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# Ankle Mechanics During Jump Landings Across Different Foot Positions in Professional Ballet Dancers

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#### 6 Authors:

7 Adam M. Mattiussi<sup>1,2,3,\*</sup>, Joseph W. Shaw<sup>1,2</sup>, Phil Price<sup>1</sup>, Derrick D. Brown<sup>4</sup>, Daniel D. Cohen<sup>5</sup>,

8 Jack Lineham<sup>1</sup>, Charles R. Pedlar<sup>1,6</sup>, Jamie Tallent<sup>7,8</sup>, Alexandra C. Atack<sup>1</sup>

#### 9 10 **Institutional/Corporate affiliations**:

- <sup>1</sup> School of Sport, Exercise and Applied Sciences, St Mary's University, Twickenham, UK
- <sup>2</sup> Ballet Healthcare, The Royal Ballet, Royal Opera House, London, UK
- <sup>3</sup> Performance Rehabilitation, UK Sports Institute, Bisham, UK
- <sup>4</sup> Institute of Sport Science, Dance Science, University of Bern, Bern, Switzerland
- <sup>5</sup> Faculty of Health Sciences, University of Santander, Bucaramanga, Colombia
- <sup>6</sup> Division of Surgery and Interventional Science, University College London, UK
- <sup>7</sup> School of Sport, Rehabilitation and Exercise Sciences, University of Essex, Colchester, UK
- 18 <sup>8</sup> Faculty of Medicine, Nursing and Health Science, Monash University, Melbourne, Australia

# 1920 \*Correspondence:

- 21 Adam Mattiussi
- 22 <u>Mattiussi.adam@gmail.com</u>
- 23 Performance Rehabilitation, UK Sports Institute, Bisham, United Kingdom
- Preferred running head: Ankle Mechanics during Jumping in Professional Ballet Dancers
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30	Adam Mattiussi	Twitter: @adammattiussi	Orcid ID: 0000-0001-7287-6501
31	Joseph Shaw	Twitter: @josephshaw	Orcid ID: 0000-0002-1538-9966
32	Daniel Cohen	Twitter: @danielcohen1971	Orcid ID: 0000-0002-0899-4623
33	Phil Price	Twitter: @thepricep	Orcid ID: 0000-0001-8849-2959
34	Derrick Brown	Twitter: @ddbrown	Orcid ID: 0000-0001-9220-8025
35	Jack Lineham	Twitter: NA	Orcid ID: 0000-0003-3393-2771
36	Charles Pedlar	Twitter: @pedlarcr	Orcid ID: 0000-0002-3075-9101
37	Jamie Tallent	Twitter: @jamietallent	Orcid ID: 0000-0002-4354-9912
38	Alexandra Atack	Twitter: @a_atack2	Orcid ID: 0000-0001-5766-5861

#### 39 ABSTRACT

40 This study aimed to investigate the effect foot position on ankle joint mechanics and vertical 41 ground reaction forces (vGRF) across jump landings in professional ballet dancers. Twentyseven professional ballet dancers (men: 14; women: 13) attended one data collection session, 42 43 completing five maximal countermovement jumps in parallel, first, second, fourth, and fifth 44 positions. Three-dimensional ankle mechanics, landing vGRF variables, and jump height were 45 recorded via a seven-camera motion capture system and one force platform. A repeated 46 measures multivariate analysis of variance was used to assess the main effects foot position 47 across all target variables. A linear discriminate analysis was conducted to investigate target 48 variables across foot positions. Frontal and transverse plane ankle mechanics had the largest impact when discriminating between foot positions. Ankle power in the transverse plane during 49 jump landing in fourth was double that of all other positions. Our findings suggest that ankle 50 range of motion should be restored before returning to jumps in fourth and fifth positions 51 52 following distal lower extremity injury. The multiplanar energy transfer observed indicates a need for specific exercises to develop multiplanar force and rate of force development of local 53 54 structures around the ankle.

55 Keywords: Biomechanics, Ground Reaction Forces, Kinematics, Kinetics, Machine Learning

#### 56 INTRODUCTION

57 The rehearsal and performance demands of professional ballet are characterised by a high 58 volume of jumping actions (Shaw et al., 2021). Jumping actions have been associated with a 59 third of all medical attention and time-loss injuries in professional ballet dancers (A. M. 60 Mattiussi et al., 2021); with the greatest burden observed around the distal lower extremity. Moran et al. (2019) suggested that landing biomechanics (and jump volume) may provide 61 62 practitioners with 'the next great injury analytic' for activities that have high jumping demands. Indeed, investigations into landing biomechanics will provide insights into the load 63 experienced by different structures of the lower extremity. Once the load experienced during 64 landing is understood, practitioners can better manage the load-capacity relationship in hope 65 66 of mitigating potential injury risk and maximising performance in ballet dancers (Edwards, 67 2018).

