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# Finite Element Simulation of Multiple Slip Effects on MHD Unsteady Maxwell Nanofluid Flow over a Permeable Stretching Sheet with Radiation and Thermo-Diffusion in the Presence of Chemical Reaction

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**Abstract:** The aim of the present study is to investigate the multiple slip effects on magnetohydrodynamic unsteady Maxwell nanofluid flow over a permeable stretching sheet with thermal radiation and thermo-diffusion in the presence of chemical reaction. The governing nonlinear partial differential equations are transformed into a system of coupled nonlinear ordinary differential equations with the aid of appropriate similarity variables, and the transformed equations are then solved numerically by using a variational finite element method. The effects of various physical parameters on the velocity, temperature, solutal concentration, and nanoparticle concentration profiles as well as on the skin friction coefficient, rate of heat transfer, and Sherwood number for solutal concentration are discussed by the aid of graphs and tables. An exact solution of flow velocity, skin friction coefficient, and Nusselt number is compared with the numerical solution obtained by FEM and also with numerical results available in the literature. A good agreement between the exact and numerical solution is observed. Also, to justify the convergence of the finite element numerical solution, the calculations are carried out by reducing the mesh size. The present investigation is relevant to high-temperature nanomaterial processing technology.

**Keywords:** MHD; finite element method; nanofluid; Maxwell fluid; thermo-diffusion; multiple slip

## 1. Introduction

The investigation of unsteady Maxwell nanofluid flow over a stretched surface has significantly expanded in recent decades due to several applications in engineering and physical processes. These include microelectromechanical systems (MEMS), advanced nuclear system, combustion chambers, nuclear plants, aircraft, nanoelectromechanical systems (NEMS), fuel cells, glass fiber, and paper production, which play an important role in our daily lives. Daily, several vehicles and devices generate a large quantity of energy, which influences the general activities of the vehicles and devices. Due to energy loss and the requirement to maintain the daily use of the appliance, we need a system which can achieve maximum productivity with minimum wasted expense. The concept of nanofluid (nanoparticles) was first introduced by Choi [1], to describe that base fluid (water, kerosene,

biofluids, and ethylene–glycol mixture) enhance thermal conductivity when nanoparticles are added. The thermal conductivity increases when nanoparticles are added, as described by the authors of [2–5]. Rashidi et al. [6] examined the Brownian and thermophoresis effects on the thermal boundary layer. Akbari et al. [7] examined the influence of nanoparticles on non-Newtonian nanofluids, and they described that the thermal conductivity enhances due to the increase in nanoparticle number. Similar nanoparticle behavior was examined by Mohyud-Din et al. [8] and Hayat et al. [9].

The investigation of nonlinear thermal radiative fluid flow is an area of interest for researchers because of its applications in many engineering processes. Especially, the thermal radiation impact assumes an essential job in controlling the heat transfer process in the polymer processing industry [10]. Raza et al. [11] investigated the entropy generation in the presence of nanoparticles and nonlinear thermal radiation. Mahanthesh et al. [12] investigated the nonlinear thermal radiation effects on magnetohydrodynamic Casson fluid flow. Ismail et al. [13] examined the nonlinear radiation effects on nanofluid slip flow in porous media. The study of nonlinear radiation heat transfer plays an important role in industrial applications at high temperature [14]. Slip condition on stretching surfaces is important in several manufacturing processes. It was found that when the flow pressure is low, the slip boundary condition is necessary. A slip condition on stretching or shrinking surfaces is used by several researchers [15–19]. Ramaya et al. [15] analyzed the nanofluids through a stretching sheet. They observed that the velocity of fluid increases when slip parameter values enhance and slip condition is helpful to control fluid velocity. Khalil et al. [20] conducted a numerical solution of magnetohydrodynamics Casson nanofluid flow. The effect of thermal radiation on the velocity and temperature of a stretching porous thin sheet was studied by Asmat et al. [21]. Chamkha et al. [22] carried out an investigation on heat and mass transfer in a porous medium with a chemical reaction. They obtained a similarity solution for unsteady flow.

The study of magnetohydrodynamics (MHD) with heat transfer flow over a permeable stretching or shrinking sheet is important in many manufacturing processes in the industry, such as in specific applications like polymer processing technology and laser devices used in medical treatment. Daniel et al. [23] studied the free or mixed convection magnetohydrodynamic flow over a sheet. They investigated the numerical solution of free convection and the effects of various physical parameters of interest using the homotopy analysis method. Dhanai et al. [24] conducted multiple solutions of magnetohydrodynamic heat transfer and boundary layer flow over a permeable sheet with viscous dissipation. Gireesha et al. [25] use a dusty fluid to check the flow and heat transfer of magnetohydrodynamic fluid. Haile et al. [26] studied the heat and mass transfer fluid flow in the presence of nanoparticles. They consider unsteady 2D flow and fluid passing along a vertical stretching sheet.

The boundary layer fluids flow caused by the stretching/shrinking surface is an important type of flow occurring in engineering and chemical industries flow processes. These include paper production, liquid metal, glass fiber, and polymer sheet synthesis. The manufacture of non-Newtonian fluids, including lubricants, physiological liquids, paints, colloidal liquids, biological liquids, biopolymers, and foodstuffs, plays an important role in our daily lives. Ashraf et al. [27] investigated the micropolar fluid flow toward a shrinking surface and also studied the radiation effects on thermal conductivity. Dhanai et al. [28] conducted multiple solutions of MHD heat transfer flow with viscous dissipation. The study of unsteady an axisymmetric flow and heat transfer of non-Newtonian fluid over a radially stretching sheet has considered by Shahzad et al. [29]. They also studied the radiation effects on the thermal boundary layer. Ashraf et al. [30] examined the magnetohydrodynamic flow and heat transfer in a micropolar fluid using the stretchable disk. They obtained the numerical solution of an axisymmetric flow over a stretchable disk. Azeem et al. [31] analyzed the heat transfer of an axisymmetric viscous fluid over a nonlinear radially stretching sheet.

The study of free convection or mixed convection flow is important in the electronics cooling process, heat exchangers, etc. Chen [32] examined the laminar mixed convection flow over a continuously stretching sheet. Many researchers engaged in analyzing the mixed convection flow of

non-Newtonian fluids [33–37]. Elahi et al. [38] described the numerical solution of mixed convection heat transfer over a stretching sheet. Hayat et al. [39] considered the magnetohydrodynamic flow of non-Newtonian nanofluid flow with the convective condition. They investigated the slip effects on MHD flow of non-Newtonian with a stretching surface. They also found radiation effects on velocity, temperature, and concentration profiles. Baag et al. [40] studied the stagnation point of a magnetohydrodynamic non-Newtonian fluid subject to the chemical reaction and heat source. Singh [41] examined the effects of viscous on free convection non-Newtonian fluid in the presence of chemical reaction. Mabood et al. [42] discussed steady non-Newtonian fluid with a chemical reaction through a porous medium. Hayat et al. [43] discussed a non-Newtonian fluid with chemical aspects and they investigated a numerical solution. Seth et al. [44] examined a chemically reacting nanofluid over a permeable vertical plate.

Motivated by the above literature and the range of applications discussed therein, the study of Unsteady Maxwell Nanofluid Flow and thermo-diffusion with regard to the multiple slips in the presence of chemical reactions has not been discussed before, to best of the authors' knowledge. The main aim of the present study was to extend the recently published work of Nayak et al. [45]. The governing nonlinear PDEs are transformed into a set of highly nonlinear ODEs with the aid of suitable similarity transformations, and the nonlinear coupled ODEs are solved numerically with the most popular FEM. The influences of the various physical parameters on the fluid velocity, temperature, and solutal and nanoparticle volume fraction functions are examined in detail for specific cases. An exact solution of flow velocity, skin friction coefficient, and Nusselt number is compared with the numerical solution obtained by FEM and also with numerical results available in the literature. Further, the convergence table of the finite element method is discussed with reference to different mesh sizes.

