.08 0.00	14

(0.9)	0.8472	0.99	0.98	0.95	0.89	0.76	0.58	0.39	0.16	
	1.4959	1.00	1.00	0.95	0.61	0.15	0.01	0.00	0.00	16
(1.1)	0.8245	1.00	0.99	0.98	0.95	0.88	0.74	0.60	0.40	
	1.5193	1.00	1.00	1.00	0.95	0.67	0.23	0.03	0.00	18
(1.3)	0.7991	1.00	1.00	0.99	0.98	0.95	0.87	0.72	0.49	
	1.5390	1.00	1.00	1.00	1.00	0.95	0.71	0.21	0.06	20
(1.5)	0.7708	1.00	1.00	1.00	1.00	0.98	0.95	0.86	0.70	
	1.5543	1.00	1.00	1.00	1.00	0.95	0.74	0.37	0.06	22
(1.7)	0.7405	1.00	1.00	1.00	1.00	1.00	0.99	0.93	0.86	
	1.5671	1.00	1.00	1.00	1.00	1.00	0.99	0.85	0.77	24
(1.9)	0.7085	1.00	1.00	1.00	1.00	1.00	1.00	0.99	0.95	
	1.5774	1.00	1.00	1.00	1.00	1.00	1.00	0.99	0.95	25

* S. Size= 32 AMU=1.60 (i.e. p0= 0.0542) *

(B) Test	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma	
Crater.										
(0.5)	0.8269	0.95	0.89	0.79	0.62	0.42	0.22	0.08	0.02	
	1.1882	0.94	0.40	0.02	0.00	0.00	0.00	0.00	0.00	15
(0.7)	0.8036	0.98	0.95	0.89	0.77	0.58	0.36	0.17	0.06	
	1.2120	1.00	0.95	0.57	0.10	0.00	0.00	0.00	0.00	17
(0.9)	0.7773	0.99	0.98	0.95	0.88	0.75	0.54	0.32	0.14	
	1.2311	1.00	1.00	0.95	0.66	0.22	0.02	0.00	0.00	19
(1.1)	0.7486	1.00	0.99	0.98	0.95	0.87	0.73	0.51	0.28	
	1.2477	1.00	1.00	1.00	0.95	0.72	0.32	0.07	0.01	21
(1.3)	0.7176	1.00	1.00	1.00	0.98	0.95	0.87	0.71	0.49	
	1.2614	1.00	1.00	1.00	0.99	0.95	0.76	0.41	0.12	23
(1.5)	0.6848	1.00	1.00	1.00	1.00	0.98	0.95	0.86	0.70	
	1.2725	1.00	1.00	1.00	1.00	0.99	0.95	0.78	0.48	25
(1.7)	0.6508	1.00	1.00	1.00	1.00	1.00	0.99	0.95	0.86	
	1.2813	1.00	1.00	1.00	1.00	1.00	0.99	0.95	0.80	26
(1.9)	0.6162	1.00	1.00	1.00	1.00	1.00	1.00	0.99	0.95	
	1.2881	1.00	1.00	1.00	1.00	1.00	1.00	0.99	0.95	27

* S. Size= 32 AMU=1.30 (i.e. p0= 0.0960) *

(B) Test	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma	
Crater.										
(0.5)	0.7497	0.95	0.89	0.77	0.59	0.38	0.19	0.07	0.02	
	0.8171	0.95	0.70	0.29	0.05	0.00	0.00	0.00	0.00	11
(0.7)	0.7202	0.98	0.95	0.88	0.75	0.56	0.34	0.16	0.05	
	0.8357	0.99	0.95	0.78	0.48	0.19	0.04	0.01	0.00	12
(0.9)	0.6885	0.99	0.98	0.95	0.88	0.74	0.53	0.31	0.14	
	0.8514	1.00	0.99	0.95	0.85	0.60	0.25	0.07	0.01	13
(1.1)	0.6549	1.00	1.00	0.98	0.95	0.87	0.73	0.51	0.29	
	0.8640	1.00	1.00	0.99	0.95	0.85	0.68	0.45	0.24	14
(1.3)	0.6201	1.00	1.00	1.00	0.98	0.95	0.87	0.72	0.50	
	0.8740	1.00	1.00	1.00	0.98	0.94	0.86	0.72	0.53	14
(1.5)	0.5846	1.00	1.00	1.00	1.00	0.98	0.95	0.87	0.71	
	0.8816	1.00	1.00	1.00	0.99	0.98	0.95	0.86	0.76	15
(1.7)	0.5493	1.00	1.00	1.00	1.00	1.00	0.98	0.95	0.87	
	0.8878	1.00	1.00	1.00	1.00	0.99	0.98	0.94	0.88	15
(1.9)	0.5147	1.00	1.00	1.00	1.00	1.00	1.00	0.98	0.95	
	0.8922	1.00	1.00	1.00	1.00	1.00	0.99	0.98	0.95	16