68 There is a vast repertoire of jumps to which ballet dancers will be exposed each day, making 69 the documentation of all of them challenging. Different ballet jumps may be characterised by 70 whether they are travelling or stationary; have contributions from a single limb or both limbs; 71 and whether there are technical actions throughout the different phases of the jump (such as 72 beats, splits, or arabesques) (A. Mattiussi et al., 2021). There are, however, codified foot positions that underpin all ballet technique, referred to as first, second, third, fourth, and fifth 73 74 positions. All jumping actions will take off or land in one of these fundamental foot positions 75 which provides an opportunity to refine the documentation of jumping biomechanics in ballet. 76 To date, only two studies have investigated the effect of these codified foot positions on lower 77 extremity biomechanics during jumping (Imura & Iino, 2017; Ravn et al., 2007).

78 The technical requirements of ballet change the kinetic and kinematic characteristics of

- <sup>79</sup> jumping when compared to more typical foot positions (i.e., parallel) (A. Mattiussi et al., 2021).
- 80 For example, kinematic differences such as minimal hip flexion, an upright torso, and an

81 externally rotated lower limb were observed when jumps in turn out were compared to jumps 82 in parallel (Imura & Iino, 2017). Kinetic variables, such as lower extremity joint moment, power, and work have exhibited a proximal-to-distal shift in joint contributions during ballet-83 84 specific jumps compared to traditional jumps (Ravn et al., 2007). All of these characteristics are indicative of greater contributions from the distal lower extremities during jumping actions 85 in ballet dancers, placing a greater demand on the tissues around the foot and ankle. It should 86 be noted, however, that both of the aforementioned studies have only investigated the take-off 87

88 phase of a jump. Presently there is a lack of data pertaining to distal lower extremity joint

- 89 mechanics during the landing phase of different ballet jumps.
- 90 Where studies have investigated landing biomechanics in ballet dancers peak landing vertical 91 ground reaction force (vGRF) has been the most commonly reported variable (A. Mattiussi et
- 92 al., 2021). The range in peak landing vGRF is between 1.4–9.6 times body weight (BW) during
- 93 various unilateral and bilateral ballet-specific jumps (Dworak et al., 2006; Gorwa et al., 2020;
- Lee et al., 2012; McPherson et al., 2019; Mertz & Docherty, 2012; Peng et al., 2015). The 94
- 95 technical requirements of the jump may influence the peak landing vGRF, as ballet-specific
- 96 jumps tend to result in greater vGRF than traditional jumps (A. Mattiussi et al., 2021). Two of 97 these studies, however, included sample sizes of one and two participants, which may not be
- generalisable to all dancers (Dworak et al., 2006; Gorwa et al., 2020). Loading rate has also 98
- 99 been described during several ballet-specific jumps, with values ranging between 10-223

BW·s<sup>-1</sup> (Arnwine & Powell, 2020; Dworak et al., 2006; Gorwa et al., 2020; Lee et al., 2012; 100

- Peng et al., 2015), however, similar to the vGRF data, two of these studies had very small 101
- sample sizes (Dworak et al., 2006; Gorwa et al., 2020). 102

103 Much of the existing literature investigating jumping and landing in ballet dancers may not 104 apply to elite populations as it has largely been conducted on non-professional or non-ballet populations (A. Mattiussi et al., 2021). The aim of this study was to investigate the effect of 105 foot position (parallel, first, second, fourth, and fifth) on ankle joint mechanics and vGRFs 106 across jump landings in professional ballet dancers. We hypothesised that ballet-specific foot 107 108 positions would have different biomechanics characteristics compared to parallel and one 109 another.