## 2. Mathematical Formulation

We consider the unsteady two-dimensional MHD flow of an electrically conducting incompressible viscous flow immersed in nanofluid with the presence of thermal radiation and first-order chemical reaction over a permeable stretching surface. The  $x$ -axis is chosen along with the sheet and the  $y$ -axis is taken normal to it, as shown in Figure 1. It is assumed that the sheet is moving with nonuniform velocity  $U(x, t) = ax/(1 - \lambda t)$ , chosen along the  $x$ -axis. Where  $a$  is the stretching rate of sheet and  $\lambda$  is the positive constant with the property  $\lambda t < 1$ . The magnetic field of strength  $B(x) = B_0 x^{-\frac{1}{2}}$  is assumed to be applied in normal direction with  $B_0 \neq 0$ . The magnetic Reynolds number  $Rex$  is taken to be very small for most of the fluids in industrial applications so that induced magnetic field is ignored. Let  $T_\infty, C_\infty, T_\infty$ , and  $\chi_\infty$  be the ambient temperature, ambient solutal concentration, and ambient nanoparticle concentration, respectively.  $T_w(x, t), C_w(x, t)$ , and  $\chi_w(x, t)$  are the temperature of the sheet, the concentration, and the nanoparticle volume fraction, respectively, at the surface.  $T_w(x, t), C_w(x, t)$  and  $\chi_w(x, t)$  are assumed to be of the following form (see the work by the authors of [46]).

$$\begin{aligned} T_w &= T_\infty + T_0 \left( \frac{ax}{2\nu(1-\lambda t)^2} \right) \\ C_w &= C_\infty + C_0 \left( \frac{ax}{2\nu(1-\lambda t)^2} \right) \\ \chi_w &= \chi_\infty + \chi_0 \left( \frac{ax}{2\nu(1-\lambda t)^2} \right) \end{aligned}$$

where  $T_0, C_0$ , and  $\chi_0$  are the reference temperature, reference solutal concentration, and reference nanoparticle concentration, respectively, such that  $0 \leq T_0 \leq T_w, 0 \leq C_0 \leq C_w$  and  $0 \leq \chi_0 \leq \chi_w$ . The above expressions are valid if  $(1 - \lambda t) > 0$ .

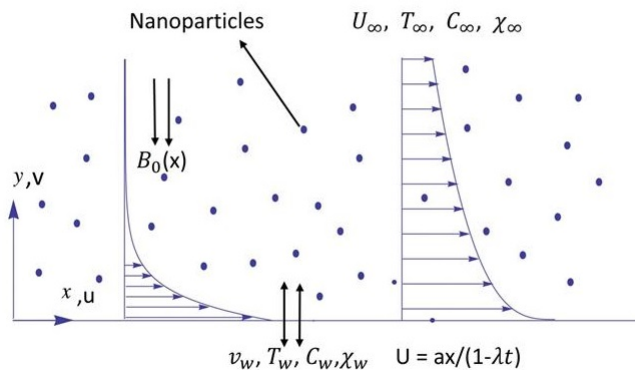


Figure 1. Physical configuration and coordinate system.

Under the above assumptions, the governing boundary layer equations for the flow problem are as follows (see the works by the authors of [9,19,37,46]).

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \tag{1}$$

$$\begin{aligned} \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = & \nu \frac{\partial^2 u}{\partial y^2} - k_0(u^2 \frac{\partial u^2}{\partial x^2} + v^2 \frac{\partial u^2}{\partial y^2} + 2uv \frac{\partial u^2}{\partial x \partial y}) \\ - \frac{\sigma B^2(x)u}{\rho} + g\beta_T(T - T_\infty) + g\beta_C(C - C_\infty) + g\beta_\chi(\chi - \chi_\infty) - \frac{\nu}{\kappa'}u \end{aligned} \tag{2}$$

$$\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \alpha \left( 1 + \frac{16T_\infty^3 \sigma^*}{3k^* \kappa} \right) \frac{\partial^2 T}{\partial y^2} + \tau D_B \frac{\partial \chi}{\partial y} \frac{\partial T}{\partial y} + \tau \frac{D_T}{T_\infty} \left( \frac{\partial T}{\partial y} \right)^2 + D_{TC} \frac{\partial C^2}{\partial y} \tag{3}$$

$$\frac{\partial C}{\partial t} + u \frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} = D_S \frac{\partial^2 C}{\partial y^2} - k_1(C - C_\infty) + D_{CT} \frac{\partial^2 T}{\partial y^2} \tag{4}$$

$$\frac{\partial \chi}{\partial t} + u \frac{\partial \chi}{\partial x} + v \frac{\partial \chi}{\partial y} = D_B \frac{\partial^2 \chi}{\partial y^2} + \frac{D_T}{T_\infty} \frac{\partial^2 T}{\partial y^2} \tag{5}$$

and the boundary conditions are (see the works by the authors of [46,47])

$$\begin{aligned} u = U(x, t) + U_{slip}, v = v_w, T = T_w(x, t) + T_{slip}, C = C_w(x, t) + C_{slip}, \\ \chi = \chi_w(x, t) + \chi_{slip} \text{ at } y = 0 \end{aligned} \tag{6}$$

$$u \rightarrow 0, T \rightarrow T_\infty, C \rightarrow C_\infty, \chi \rightarrow \chi_\infty, \text{ as } y \rightarrow \infty, \tag{7}$$

where  $u$  and  $v$  are the velocity components along  $x$  and  $y$ , respectively;  $\alpha, \nu, \sigma$ , and  $\rho$  are the thermal diffusivity, kinetic viscosity, electrical conductivity, and density of fluid, respectively;  $g$  is the acceleration due to gravity;  $\beta_T$  is thermal expansion coefficient;  $\beta_C$  is the solutal concentration expansion coefficient;  $\beta_\chi$  is the nanoparticle concentration expansion coefficient;  $T$  is the temperature;  $C$  is the solutal concentration;  $\chi$  is the nanoparticle concentration;  $D_M$  is the molecular diffusivity;  $D_T$  is the thermal diffusivity;  $D_B$  is the Brownian diffusivity;  $\sigma^*$  is the Stefan-Boltzmann constant;  $k^*$  is the mean absorption coefficient;  $D_{CT}$  and  $D_{TC}$  are the Soret and Dufour diffusivity, respectively; and  $k_1$  is the chemical reaction.

In order to solve Equations (1)–(5), we introduce the following similarity transformations (see the works by the authors of [19,46]).

$$\begin{aligned}\eta &= \sqrt{\frac{a}{v(1-\lambda t)}}y, & \psi &= \sqrt{\frac{av}{(1-\lambda t)}}xf(\eta), & \theta(\eta) &= \frac{T-T_\infty}{T_w-T_\infty}, \\ \phi(\eta) &= \frac{C-C_\infty}{C_w-C_\infty}, & \gamma(\eta) &= \frac{\chi-\chi_\infty}{\chi_w-\chi_\infty}\end{aligned}\quad (8)$$

In view of the similarity transformation in Equation (8), the partial nonlinear differential equations, Equations (1)–(5), transform into the following system of nonlinear ODEs,

$$f''' + ff'' - f'^2 - \sigma\left(\frac{\eta}{2}f'' + f'\right) - Mf' - \beta(f^2f''' - 2ff'f'') + \lambda_1\theta + \lambda_2\phi + \lambda_3\gamma - k_p f' = 0, \quad (9)$$

$$(1+R)\frac{1}{Pr}\theta'' - f'\theta + f\theta' - \sigma\left(\frac{\eta}{2}\theta' + 2\theta\right) + Nb\gamma'\theta' + Nt\theta'^2 + Nd\phi'' = 0 \quad (10)$$

$$\frac{1}{Sc}\phi'' - f'\phi + f\phi' - \sigma\left(\frac{\eta}{2}\phi' + 2S\right) + Sr\theta'' - kc\phi = 0 \quad (11)$$

$$\gamma'' - Ln\left[f'\gamma - f\gamma' + \sigma\left(\frac{\eta}{2}\gamma' + 2\gamma\right)\right] + \frac{Nt}{Nb}\theta'' = 0 \quad (12)$$

and the transformed boundary conditions, Equations (6) and (7), are

$$\begin{aligned}f(0) = f_w, f'(0) = 1 + S_f f''(0), \theta(0) = 1 + S_\theta \theta'(0), \phi(0) = 1 + S_\phi \phi'(0), \\ \gamma(0) = 1 + S_\gamma \gamma'(0),\end{aligned}\quad (13)$$

$$f'(\infty) \rightarrow 0, \theta(\infty) \rightarrow 0, \phi(\infty) \rightarrow 0, \gamma(\infty) \rightarrow 0, \quad (14)$$