* S. Size= 64 AMU=2.20 (i.e. p0= 0.0139) *

(B) Test	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma	
Crater.										
(0.5)	0.9403	0.95	0.89	0.76	0.56	0.31	0.11	0.02	0.00	
	1.8000	0.95	0.10	0.00	0.00	0.00	0.00	0.00	0.00	16
(0.7)	0.9294	0.98	0.95	0.88	0.72	0.48	0.22	0.06	0.01	
	1.8383	1.00	0.95	0.23	0.00	0.00	0.00	0.00	0.00	20
(0.9)	0.9165	0.99	0.98	0.95	0.86	0.67	0.40	0.15	0.03	
	1.8677	1.00	1.00	0.95	0.34	0.01	0.00	0.00	0.00	24
(1.1)	0.9011	1.00	1.00	0.99	0.95	0.84	0.62	0.32	0.09	
	1.8927	1.00	1.00	1.00	0.95	0.42	0.02	0.00	0.00	28
(1.3)	0.8823	1.00	1.00	1.00	0.99	0.95	0.83	0.58	0.26	
	1.9117	1.00	1.00	1.00	1.00	0.95	0.49	0.04	0.00	32
(1.5)	0.8610	1.00	1.00	1.00	1.00	0.99	0.95	0.81	0.53	
	1.9297	1.00	1.00	1.00	1.00	1.00	0.95	0.53	0.07	37
(1.7)	0.8370	1.00	1.00	1.00	1.00	1.00	0.99	0.95	0.80	
	1.9446	1.00	1.00	1.00	1.00	1.00	1.00	0.95	0.57	41
(1.9)	0.8103	1.00	1.00	1.00	1.00	1.00	1.00	0.99	0.95	
	1.9562	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.95	45

* S. Size= 64 AMU=1.90 (i.e. p0= 0.0287) *

(B) Test	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma	
Crater.										
(0.5)	0.9049	0.95	0.87	0.71	0.47	0.21	0.06	0.01	0.00	
	1.5636	0.95	0.08	0.00	0.00	0.00	0.00	0.00	0.00	23
(0.7)	0.8883	0.99	0.95	0.86	0.67	0.40	0.15	0.03	0.00	
	1.5838	1.00	0.95	0.24	0.00	0.00	0.00	0.00	0.00	27
(0.9)	0.8696	1.00	0.99	0.95	0.85	0.63	0.33	0.10	0.02	
	1.6038	1.00	1.00	0.95	0.37	0.01	0.00	0.00	0.00	30

(1.1)	0.8479	1.00	1.00	0.99	0.95	0.87	0.58	0.37	0.07	
	1.8235	1.00	1.00	1.00	0.95	0.46	0.03	0.10	0.00	35
(1.3)	0.8234	1.00	1.00	1.00	0.99	0.95	0.22	0.34	0.23	
	1.8393	1.00	1.00	1.00	1.00	0.95	0.52	0.06	0.00	39
(1.5)	0.7990	1.00	1.00	1.00	1.00	0.99	0.94	0.75	0.48	
	1.6521	1.00	1.00	1.00	1.00	1.00	0.95	0.97	0.10	44
(1.7)	0.7663	1.00	1.00	1.00	1.00	1.00	0.99	0.95	0.80	
	1.6611	1.00	1.00	1.00	1.00	1.00	1.00	0.95	0.62	47
(1.9)	0.7348	1.00	1.00	1.00	1.00	1.00	1.00	0.99	0.95	
	1.6693	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.95	50