#### **METHODS** 110

#### 111 Study Design

A cross-sectional study design was employed to investigate the effect of foot position on ankle 112 mechanics and vGRF (Supplementary Material 1) during jump landing in professional ballet 113 114 dancers. Dancers attended one data collection session where they completed five countermovement jumps (CMJ) across seven different foot positions (Figure 1). All testing was 115

conducted in the \*BLINDED\* during the 2020-21 season. 116

#### 117 **Participants**

- Twenty-seven professional ballet dancers (men: n = 14, age:  $26.7 \pm 4.9$  y, height:  $1.79 \pm 0.04$ 118
- m, mass:  $72.6 \pm 5.2$  kg, professional:  $8.9 \pm 5.2$  y; women: n = 13, age:  $24.0 \pm 3.7$  y, height: 119
- $1.68 \pm 0.04$  m, mass:  $55.2 \pm 3.3$  kg, professional:  $5.9 \pm 3.8$  y) volunteered to participate in this 120
- 121 study from a cohort of 105 dancers (25.7%). Dancer ranks included Apprentices (n = 3), Artists

- 122 (n = 8), First Artists (n = 6), Soloists (n = 2), First Soloists (n = 5), and Principals (n = 3).
- 123 Participants were required to not have sustained a lower extremity time-loss injury in the six
- 124 weeks prior to testing. Informed consent was obtained prior to data collection and ethical 125 approval was provided by \*PL NDED\* Ethics Committee in accordance with the Declaration
- approval was provided by \*BLINDED\* Ethics Committee in accordance with the Declarationof Helsinki.

#### 127 Procedure

128 Participants completed a standardised and progressive warm-up prior to testing. Retroreflective

- 129 markers (22 mm diameter) were attached to the right: greater trochanter, medial and lateral
- 130 joint lines of the knee, medial and lateral malleolus, posterior aspect of the calcaneus, superior
- 131 aspect of the navicular, medial aspect of the  $1^{st}$  metatarsal head, and the lateral aspect of the  $5^{th}$
- 132 metatarsal head using double-sided adhesive tape and adhesive spray. Curved rigid moulded 133 clusters with four retroreflective markers were attached to the lateral aspect of the right shank
- 133 clusters with four retroreflective markers were attached to the late134 using cohesive elastic tape and electrical tape (Figure 2).
- 135 Participants completed five maximal bilateral CMJs across seven different foot positions: 136 parallel, first, second, fourth with the front leg on the force platform (fourth front), fourth 137 position with the back leg on the force platform (fourth back), fifth position with the front leg 138 on the force platform (fifth front), and fifth position with the back leg on the force platform 139 (fifth back; Figure 1). Dancers were informed to maintain ballet technique to the best of their 140 ability (i.e., turned out across ballet positions and crossed in fourth and fifth positions). The 141 right limb was positioned on the force platform and the left limb was positioned on a wooden 142 frame that surrounded the force platform (Figure 1). The participant's hands were placed on their shoulders for all jumps. Order effects were mitigated by alternating jumps until a jump in 143 144 each foot position was performed within a set. Twenty seconds of intra-set rest and two minutes
- 145 of inter-set rest were provided (Pereira et al., 2008).
- 146 A seven-camera motion capture system (MX3/MX3+, Vicon Motion Systems Ltd, Oxford,

147 United Kingdom) sampling at 200 Hz, and one piezoelectric force platform (9268A, Kistler,

- 148 Winterthur, Switzerland) sampling at 1000 Hz synchronously recorded retroreflective marker
- 149 coordinates and ground reaction forces, respectively. The global coordinate system was defined
- 150 such that Z was vertical, X was horizontal, and Y was the cross-product of Z and X.

### 151 Data Analysis

152 Marker trajectories were reconstructed and labelled in Vicon Nexus (Vicon Motion Systems Ltd, Oxford, United Kingdom) before being processed in Visual 3D (v2021.113 C-Motion©, 153 154 USA). All marker trajectory gaps consisted of seven frames or fewer and were interpolated 155 using cubic splines. A foot and a shank segment were created in Visual 3D. The foot was defined by the medial and lateral malleolus as the proximal endpoints and the medial aspect of 156 the 1<sup>st</sup> metatarsal head and the lateral aspect of the 5<sup>th</sup> metatarsal head as the distal endpoints. 157 158 The shank was defined by the medial and lateral joint lines of the knee as the proximal 159 endpoints and the medial and lateral malleolus as the distal endpoints. Foot and shank segment 160 inertia parameters were defined in line with de Leva (de Leva, 1996). Individual and cluster 161 markers for the foot and shank were used to track segments during dynamic trials. An inverse 162 kinematics approach was used to estimate the pose of the segments (Lu & O'Connor, 1999), 163 filtered at 8 Hz and allowing three degrees of rotation but no translation between the foot and 164 shank segments. Ankle joint angles were calculated using an XYZ Cardan rotation sequence 165 whilst the proximal segment was used as both the reference segment and the resolution 166 coordinate system when determining ankle angular velocity. Kinematic data and segmental inertial data were combined with ground reaction force data to calculate joint kinetics using an 167 inverse dynamics approach (de Leva, 1996). Marker and ground reaction force data were 168 169 filtered at 8 Hz using a low-pass fourth-order Butterworth filter, determined via residual analysis (Winter, 2009). Ankle joint moment and joint power were normalised for comparisons 170 171 between participants (Hof, 1996)—leg length was replaced with height (Atack et al., 2019) and 172 an adjusted calculation for normalized power was used to provide a dimensionless value 173 (Bezodis et al., 2010):