The primes shows the differentiation with respect to  $\eta$ . The parameters in Equations (9)–(12) are defined as

$$\begin{aligned}M &= \sqrt{\frac{\sigma(1-\lambda t)}{\rho a}}B_0, Pr = \frac{\nu}{\alpha}, Nb = \frac{\tau D_B(\chi_w - \chi_\infty)}{\nu}, Nt = \frac{\tau D_T(T_w - T_\infty)}{\nu T_\infty}, \beta = \frac{k_0 a}{1-\lambda t}, Sc = \frac{\nu}{D_S}, Ln = \frac{\sigma}{D_B}, \\ R &= \frac{16\sigma^* T_\infty^3}{3k^* K}, \sigma = \frac{\lambda}{a}, \lambda_1 = \frac{g\beta_T T_0}{2av}, \lambda_2 = \frac{g\beta_C C_0}{2av}, \lambda_3 = \frac{g\beta_\chi \chi_0}{2av}, Sr = \frac{D_{CT} T_0}{\nu C_0}, Nd = \frac{D_{TC} C_0}{\nu T_0}, kc = \frac{k_1(1-\lambda t)}{a}, \\ k_p &= \frac{\nu(1-\lambda t)}{a}, f_w = -v_w\left(\sqrt{\frac{(1-\lambda t)}{\nu a}}\right),\end{aligned}$$

where  $\sigma$  is the unsteadiness parameter;  $M$  is the magnetic field parameter;  $Pr$  is the Prandtl number;  $Nb$  is the Brownian motion parameter;  $Nt$  is the thermophoresis parameter;  $\beta$  is the Deborah number;  $Sc$  is the Schmidt number;  $Ln$  is the Lewis number;  $R$  is the thermal radiation parameter;  $\lambda_1, \lambda_2$ , and  $\lambda_3$  are the buoyancy parameters;  $k_p$  is the permeability parameter;  $k_c$  is the chemical reaction parameter;  $Nd$  is the Dufour parameter;  $Sr$  is the Soret parameter; and  $f_w$  is the Suction/injection parameter.

### 3. Finite Element Method Solutions

Equations (9)–(12) under the boundary conditions (13)–(14) have been solved numerically using the finite element method (FEM). The FEM has been applied to study different problems in computational fluid dynamic and extremely efficient method to solve different nonlinear problems [48–50]. Reddy [51] described an excellent general detail of variational finite element method. It has been found that the finite element method is exclusively employed in commercial software like ADINA, ANSYS, MATLAB, and ABAQUS. Swapna et al. and Rana et al. [52,53] described that variational finite element method solves boundary value problem very effectively, quickly, and accurately. We employ the finite element method to the solve nonlinear differential equations, Equations (9)–(12), with the boundary conditions (13)–(14), first we consider

$$f' = h. \quad (15)$$

The Equations (9)–(12) thus reduce to

$$h'' + fh' - h^2 - \sigma\left(\frac{\eta}{2}h' + f\right) - Mh + \lambda_1\theta + \lambda_2\phi + \lambda_3\gamma - \beta(f^2h'' - 2fhh') - k_ph = 0, \tag{16}$$

$$(1 + R)\frac{1}{Pr}\theta'' - h\theta + f\theta' - \sigma\left(\frac{\eta}{2}\theta' + 2\theta\right) + Nb\gamma'\theta' + Nt\theta'^2 + Nd\phi'' = 0, \tag{17}$$

$$\frac{1}{Sc}\phi'' - f'\phi + f\phi' - \sigma\left(\frac{\eta}{2}\phi' + 2\phi\right) + S_r\theta'' - kc\phi = 0, \tag{18}$$

$$\gamma'' - Ln\left[h\gamma - f\gamma' + \sigma\left(\frac{\eta}{2}\gamma' + 2\gamma\right)\right] + \frac{Nt}{Nb}\theta'' = 0, \tag{19}$$

The corresponding boundary conditions reduce to the following form,

$$f(0) = f_w, h(0) = 1 + S_f h'(0), \theta(0) = 1 + S_\theta \theta'(0), \phi(0) = 1 + S_\phi \phi'(0), \tag{20}$$

$$\gamma(0) = 1 + S_\gamma \gamma'(0), \tag{20}$$

$$h(\infty) \rightarrow 0, \theta(\infty) \rightarrow 0, S(\infty) \rightarrow 0, \gamma(\infty) \rightarrow 0, \tag{21}$$

### 3.1. Variational Formulations

The variational form associated with Equations (15)–(19) over a linear element  $\Omega_a = (\eta_a, \eta_{a+1})$  is given by

$$\int_{\eta_a}^{\eta_{a+1}} s_1 \{f' - h\} d\eta = 0, \tag{22}$$

$$\int_{\eta_a}^{\eta_{a+1}} s_2 \{h'' + fh' - h^2 - \sigma\left(\frac{\eta}{2}h' + f\right) - Mh + \lambda_1\theta + \lambda_2\phi + \lambda_3\gamma - \beta(f^2h'' - 2fhh') - k_ph\} d\eta = 0, \tag{23}$$

$$\int_{\eta_a}^{\eta_{a+1}} s_3 \left\{ (1 + R)\frac{1}{Pr}\theta'' - h\theta + f\theta' - A\left(\frac{\eta}{2}\theta' + 2\theta\right) + Nb\gamma'\theta' + Nt\theta'^2 + Nd\phi'' \right\} d\eta = 0, \tag{24}$$

$$\int_{\eta_a}^{\eta_{a+1}} s_4 \left\{ \frac{1}{Sc}\phi'' - h\phi + f\phi' - A\left(\frac{\eta}{2}\phi' + 2\phi\right) + S_r\theta'' - kc\phi \right\} d\eta = 0, \tag{25}$$

$$\int_{\eta_a}^{\eta_{a+1}} s_5 \left\{ \gamma'' - Ln\left[h\gamma - f\gamma' + A\left(\frac{\eta}{2}\gamma' + 2\gamma\right)\right] + \frac{Nt}{Nb}\theta'' \right\} d\eta = 0, \tag{26}$$

where  $s_1, s_2, s_3, s_4$  and  $s_5$  are arbitrary shape function or trial functions.

### 3.2. Finite Element Formulations

The equation of finite element model is obtained by replacing finite element approximation of the following form in Equations (22)–(26).

$$\bar{f} = \sum_{j=1}^3 \bar{f}_j \psi_j, \bar{h} = \sum_{j=1}^3 \bar{h}_j \psi_j, \bar{\theta}' = \sum_{j=1}^3 \bar{\theta}'_j \psi_j, \bar{\phi}' = \sum_{j=1}^3 \bar{\phi}'_j \psi_j, \tag{27}$$

with  $s_1 = s_2 = s_3 = s_4 = s_5 = \psi_i (i = 1, 2, 3)$ , where the shape function,  $\psi_i$ , for a line element,  $\Omega_e = (\eta_a, \eta_{a+1})$ , is given by

$$\psi_1 = \frac{(\eta_{a+1} - \eta_a - 2\eta)(\eta_{a+1} - \eta)}{(\eta_{a+1} - \eta_a)^2}, \psi_2 = \frac{4(\eta - \eta_a)(\eta_{a+1} - \eta)}{(\eta_{a+1} - \eta_a)^2}, \psi_3 = -\frac{(\eta_{a+1} - \eta_a - 2\eta)(\eta - \eta_a)}{(\eta_{a+1} - \eta_a)^2}, \eta_a \leq \eta \leq \eta_{a+1}. \tag{28}$$