* S. Size= 64 AMU=1.60 (i.e. p0= 0.0548) *

(B) Test	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma	
Criter.										
(0.5)	0.8520	0.95	0.86	0.67	0.40	0.16	0.03	0.00	0.00	
	1.3000	0.95	0.11	0.00	0.00	0.00	0.00	0.00	0.00	30
(0.7)	0.8300	0.99	0.95	0.85	0.63	0.34	0.11	0.02	0.00	
	1.3181	1.00	0.95	0.29	0.00	0.00	0.00	0.00	0.00	34
(0.9)	0.8046	1.00	0.99	0.95	0.83	0.59	0.29	0.00	0.01	
	1.3331	1.00	1.00	0.95	0.43	0.02	0.00	0.00	0.00	37
(1.1)	0.7767	1.00	1.00	0.99	0.95	0.82	0.56	0.25	0.06	
	1.3463	1.00	1.00	1.00	0.95	0.52	0.06	0.00	0.00	42
(1.3)	0.7463	1.00	1.00	1.00	0.99	0.95	0.81	0.53	0.22	
	1.3569	1.00	1.00	1.00	1.00	0.95	0.59	0.12	0.01	45
(1.5)	0.7139	1.00	1.00	1.00	1.00	0.99	0.95	0.80	0.51	
	1.3657	1.00	1.00	1.00	1.00	1.00	0.95	0.64	0.18	49
(1.7)	0.6800	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
	1.3725	1.00	1.00	1.00	1.00	1.00	1.00	0.95	0.61	52
(1.9)	0.6454	1.00	1.00	1.00	1.00	1.00	1.00	0.99	0.95	
	1.3780	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.95	54

* S. Size= 64 AMU=1.30 (i.e. p0= 0.0968) *

(B) Test	B=0.5	B=0.7	B=0.9	B=1.1	B=1.3	B=1.5	B=1.7	B=1.9	Nsigma	
Criter.										
(0.5)	0.7802	0.95	0.85	0.64	0.35	0.12	0.02	0.00	0.00	
	0.9210	0.95	0.52	0.06	0.00	0.00	0.00	0.00	0.00	18
(0.7)	0.7517	0.99	0.95	0.84	0.60	0.31	0.09	0.01	0.00	
	0.9361	1.00	0.95	0.67	0.22	0.02	0.00	0.00	0.00	20
(0.9)	0.7204	1.00	0.99	0.95	0.83	0.58	0.27	0.07	0.01	
	0.9484	1.00	1.00	0.95	0.74	0.37	0.10	0.01	0.00	21
(1.1)	0.6872	1.00	1.00	0.99	0.95	0.79	0.49	0.19	0.04	
	0.9586	1.00	1.00	0.99	0.95	0.79	0.49	0.19	0.04	23
(1.3)	0.6524	1.00	1.00	1.00	0.99	0.95	0.81	0.54	0.23	
	0.9670	1.00	1.00	1.00	0.99	0.95	0.82	0.57	0.29	24
(1.5)	0.6167	1.00	1.00	1.00	1.00	0.99	0.95	0.81	0.53	
	0.9732	1.00	1.00	1.00	1.00	0.99	0.95	0.84	0.63	25
(1.7)	0.5809	1.00	1.00	1.00	1.00	1.00	0.99	0.95	0.81	
	0.9780	1.00	1.00	1.00	1.00	1.00	0.99	0.95	0.85	26
(1.9)	0.5456	1.00	1.00	1.00	1.00	1.00	1.00	0.99	0.95	
	0.9813	1.00	1.00	1.00	1.00	1.00	1.00	0.98	0.95	26

The following table is useful in giving the true changes in λ for the above tables :

		* Value of True $\lambda = B / B$							
		* =====							
		(B : is the planned value , and B is the True value)							
B :		0.5	0.7	0.9	1.1	1.3	1.5	1.7	1.9
* B	0.5 :	1	0.714	0.556	0.455	0.385	0.333	0.294	0.263
	0.7 :	1.400	1	0.778	0.636	0.538	0.467	0.412	0.368
	0.9 :	1.800	1.286	1	0.818	0.692	0.600	0.529	0.474
	1.1 :	2.200	1.571	1.222	1	0.846	0.733	0.647	0.579
	1.3 :	2.600	1.857	1.444	1.182	1	0.867	0.765	0.684
	1.5 :	3.000	2.143	1.667	1.364	1.154	1	0.882	0.789
	1.7 :	3.400	2.429	1.889	1.545	1.308	1.133	1	0.895
	1.9 :	3.800	2.714	2.111	1.727	1.462	1.267	1.118	1