174 Normalised Ankle Moment = 
$$\frac{M}{mgh}$$
  
175 Normalised Ankle Power =  $\frac{P}{mg^{3/2}h^{1/2}}$ 

Vertical ground reaction force data were reprocessed and filtered at 250 Hz using a low pass
fourth-order Butterworth filter, determined via residual analysis (Winter, 2009), to calculate

179 Normalised vGRF = 
$$\frac{F}{mg}$$

180 The start of each landing phase was identified where vGRF was >50 N following the period of 181 flight. The end of each landing phase was calculated as the point at which data collection 182 ceased. Data were extracted from the landing phase and variables were computed. Peak values 183 of ankle mechanics and vGRF measures were calculated as the greatest value throughout the 184 landing phase. through all planes of motion. Ankle excursion was calculated by subtracting the 185 minimum ankle angle from the peak ankle angle. Loading rate was calculated using the 186 following equation:

187 Loading Rate = 
$$\frac{Normalised Peak Landing vGRF}{Time to Normalised Peak Landing vGRF}$$

188 Vertical displacement—hereon referred to as jump height—was calculated as the difference 189 between the height of the greater trochanter in standing and at the peak of flight using the raw

- 190 marker coordinates.
- 191 Statistical Analysis

A repeated measures MANOVA was conducted to investigate within-subject multivariate main 192 effects of foot position on ankle mechanics and vGRF during jump landings in professional 193 194 ballet dancers using the R package stats (R Core Team, 2022). Extreme outliers—where values 195 above Q3 + 3 × IQR or below Q1 - 3 × IQR—were removed (n = 22; 0.8%) using the R package *rstatix* (Kassambara, 2020). A post-hoc sensitivity analysis revealed that a sample size 196 197 of 27 participants was sensitive to detect an effect size = 0.232 ( $\beta$  = 0.80,  $\alpha$  = 0.05, Pillai V = 198 0.4, correlation among repeated measures = 0.5, measurements = 7) using G\*Power 3 (Faul et 199 al., 2007). The assumption of multivariate normality was violated and thus ordered quantile transformations were applied to all dependent variables using the R package bestNormalize 200

201 (Peterson, 2017). A parametric approach was selected over a non-parametric approach as a
 202 MANOVA is robust to type 1 error and power decrements and outperforms non-parametric
 203 equivalents in the presence of non-normal data (Finch, 2005).

Linear discriminate analyses (LDA) were conducted to investigate significant main effects using the R package *MASS* (Venables & Ripley, 2002). The LDA provides regression equations in which the contributions of all kinetic and kinematic outcome variables can be used to classify the main effect grouping variable (i.e., foot position). One additional post-hoc LDA was conducted based on visual inspection of the results from the initial LDA, where a hypothesis on how model accuracy may be improved was acted on (Hollenbeck & Wright, 2017). All data processing and statistical analysis were conducted using R (version 4.2.1, R Foundation for

211 Statistical Computing, Vienna, Austria).

#### 212 RESULTS

213 The repeated measures MANOVA revealed a significant within-subject main effect of foot

- 214 position ( $F_6 = 6.6$ ; p < .001; Pillai = 2.9). The mean, standard deviation, and 95% CI for all
- 215 variables across foot positions are presented in Supplementary Material 2. The mean, standard
- 216 deviation, and 95% CI for all variables across men and woment are presented in Supplementary
- 217 Material 3.