The FE model equations are, therefore, given by

$$\begin{bmatrix} W^{11} & W^{12} & W^{13} & W^{14} & W^{15} \\ W^{21} & W^{22} & W^{23} & W^{24} & W^{25} \\ W^{31} & W^{32} & W^{33} & W^{34} & W^{35} \\ W^{41} & W^{42} & W^{43} & W^{44} & W^{45} \\ W^{51} & W^{52} & W^{53} & W^{54} & W^{55} \end{bmatrix} \begin{bmatrix} f \\ h \\ \theta \\ \phi \\ \gamma \end{bmatrix} = \begin{bmatrix} b_1 \\ b_2 \\ b_3 \\ b_4 \\ b_5 \end{bmatrix} \tag{29}$$

where  $W_{mn}$  and  $b_m$  ( $m, n = 1, 2, 3, 4, 5$ ) are defined as

$$\begin{aligned} W_{ij}^{11} &= \int_{\eta_a}^{\eta_{a+1}} \psi_i \frac{d\psi_j}{d\eta} d\eta, W_{ij}^{12} = - \int_{\eta_a}^{\eta_{a+1}} \psi_i \psi_j d\eta, W_{ij}^{13} = W_{ij}^{14} = 0, W_{ij}^{15} = W_{ij}^{21} = 0, \\ W_{ij}^{22} &= - \int_{\eta_a}^{\eta_{a+1}} \frac{d\psi_i}{d\eta} \frac{d\psi_j}{d\eta} d\eta + \int_{\eta_a}^{\eta_{a+1}} \bar{f} \psi_i \frac{d\psi_j}{d\eta} d\eta - \int_{\eta_a}^{\eta_{a+1}} \bar{h} \psi_i \psi_j d\eta - A \frac{\eta}{2} \int_{\eta_a}^{\eta_{a+1}} \psi_i \frac{d\psi_j}{d\eta} d\eta \\ &- \beta \int_{\eta_a}^{\eta_{a+1}} \bar{f} \bar{f} \frac{d\psi_i}{d\eta} \frac{d\psi_j}{d\eta} d\eta + 2\beta \int_{\eta_a}^{\eta_{a+1}} \bar{f} \bar{h} \psi_i \frac{d\psi_j}{d\eta} d\eta - \int_{\eta_a}^{\eta_{a+1}} \bar{h} \psi_i \psi_j d\eta \\ &- A \int_{\eta_a}^{\eta_{a+1}} \psi_i \psi_j d\eta - M \int_{\eta_a}^{\eta_{a+1}} \psi_i \psi_j d\eta + k_p \int_{\eta_a}^{\eta_{a+1}} \psi_i \psi_j d\eta \\ W_{ij}^{23} &= \lambda_1 \int_{\eta_a}^{\eta_{a+1}} \psi_i \psi_j d\eta, W_{ij}^{24} = \lambda_2 \int_{\eta_a}^{\eta_{a+1}} \psi_i \psi_j d\eta, W_{ij}^{25} = \lambda_3 \int_{\eta_a}^{\eta_{a+1}} \psi_i \psi_j d\eta, \end{aligned}$$

$$\begin{aligned} W_{ij}^{31} &= 0, W_{ij}^{32} = 0, \\ W_{ij}^{33} &= -(1+R) \frac{1}{Pr} \int_{\eta_a}^{\eta_{a+1}} \frac{d\psi_i}{d\eta} \frac{d\psi_j}{d\eta} d\eta - \int_{\eta_a}^{\eta_{a+1}} \bar{h} \psi_i \psi_j d\eta + \int_{\eta_a}^{\eta_{a+1}} \bar{f} \psi_i \frac{d\psi_j}{d\eta} d\eta \\ &- A \frac{\eta}{2} \int_{\eta_a}^{\eta_{a+1}} \psi_i \frac{d\psi_j}{d\eta} d\eta - 2A \int_{\eta_a}^{\eta_{a+1}} \psi_i \psi_j d\eta + Nb \int_{\eta_a}^{\eta_{a+1}} \bar{\gamma}' \psi_i \frac{d\psi_j}{d\eta} d\eta \\ &+ Nt \int_{\eta_a}^{\eta_{a+1}} \bar{\theta}' \psi_i \frac{d\psi_j}{d\eta} d\eta, W_{ij}^{34} = -Nd \int_{\eta_a}^{\eta_{a+1}} \frac{d\psi_i}{d\eta} \frac{d\psi_j}{d\eta} d\eta, W_{ij}^{35} = 0, W_{ij}^{41} = W_{ij}^{42} = 0, \end{aligned}$$

$$\begin{aligned} W_{ij}^{43} &= -Sr \int_{\eta_a}^{\eta_{a+1}} \frac{d\psi_i}{d\eta} \frac{d\psi_j}{d\eta} d\eta, \\ W_{ij}^{44} &= -\frac{1}{Sc} \int_{\eta_a}^{\eta_{a+1}} \frac{d\psi_i}{d\eta} \frac{d\psi_j}{d\eta} d\eta + \int_{\eta_a}^{\eta_{a+1}} \bar{f} \psi_i \frac{d\psi_j}{d\eta} d\eta - \int_{\eta_a}^{\eta_{a+1}} \bar{h} \psi_i \psi_j d\eta d\eta \\ &- A \frac{\eta}{2} \int_{\eta_a}^{\eta_{a+1}} \psi_i \frac{d\psi_j}{d\eta} d\eta - 2A \int_{\eta_a}^{\eta_{a+1}} \psi_i \psi_j d\eta - k_c \int_{\eta_a}^{\eta_{a+1}} \psi_i \psi_j d\eta, \\ W_{ij}^{45} &= W_{ij}^{51} = W_{ij}^{52} = W_{ij}^{54} = 0, W_{ij}^{53} = -\frac{Nt}{Nb} \int_{\eta_a}^{\eta_{a+1}} \frac{d\psi_i}{d\eta} \frac{d\psi_j}{d\eta} d\eta \end{aligned}$$

$$\begin{aligned} W_{ij}^{55} &= - \int_{\eta_a}^{\eta_{a+1}} \frac{d\psi_i}{d\eta} \frac{d\psi_j}{d\eta} d\eta + Ln \int_{\eta_a}^{\eta_{a+1}} \bar{f} \psi_i \frac{d\psi_j}{d\eta} d\eta - Ln \int_{\eta_a}^{\eta_{a+1}} \bar{h} \psi_i \psi_j d\eta d\eta \\ &- LnA \frac{\eta}{2} \int_{\eta_a}^{\eta_{a+1}} \psi_i \frac{d\psi_j}{d\eta} d\eta - 2LnA \int_{\eta_a}^{\eta_{a+1}} \psi_i \psi_j d\eta, \end{aligned} \quad (30)$$

and

$$\begin{aligned} b_i^1 &= 0, b_i^2 = -(\psi \frac{dh}{d\eta})_{\eta_a}^{\eta_{a+1}}, b_i^3 = -(1+R) \frac{1}{Pr} (\psi \frac{d\theta}{d\eta})_{\eta_a}^{\eta_{a+1}} - Nd (\psi \frac{d\phi}{d\eta})_{\eta_a}^{\eta_{a+1}}, \\ b_i^4 &= -\frac{1}{Sc} (\psi \frac{d\phi}{d\eta})_{\eta_a}^{\eta_{a+1}} - Sr (\psi \frac{d\theta}{d\eta})_{\eta_a}^{\eta_{a+1}}, \\ b_i^5 &= -(\psi \frac{d\gamma}{d\eta})_{\eta_a}^{\eta_{a+1}} - \frac{Nt}{Nb} (\psi \frac{d\theta}{d\eta})_{\eta_a}^{\eta_{a+1}}, \end{aligned} \quad (31)$$

where  $\bar{f} = \sum_{j=1}^3 \bar{f}_j \psi_j$ ,  $\bar{h} = \sum_{j=1}^3 \bar{h}_j \psi_j$ ,  $\bar{\theta}' = \sum_{j=1}^3 \bar{\theta}'_j \psi_j$  and  $\bar{\phi}' = \sum_{j=1}^3 \bar{\phi}'_j \psi_j$  are supposed to be known. After the assembly of the element Equation (30), the obtained equations are nonlinear, along these lines this requires the utilization of an iterative plan for an effective solution. The functions  $\bar{f}$ ,  $\bar{h}$ ,  $\bar{\theta}'$ , and  $\bar{\phi}'$  are assumed to be known at a lower iteration level to linearize the system and the Gaussian quadrature

technique is used to solve the integral. The computations for functions velocity, temperature, solutal and nanofluid volume fraction profile are then completed for higher level, continued until the desired precision of 0.00005 is obtained. The whole algorithm is executed in MATLAB software. To ensure mesh independence, a mesh affectability practice has been performed. No significant variation in the results is noticed for  $\eta > 10$ . Therefore,  $\eta$  has been fixed at 10. To check the convergence of the results, we calculated the number of elements that increased at  $n = 300, 600, 900, 1200, 1500, 1800,$  and  $2100$ . The outcomes are delineated in Table 1. It is observed that as  $n$  increases beyond 1800, no significant change in the values of velocity, temperature, solutal, and nanoparticles concentration functions is revealed; in this manner, the last outcomes are reported for  $n = 1800$  elements.