218 One LDA was performed to investigate the main effect of foot position which included all 219 variables across all seven foot positions. Six linear discriminants were identified to classify

- foot position (LD1: 49.3%; LD2: 36.3%; LD3: 10.4%; LD4: 1.4%; LD5: 1.4%; LD6: 0.7%).
  The LDA investigating the effects of foot position had a classification accuracy of 56.8% when
- tested for performance. Clear clusters were visually observed between the symmetrical ballet
- foot positions (first and second), positions assessing the back foot (fourth back and fifth back),
  and positions assessing the front foot (fourth front and fifth front) when plotted (Figure 3).
- Thus, a second LDA was conducted where these foot positions were grouped such that only four different foot positions were input into the model (i.e., parallel, first and second combined, fourth back and fifth back combined, and fourth front and fifth front combined). Three linear discriminants were identified to classify grouped foot positions (LD1: 51.4%; LD2: 43.0%; LD3: 5.5%). The LDA investigating the effects of grouped foot position had a classification accuracy of 91.4% (60% improvement) when tested for performance. The results of both
- accuracy of 91.4% (60% improvement) when tested for performance. The results of both models investigating the effect of foot position are presented in Figure 3. The regression
- equations representing the three linear discriminants for grouped foot positions can be found in Figure 4. The mean, standard deviation, and 95% CI for all variables across the grouped foot
- 234 positions are presented in Table 1.

235 Due to the relatively small contribution of LD3 (5.5%), only LD1 (51.4%) and LD2 (43.0%) 236 are discussed in detail. Linear discriminate one was able to classify jump landings in parallel 237 from all ballet-specific foot positions (Figure 3). The regression equation for LD1 revealed that frontal plane ankle joint angles and excursions and transverse plane excursions have a 238 239 considerable contribution to the classification of parallel from all other ballet-specific foot positions (Figure 4). Further, transverse plane ankle joint moments, frontal plane ankle joint 240 241 power, and jump height were also identified as important variables contributing to this 242 classification. Linear discriminate two was able to classify jump landings in the grouped front 243 foot position from all other positions (Figure 3). The regression equation for LD2 revealed that transverse plane ankle joint power and frontal plane ankle joint angles have a considerable contribution to the classification of jump landings in the grouped front foot position from all other positions. (Figure 4).

247 Both fourth and fifth positions demonstrated a greater peak ankle abduction angle compared to 248 all other foot positions, with the grouped front foot involving six times more abduction 249 compared to first and second, and three times more abduction compared to the grouped back 250 foot (Table 1). Frontal plane ankle excursions were greatest in the grouped back foot position, 251 with values 15–20% larger than all other positions. Grouped first and second position exhibited transverse plane excursions 1.5 times that of parallel, and grouped front and grouped back foot 252 positions exhibited transverse plane excursions twice that of parallel (Table 1). Transverse 253 254 plane ankle joint moments in parallel were at least twice that of all ballet foot positions. 255 Conversely, frontal plane ankle joint power was 1.3–2.3 times greater in all ballet foot positions when compared to parallel. The grouped back foot peak ankle power in the transverse plane 256 exhibited more than double that of all other foot positions. Jump height was comparable across 257 all foot positions other than parallel where participants jumped an additional 3-4 cm (Table 1). 258 259 Loading rate was 15% higher in grouped first and second position and grouped back foot position compared to parallel and front foot position. Vertical ground reaction force was 6-8%260 greater in first and second and the grouped front foot position when compared to parallel and 261 262 the grouped back foot position.

#### 263 DISCUSSION AND IMPLICATION

264 This is the first study to investigate the effect of parallel, first, second, fourth, and fifth positions on ankle mechanics and vGRF during jump landings in professional ballet dancers. The results 265 demonstrated that foot position influences ankle mechanics and vGRF during jump landings in 266 267 professional ballet dancers. Further, the results indicate that ankle mechanics and vGRFs are comparable between first and second positions, the back foot in both fourth and fifth positions, 268 269 and the front foot in both fourth and fifth positions. In particular, the peak ankle joint angle in 270 the frontal plane was able to discriminate between parallel and both grouped front and back 271 foot positions. Peak transverse plane ankle power and frontal plane ankle joint angle were both 272 able to discriminate between the grouped front foot and all other foot positions. These results 273 highlight the biomechanical variance across these fundamental foot positions which may 274 impact decision-making around technical and physical goal setting in professional ballet in a 275 performance and rehabilitation context.