**Table 1.** Convergence results of the finite element method (FEM) ( $Pr = 1, M = \sigma = \beta = 0.2, \lambda_1 = \lambda_2 = \lambda_3 = 0.2, S_f = S_\theta = S_\phi = S_\gamma = 0.5, f_w = Sr = R = 0.5, k_p = k_c = Nd = Nt = Nb = 0.1, Sc = 10, Ln = 5$ ).

Number of Elements	$h(3)$	$\theta(3)$	$\phi(3)$	$\gamma(3)$
300	0.12365	0.18517	0.06336	0.02773
600	0.12390	0.18506	0.06332	0.02772
900	0.12399	0.18503	0.06331	0.02771
1200	0.12403	0.18501	0.06330	0.02770
1500	0.12406	0.18500	0.06330	0.02770
1800	0.12408	0.18499	0.06330	0.02770
2100	0.12409	0.18499	0.06330	0.02770

The precise of the existing results, a comparison of the flow velocity is made with the exact solution given by Crane [54] as  $f(\eta) = 1 - \exp(-\eta)$ , under the special case ( $M = 0, \sigma = 0, \beta = 0, \lambda_1 = 0, \lambda_2 = 0, \lambda_3 = 0, S_f = 0, f_w = 0, kp = 0$ ). The FEM results are a decent concurrence with the exact solution which affirms the validity of FEM. It is clearly seen in Table 2.

**Table 2.** Comparison of the exact solution of Crane [54] and FEM for the flow velocity  $f'(\eta)$ .

$\eta$	Crane [54]	FEM	Error in %	$\eta$	Crane [54]	FEM	Error in %
	(a) Exact Solution	(b) (Our Results)	$ \left(\frac{b-a}{a}\right)  \times 100$		(a) Exact Solution	(b) (Our Results)	$ \left(\frac{b-a}{a}\right)  \times 100$
0	1.0000	1.00000	0.00000	5	0.0067	0.00670	0.00000
1	0.1379	0.13786	0.02901	6	0.0025	0.00251	0.40000
2	0.1353	0.13531	0.00739	7	0.0009	0.00091	1.11111
3	0.0498	0.04978	0.04016	8	0.0003	0.00033	3.33333
4	0.0183	0.01831	0.05464	9	0.0001	0.00011	10.0000

#### 4. Results and Discussion

Computations have been performed for quantities of interest like velocity, temperature, and solutal and nanofluid volume fraction for various values of physical parameters. In Table 3, the skin friction coefficient  $-f''(0)$  obtained by FEM is compared with the numerical results of Gireesha et al. [25] and the exact solution of Mudassar et al. [55], under special case ( $\sigma = 0, \beta = 0, \lambda_1 = 0, \lambda_2 = 0, \lambda_3 = 0, S_f = 0, f_w = 0, kp = 0$ ). An excellent correlation has been achieved and grid invariance test has been conducted to maintain 4 decimal point accuracy. To ensure the accuracy of the existing numerical results, the skin friction coefficient  $-f''(0)$  for steady and unsteady flow obtained by the finite element. We have seen an excellent agreement between our solution and that of the already published research articles; this confirms the validity and accuracy of the present results (see Table 4).



**Table 3.** Comparison of skin friction coefficient for various values of M.

M	Gireesha et al. [25] $\beta = 0$	Mudassar et al. [55] (a) Exact Dolution	FEM (b) (Our Results)	Error in % $ (\frac{b-a}{a})  \times 100$
0.0	1.000	1.000000	1.0000080	0.00080
0.2	1.095	1.095445	1.0954458	0.00007
0.5	1.224	1.224745	1.2247446	0.00003
1.0	1.414	1.414214	1.4142132	0.00006
1.2	1.483	1.483240	1.4832393	0.00005
1.5	1.581	1.581139	1.5811384	0.00004
2.0	1.732	1.732051	1.7320504	0.00003

**Table 4.** Comparison of  $-f''(0)$  for various values of M and  $\sigma$  ( $f_w = \lambda_1 = \lambda_2 = \lambda_3 = k_p = S_f = 0$ );).

M	[56]	[46]	FEM (Present)	$\sigma$	[22]	[46]	FEM (Present)
0	-1.000008	-1.0000084	-1.0000082	0.2	-	-	1.068027
1	1.4142135	1.41421356	1.41421353	0.4	-	-	1.134687
5	2.4494897	2.44948974	2.44948963	0.6	-	-	1.199118
10	3.3166247	3.31662479	3.31662463	0.8	1.261512	1.261042	1.261042
50	7.1414284	7.14142843	7.14142839	1.0	-	-	1.320522
100	10.049875	10.0498756	10.0498751	1.2	1.378052	1.377724	1.377724
500	22.383029	22.3830293	22.3830283	1.4	-	-	1.432836
1000	31.638584	31.6385840	31.6385833	1.6	-	-	1.486039

Table 5 depicts the results of heat transfer rate obtained by FEM compared with the results of pervious studies and exact solution of Ishak et al. [57] under special case ( $Nt = Nb = 0$ ). We noticed that our numerical results are in complete agreement and that the grid invariance test has been conducted to maintain 4 decimal point accuracy. In Table 6, the local skin friction coefficient  $-f''(0)$ , the rates of heat transfer  $-\theta'(0)$  and mass transfer  $-\phi'(0)$  at the surface obtained by FEM is also compared with the already publish research work. A good correlation has been achieved.

**Table 5.** Comparison of  $-\theta'(0)$  for various values of Pr ( $M = f_w = S_\theta = \sigma = \lambda_1 = \lambda_2 = \lambda_3 = R = Nd = k_p = S_f = 0$ );).

Pr	Aii [58]	Fazle et al. [46]	Ishak et al. [57]	Dulal Pal. [10]	Haile et al. [26]	Ishak et al. [57] (a) Exact solution	FEM (b) (Our results)	Error in % $ (\frac{b-a}{a})  \times 100$
0.72	0.8058	0.8088	-	-	-	0.8086313498	0.8086339299	0.0003
1.00	0.9691	1.0000	1.0000	1.0000	1.0004	1.0000000000	1.0000080213	0.0008
3.00	1.9144	1.9237	1.9237	1.9236	1.9234	1.923682594	1.9236777221	0.0003
10.0	3.7006	3.7207	3.7207	3.7207	3.7205	3.720673901	3.7206681683	0.0002
100	-	-	12.2941	12.2940	12.2962	12.294083260	12.294051659	0.0003

**Table 6.** Comparison of  $-f''(0)$ ,  $-\theta'(0)$ , and  $-\phi'(0)$  for various values of Pr and Sc ( $M = \sigma = \lambda_3 = \beta = R = Nb = Nt = Nd = Sr = 0, f_w = 0.5, \lambda_1 = k_p = k_c = 1, \lambda_2 = 2, S_f = S_\theta = S_\phi = S_\gamma = 0$ ).

Pr	Sc	Chamkha et al. [22]			FEM (Our Results)		
		$-f''(0)$ ,	$-\theta'(0)$ ,	$-\phi'(0)$	$-f''(0)$	$-\theta'(0)$	$-\phi'(0)$
0.71	0.22	0.27377	1.158393	0.740140	0.27371	1.158389	0.740160
	0.60	0.49677	1.101087	1.312248	0.49669	1.101082	1.312192
	0.94	0.59941	1.076931	1.713443	0.59935	1.076899	1.713358
0.3	0.62	0.38639	0.621980	1.355045	0.38655	0.621892	1.355036
0.71		0.50438	1.099032	1.337571	0.50429	1.099018	1.337267
1.0		0.55244	1.384875	1.331027	0.55237	1.384753	1.331856
3.0		0.69042	2.966999	1.316710	0.69036	2.966894	1.316382

Figure 2 shows the effect of  $M$  on the velocity function with no hydrodynamic slip (Figure 2a) and with hydrodynamic slip (Figure 2b). The results show that the velocity component decreases with the increment of  $M$  in both cases. Physically, the  $M$  produced Lorentz force slowed the motion of the fluid. However, the presence of the hydrodynamic slip, as shown in Figure 2b, decreases the velocity boundary layer. Figure 2 also shows that suction,  $f_w$ , causes a reduction in the momentum boundary layer thickness, and thus it provides control over this momentum boundary layer thickness.