The initial LDA and the post-hoc LDA revealed new insights into how foot positions might be 276 277 categorised based on ankle mechanics and vGRF. A 60% improvement in model classification accuracy was observed following the grouping of foot positions (ungrouped: 57%; grouped: 278 279 91%); demonstrating the similarities between first and second positions, the back foot in fourth 280 and fifth position, and the front foot in fourth and fifth position. To that end, grouping these 281 foot positions when considering ankle mechanics and vGRF is warranted and may aid in simplifying decision-making in applied environments. The results of the present study indicate 282 that three-dimensional ankle kinetics and kinematics play a critical role in discriminating 283 284 between different foot positions, particularly through the frontal and transverse planes. It is 285 perhaps unsurprising that frontal and transverse plane kinematics were able to discriminate the 286 grouped front and back foot positions in fourth and fifth from other positions due to the offset 287 and asymmetrical nature of these positions when compared to parallel, first, and second.

288 Presently there is limited literature investigating different foot positions, making comparison challenging. Imura and Iino (2017) investigated parallel and first during take-off and observed 289 no differences in peak ankle dorsiflexion angle, ankle plantarflexion moment, or ankle 290 plantarflexion work between parallel and first. Conversely, when Ravn et al., (2007) 291 292 investigated parallel and first during take-off, they observed peak sagittal plane ankle joint 293 moments and powers in first position at least twice that of parallel. Ravn et al., (2007), however, performed no statistical analysis and only three participants were included, potentially leading 294 295 to inflated results (Konietschke et al., 2021). Both of the aforementioned studies also used 296 different methods to calculate kinetic outcome variables, limiting any direct comparisons with 297 our analysis. The results from the present study indicate that sagittal plane kinetics and 298 kinematics are poor classifiers of foot position compared to frontal and transverse plane 299 kinetics and kinematics.

300 The landing vGRF observed in the present study ( $\sim 2 \times \text{bodyweight}$ ) is comparable to values reported during continuous *échappé sauté* (a countermovement jump alternating the landing 301 302 between fifth position and second position; Peng et al., 2015) and sissonne fermée (a horizontal 303 jump from one leg landing in fifth position; Lee et al., 2012), but roughly half to a third lower 304 than more technical jumps such as grand jeté (a travelling leap from on limb to the other with a split during flight; Arnwine & Powell, 2020) or *double tour* (a countermovement jump from 305 306 and to fifth position with a 720-degree rotation while in flight; Dworak et al., 2006; Gorwa et 307 al., 2020). It should be noted, however, that only a single limb was investigated during bilateral jumps in the present study and the total vGRF experienced through both limbs will be greater. 308 309 Several studies have reported joint kinetics during ballet jumps (Gorwa et al., 2020; Perry et al., 2019), however, differences in equations make comparisons challenging. Further research 310 311 examining joint mechanics during repeated jumping, travelling jumps, and unilateral jumps in

different foot positions may reveal insights into the biomechanical demands of ballet jumps.

#### 313 Practical Applications

314 The differences observed in ankle mechanics and vGRF during jump landings in different foot 315 positions in the present study provide a basis for grouping foot positions. Jump landings across all ballet foot positions require greater peak ankle angles and excursions when compared to 316 parallel, particularly in fourth and fifth positions. Thus, restoring ankle mobility during 317 rehabilitation could be critical prior to returning to these positions in performance settings. The 318 319 notably higher transverse plane peak ankle power observed during jump landings in the 320 grouped back foot positions indicates a high rate of energy transfer while landing in these 321 positions. To that end, exercises that emphasise rotational force or high rates of rotational force 322 around the ankle may be warranted in professional ballet dancers. Further, when planning 323 return-to-dance pathways following injury, it is recommended that jump (or *pointe*) exercises 324 in which dancers land in fourth or fifth position may be introduced later than exercises in 325 parallel, first, and second.

#### 326 Strengths, Limitations, and Future Directions

327 This research is one of few studies investigating jumping actions in both male ballet dancers

328 and professional ballet dancers (A. Mattiussi et al., 2021), demographics which have previously

- been under-studied in the ballet literature. Considering male ballet dancers and professional
- ballet dancers will typically be exposed to greater jumping demands than female dancers and

- 331 non-professionals, respectively, it is important to understand these demographics in more detail
- 332 (Shaw et al., 2021). Bilateral asymmetries or limb dominance may have affected the results of
- this study, as only the right limb was measured during bilateral jumps. Previous work, however,
- has found no association between a dancer's perception of limb dominance and their kinetics
- during jumping (Mertz & Docherty, 2012). Future work may wish to conduct a broader analysis
- of landing biomechanics in dancers which includes the trunk and entire lower extremity.

#### 337 CONCLUSION

- 338 This study investigated the effect of foot position on ankle mechanics and vGRF in professional
- ballet dancers. The results identified that foot position influences ankle mechanics and vGRF
- 340 during jump landings. Frontal and transverse plane ankle mechanics had the largest impact
- 341 when discriminating between different foot positions, with jump landings in fourth and fifth
- 342 demonstrating greater ranges of motion, moments, and power when compared to other foot
- 343 positions. Adaptations in multiplanar force and rates of force development are warranted in
- 344 professional ballet dancers. Finally, following injury, full ankle range of motion should be
- 345 restored prior to returning to fourth and fifth positions.

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### 449 TABLE 1

450 '	Table 1. Mean $\pm$ SD	[95% CI	of ankle mechanics and vGRF ad	cross grouped foot positions
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	Parallel	1st/2nd	4th/5th Back	4th/5th Front
Normalised Moment <sup>x</sup>	$0.098 \pm 0.010 \; [0.079, 0.117]$	$0.092 \pm 0.012 \; [0.068,  0.115]$	$0.102\pm 0.016\ [0.071, 0.133]$	$0.101\pm 0.018\;[0.065,0.136]$
Normalised Moment <sup>Y</sup>	$0.017 \pm 0.008 \; [0.002,  0.033]$	$0.006 \pm 0.006 \; [0.000,  0.017]$	$0.004 \pm 0.003 \; [0.000,  0.010]$	$0.005 \pm 0.004 \; [0.000,  0.014]$
Normalised Moment <sup>Z</sup>	$0.010\pm0.005\;[0.000,0.019]$	$0.005 \pm 0.003 \; [0.000,  0.012]$	$0.002\pm0.002\;[0.000,0.005]$	$0.005 \pm 0.003 \; [0.000,  0.010]$
Normalised Power <sup>X</sup>	$1.24\pm0.20\;[0.85,1.63]$	$1.24\pm0.23\;[0.78,1.70]$	$1.22\pm0.25\;[0.72,1.72]$	$1.33\pm 0.30\;[0.74,1.92]$
Normalised Power <sup>Y</sup>	$0.10\pm0.05\;[0.01,0.20]$	$0.14\pm0.06\;[0.02,0.26]$	$0.13\pm0.07\ [0.00,0.27]$	$0.23\pm0.09\;[0.06,0.40]$
Normalised Power <sup>Z</sup>	$0.08\pm0.03\;[0.01,0.14]$	$0.09\pm0.04\;[0.02,0.16]$	$0.22\pm0.06\;[0.10,0.34]$	$0.06\pm0.03\;[0.01,0.11]$
Velocity <sup>X</sup> ( $^{\circ} \cdot s^{-1}$ )	$907 \pm 68$ [774, 1040]	$945\pm80\ [788,1102]$	$933\pm84\ [768,1098]$	895 ± 88 [722, 1068]
Velocity <sup>Y</sup> ( $^{\circ} \cdot s^{-1}$ )	$97 \pm 48$ [3, 191]	$88\pm 36\;[16,159]$	$103 \pm 40$ [26, 181]	$125\pm 48\ [31,218]$
Velocity <sup>Z</sup> (°·s <sup>-1</sup> )	$135 \pm 50 \; [37, 234]$	$186\pm74~[41,330]$	$147\pm 61\ [28,266]$	$190\pm 60~[72,308]$
Angle <sup>X</sup> (°)	$103 \pm 4$ [94, 111]	$103 \pm 4$ [94, 111]	$106 \pm 5$ [97, 115]	104 ± 4 [95, 112]
Angle <sup>Y</sup> (°)	2 ± 3 [-4, 8]	-2 ± 4 [-9, 5]	-4 ± 4 [-13, 5]	-13 ± 4 [-22, -4]
Angle <sup>Z</sup> (°)	-7 ± 5 [-18, 3]	-5 ± 5 [-15, 5]	-4 ± 8 [-19, 11]	7 ± 4 [-2, 15]
Excursion <sup>X</sup> (°)	$64 \pm 7$ [50, 77]	$69 \pm 5$ [58, 79]	68±7 [54, 81]	$70 \pm 6$ [59, 81]
Excursion <sup>Y</sup> (°)	$20 \pm 4$ [13, 27]	$21 \pm 4$ [13, 29]	$24 \pm 4$ [15, 32]	$20 \pm 4$ [12, 28]
Excursion <sup>Z</sup> (°)	11 ± 4 [4, 19]	$15 \pm 5$ [5, 26]	$18 \pm 5$ [7, 28]	$20 \pm 7$ [8, 33]
vGRF (BW)	$1.94 \pm 0.45 \; [1.07, 2.82]$	$2.05\pm0.56\;[0.95,3.14]$	$1.90\pm0.39\ [1.14,2.66]$	$2.04\pm0.58\;[0.90,3.17]$
TTP vGRF (s)	$0.09\pm0.02\;[0.05,0.13]$	$0.08\pm0.02\;[0.04,0.12]$	$0.09\pm0.02\;[0.04,0.13]$	$0.09\pm0.02\;[0.05,0.12]$
Loading rate (BW·s <sup>-1</sup> )	$26.9 \pm 13.3 \; [0.9,  53.0]$	$30.5\pm15.1\;[0.9,60.1]$	$30.7 \pm 19.0 \ [0.00, \ 67.9]$	$26.5 \pm 11.7 \; [3.6, 49.5]$
Jump height (cm)	42.2 ± 7.7 [27.0, 57.4]	$39.5 \pm 7.0 \ [25.9, 53.2]$	$39.5 \pm 6.4$ [27.0, 52.0]	38.6 ± 6.6 [25.6, 51.6]