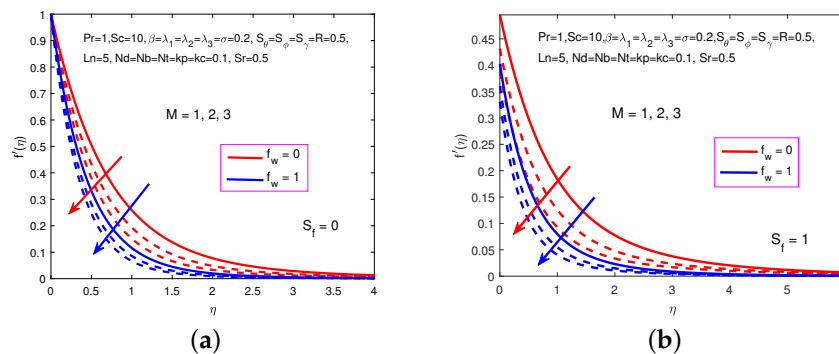


Figure 2. Influence of  $M$  and  $f_w$  on  $f'$ . (a) No hydrodynamic slip. (b) With hydrodynamic slip.

Figures 3 and 4 illustrate that the velocity increases with the increment in values of the buoyancy parameters in presence of no hydrodynamic slip (Figures 3 and 4a) and hydrodynamic slip (Figures 3 and 4b). Expanding the estimations of the buoyancy parameters leads to growth of the velocity profile. Physically, the buoyancy supporting forces are strengthened with these increments in buoyancy parameters. We additionally see in Figure 3 that the velocity profile declines reciprocally to as the unsteadiness parameter. It is noticed that the increment in radiation parameter  $R$  causes the profile of velocity to enhance. Also increment in hydrodynamic slip causes the profile of the velocity to decrease (Figures 3 and 4b).

A similar behavior of nanoparticle concentration is noticed for buoyancy parameter buoyancy parameter ( $\lambda_3$ ), unsteadiness parameter, and hydrodynamic slip is observed in Figure 5. The influence of varying the permeability parameter  $k_p$  on the velocity profile is depicted in Figure 6. We observe in Figure 6 that, as the permeability  $k_p$  increases, it causes a decrease in the velocity profile. However, the presence of the hydrodynamic slip, as noticed from Figure 6b decreases the velocity boundary layer. We also observe in Figure 6 that suction reduce the momentum boundary layer thickness. A similar behaviour of Deborah number,  $\beta$ , is observed in the velocity profile, as in Figure 7.

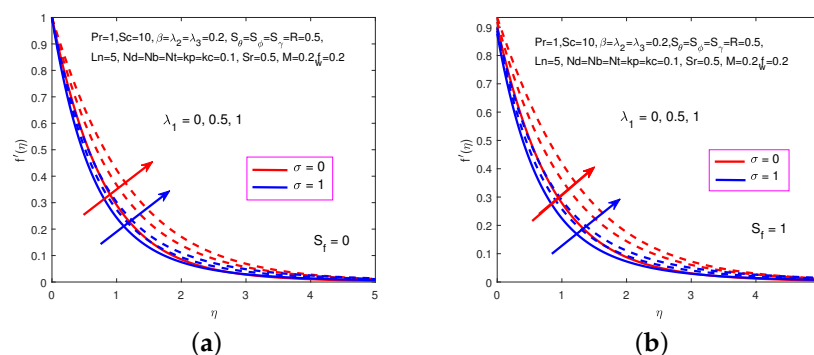


Figure 3. Influence of  $\lambda_1$  and  $\sigma$  on  $f'$ . (a) No hydrodynamic slip. (b) With hydrodynamic slip.

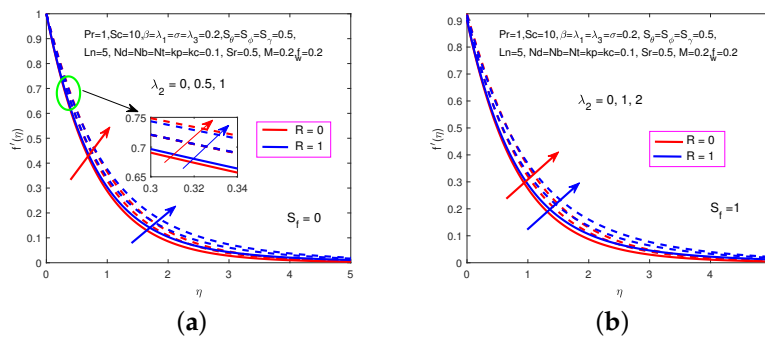


Figure 4. Influence of  $\lambda_2$  and  $R$  on  $f'$ . (a) No hydrodynamic slip. (b) With hydrodynamic slip.

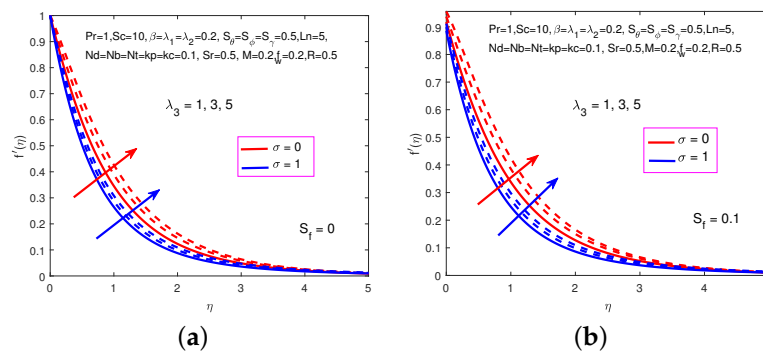


Figure 5. Influence of  $\lambda_3$  and  $\sigma$  on  $f'$ . (a) No hydrodynamic slip. (b) With hydrodynamic slip.

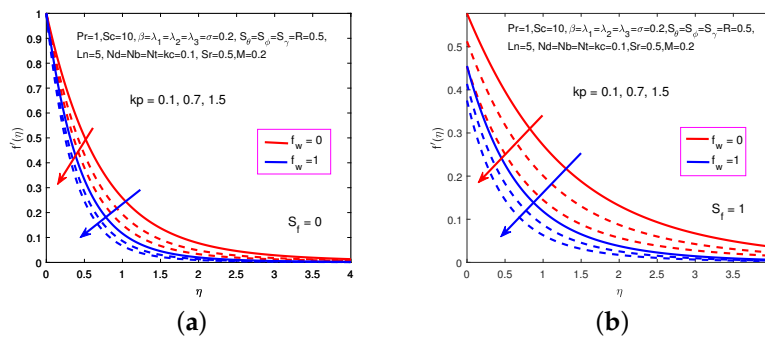


Figure 6. Influence of  $kp$  and  $f_w$  on  $f'$ . (a) No hydrodynamic slip. (b) With hydrodynamic slip.

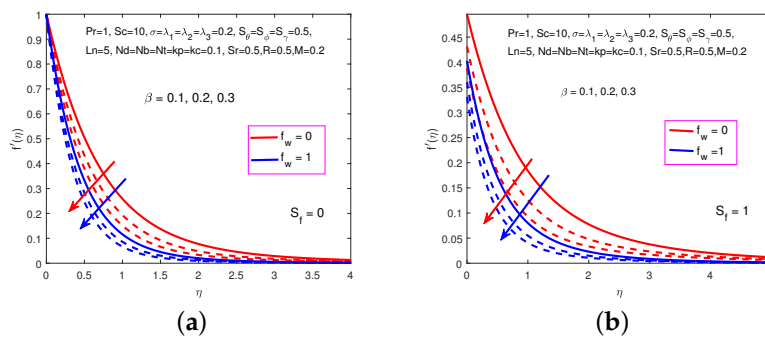


Figure 7. Influence of  $\beta$  and  $f_w$  on  $f'$ . (a) No hydrodynamic slip. (b) With hydrodynamic slip.

Figure 8 demonstrates the influence of  $M$  on the temperature profile with no thermal slip (Figure 8a) and thermal slip (Figure 8b). The figure shows that the temperature profile increases

with the increase of  $M$ . Physically, applying the magnetic field warms up the liquid and in this way diminishes the warmth and mass exchange rates from the boundary causing increments in liquid temperature. Figure 8a,b also demonstrates that suction,  $f_w$ , and thermal slip decrease the thermal boundary layer thickness. A similar behaviour of Brownian motion is observed on temperature profile as in Figure 9. Brownian motion will be more prominent and  $Nb$  will have large values for small size nanoparticles. Consequently, we see that temperatures are upgraded with higher  $Nb$  values.

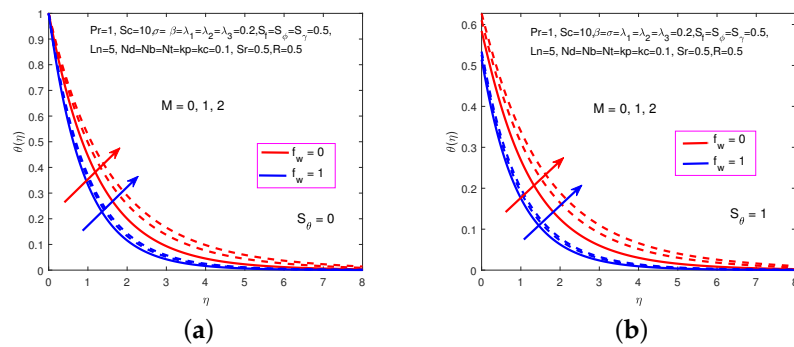


Figure 8. Influence of  $M$  and  $f_w$  on  $\theta$ . (a) No thermal slip. (b) With thermal slip.

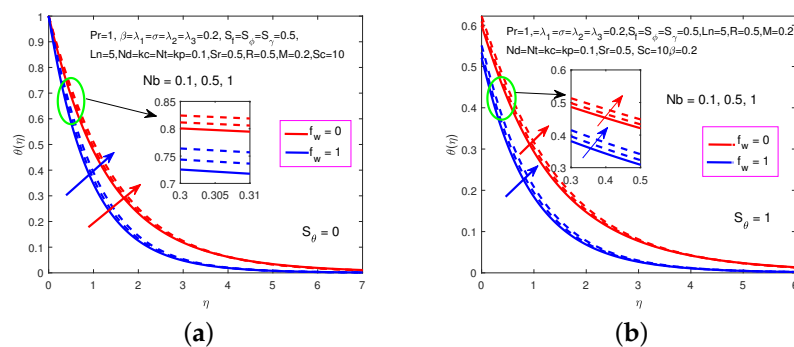


Figure 9. Influence of  $Nb$  and  $f_w$  on  $\theta$ . (a) No thermal slip. (b) With thermal slip.

Figure 10 shows that decreases of the solutal profile are associated with the increase of  $kc$ . Expanding estimations of the unsteadiness parameters lead to decline in concentration profile. We additionally see in Figure 10b that the concentration profile decline as the solutal slip parameter increments. Figure 11 demonstrates the influence of Soret parameter  $Sr$  on the solutal profile. It is clear from Figure 11 that the boundary layer of solutal profile increases with an increment in  $Sr$ . A similar behavior of unsteadiness parameter, and solutal slip is observed in Figure 11.

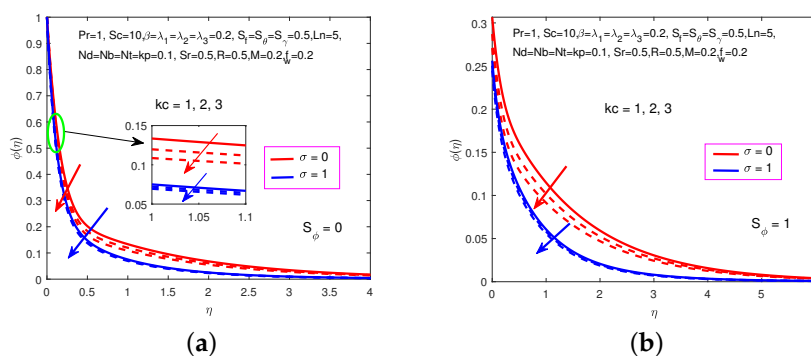


Figure 10. Influence of  $kc$  and  $\sigma$  on  $\phi$ . (a) No solutal slip. (b) With solutal slip.

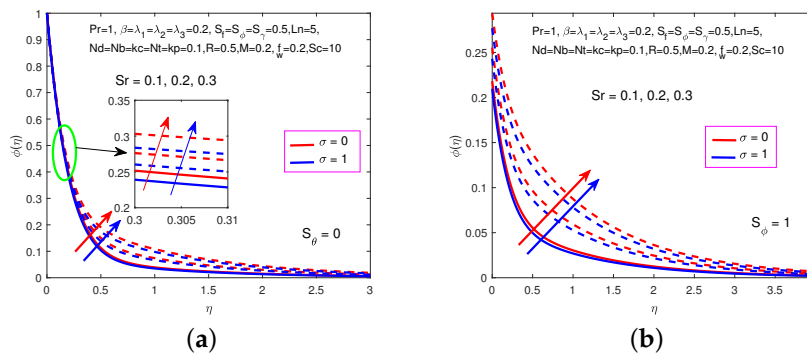


Figure 11. Influence of  $Sr$  and  $\sigma$  on  $\phi$ . (a) No solutal slip. (b) With solutal slip.

Figure 12 shows the influence of  $Nt$  on the nanoparticle volume fraction profile with no nanoparticle concentration slip (Figure 12a) and nanoparticle concentration slip (Figure 12b). The nanoparticle volume fraction profile decreases with the increase of  $Nt$ . The effects of  $\sigma$  over the nanoparticle volume fraction profile is also depict in Figure 12b and it is observed that nanoparticle volume fraction profile decreases in unsteady cases. We also see in Figure 12b that the nanoparticles concentration profile decline as the  $S_\gamma$  incremented. Figure 13 demonstrates the influence of Lewis number  $Ln$ , slip parameter  $S_\gamma$  and suction parameter  $f_w$  on nanoparticle volume fraction profile is observed, and some interesting observations of nanoparticle volume fraction profile are made. It is clear from Figure 13 that the boundary layer of nanoparticle volume fraction profile decreases with an increment in  $Ln$ ,  $f_w$ , and  $S_\gamma$ . Figure 14 shows the influence of  $M$ ,  $\sigma$ ,  $S_f$ ,  $\lambda_1, \lambda_2$  and  $f_w$  on the skin friction coefficient. It is clear from the Figure 14 that skin friction coefficient decreases with increasing values of the slip parameter and buoyancy parameter but skin friction coefficient increases with increasing values of the magnetic, unsteadiness, and suction parameters. The Nusselt number increases with increasing values of magnetic and thermal buoyancy parameters and decreases with increasing values of thermal slip, solutal buoyancy, suction and radiation parameters. It is clearly seen in Figure 15. Figure 16 illustrate the influence of  $M, Sc, Sr, S_\phi, \sigma$  and  $f_w$  on the reduced Sherwood number. It is clear from Figure 16 that the Sherwood number increases with increasing values of the Schmidt number, unsteadiness, and suction parameters, whereas a reduced Sherwood number decreases with increasing values of the Soret number, magnetic, and solutal slip parameters.

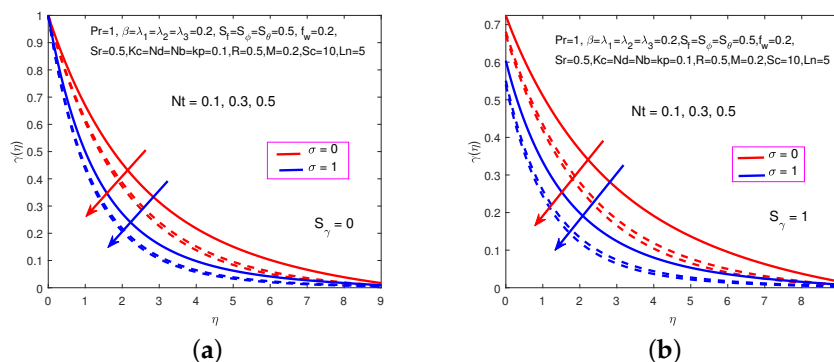


Figure 12. Influence of  $Nt$  and  $\sigma$  on  $\gamma$ . (a) No nanoparticles concentration slip. (b) With nanoparticles concentration slip.

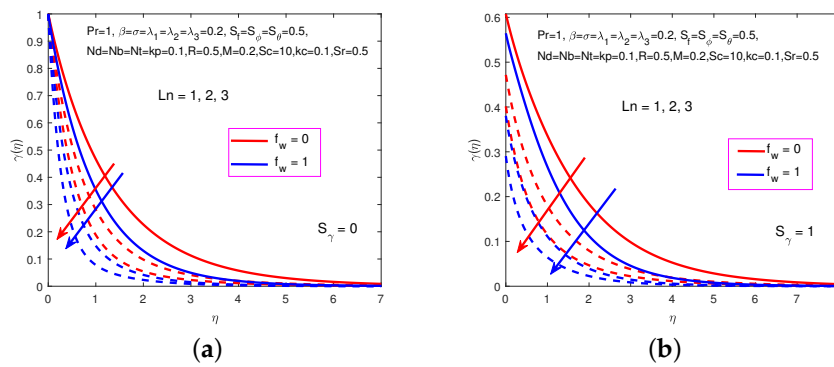


Figure 13. Influence of  $L_n$  and  $f_w$  on  $\gamma$ . (a) No nanoparticles concentration slip. (b) With nanoparticles concentration slip.

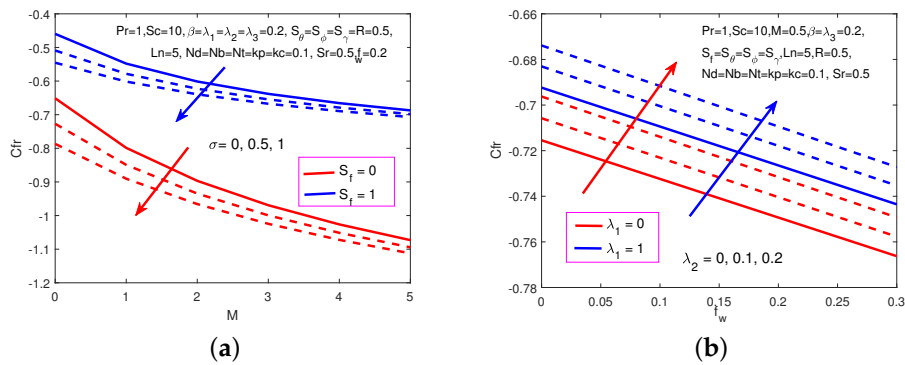


Figure 14. Influence of  $M, \sigma, S_f, \lambda_1, \lambda_2,$  and  $f_w$  on the skin friction coefficient. (a) No hydrodynamic slip and with hydrodynamic slip. (b) No thermal buoyancy and with thermal buoyancy.

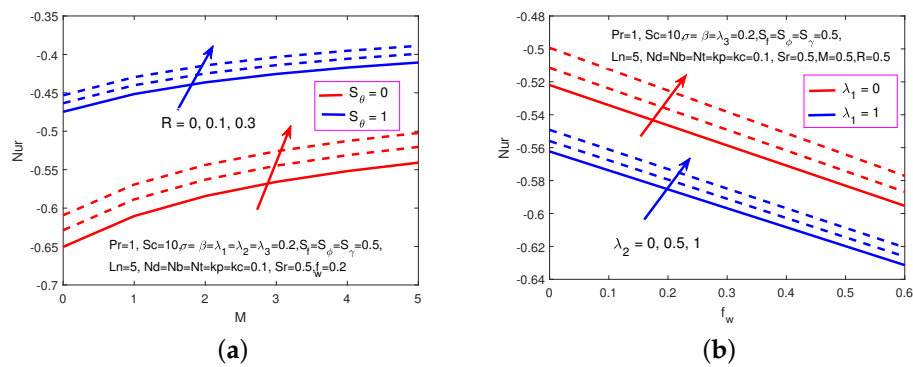
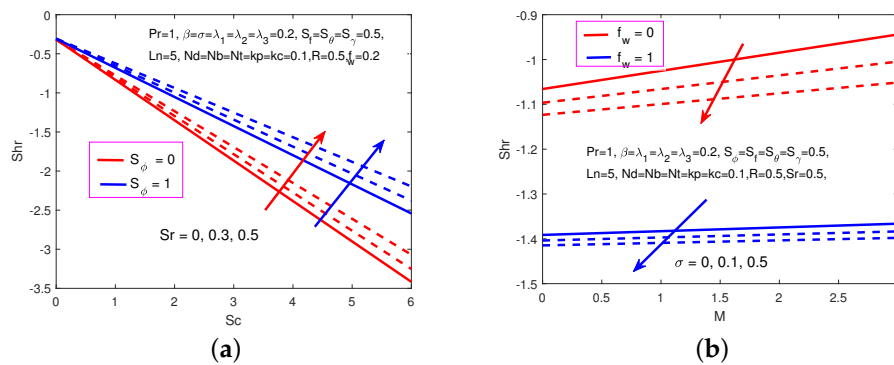


Figure 15. Influence of  $M, R, S_\theta, \lambda_1, \lambda_2,$  and  $f_w$  on the reduced Nusselt number. (a) No thermal slip and with thermal slip. (b) No thermal buoyancy and with thermal buoyancy.



**Figure 16.** Influence of  $Sc, Sr, M, S_\phi, \sigma,$  and  $f_w$  on the reduced Sherwood number. (a) No solutal slip and with solutal slip. (b) No suction and with suction.

## 5. Conclusions

The present study analyzes the multiple slip effects on magnetohydrodynamic unsteady Maxwell Nanofluid flow over a permeable stretching sheet with radiation and thermo-diffusion in the presence of chemical reaction. By using the appropriate similarity transformation, the control nonlinear PDEs are transformed into a set of highly nonlinear ODEs, and the nonlinear coupled ODEs are solved by using robust and verified variational finite element method under the realistic boundary conditions. The computations have been performed for velocity, temperature, solutal and nanofluid volume fraction functions for various values of physical parameters. The key conclusions of this work are as follows.

- The velocity profiles decrease with increasing values of suction, slip, unsteadiness, magnetic, Deborah number, and permeability parameters, but the influence is opposite for increasing values of buoyancy parameters and thermal radiation.
- Increments in magnetic field and Brownian motion parameters enhance the fluid temperature. However, the opposite influence is experienced with increasing values of suction and slip parameters.
- The solutal profile reduces with increasing values of the chemical reaction parameter, unsteadiness parameter, and slip parameter, but the solutal profile is enhanced with increasing values Soret number.
- Increasing the values of the thermophoresis, suction, slip, Lewis number, and unsteady parameters leads to the deceleration of the nanoparticles volume fraction profile.
- The skin friction coefficient increases with increasing rates of magnetic, suction, and unsteadiness parameters, whereas the skin friction coefficient decreases with the higher values of the slip and buoyancy parameters.
- Increments in magnetic field and thermal buoyancy parameters enhance the fluid Nusselt number but the opposite influence is experienced with increasing values of slip, solutal buoyancy, suction, and thermal radiation parameters.
- The Sherwood number increases with increasing values of Schmidt number, unsteadiness, and suction parameters, but reduces with increasing values of the Soret number, magnetic, and slip parameters.

**Author Contributions:** B.A. and S.A.K. modeled the problem and wrote the manuscript. Y.N. thoroughly checked the mathematical modeling and English corrections. B.A. solved the problem using MATLAB software. M.T.S. and M.T.: writing—review and editing. Y.N. contributed to the results and discussions. All authors finalized the manuscript after its internal evaluation.

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