<sup>451</sup> Superscripts X, Y, and Z represent the sagittal, frontal, and transverse planes, respectively. Ninety degrees represent ankle plantar grade for Angle<sup>X</sup>,

452 with greater values denoting dorsiflexion; positive values represent ankle adduction and internal rotation for Angle<sup>Y</sup> and Angle<sup>Z</sup>, respectively.

453 vGRF, vertical ground reaction force; TTP, time to peak

#### 454 FIGURE 1



455

- 456 Figure 1. The foot positions tested in the present study with reference to the force platform. (A)
- 457 parallel, (B) first, (C) second, (D) fourth back, (E) fourth front, (F) fifth back, (G) fifth front.

458 FIGURE 2

459





#### 462 FIGURE 3



464 Figure 4. A) visualises the individual data and B) visualises the convex hull of the first linear

465 discriminate analysis where seven individual foot positions were included. C) and D) show the 466 results of the second linear discriminate analysis, where the seven foot positions were grouped

- 467 following visual inspection.
- 468 LD, Linear discriminate.



#### 470

471 Figure 4. The canonical coefficients (referred to as absolute proportion) and relative

472 percentage of each canonical coefficient to each linear discriminate (referred to as relative

473 proportion) for the grouped foot positions following the second linear discriminate analysis.

474 The absolute proportion can be used as a regression equation to calculate the linear

475 discriminate value from individual dancer data. The relative proportion provides an

476 understanding of how each variable contributes to the linear discriminate value. Superscripts

477 X, Y, and Z represent the sagittal, frontal, and transverse planes, respectively.

478 LD, Linear discriminate; TTP, Time to peak; vGRF, vertical ground reaction force

#### 479 SUPPLEMENTARY MATERIAL 1

480 The kinetic and kinematic outcome variables that were included in the present study are

outlined in the table below. The X, Y, and Z planes represent the sagittal, frontal, and transverse
planes, respectively.

Variable	Plane
Moment	Х
	Y
	Ζ
Angle	Х
	Y
	Ζ
Power	Х
	Y
	Ζ
Velocity	Х
	Y
	Ζ
Excursion	Х
	Y
	Ζ
Vertical Ground Reaction Force	_
Time to Peak vGRF	-
Loading Rate	-
Jump Height	-

484

## 485 SUPPLEMENTARY MATERIAL 2

### 486 Mean $\pm$ SD [95% CI] of ankle mechanics and vGRF across all foot positions.

	Parallel	First	Second	Fourth Back	Fifth Back	Fourth Front	Fifth Front
Normalised Moment <sup>x</sup>	$0.098 \pm 0.010 \; [0.094,  0.102]$	$0.093 \pm 0.013 \; [0.088,  0.098]$	$0.090 \pm 0.012 \; [0.086,  0.094]$	$0.099 \pm 0.013 \; [0.094, 0.104]$	$0.105\pm0.018\ [0.099,0.112]$	$0.102 \pm 0.020 \; [0.094,  0.109]$	$0.099 \pm 0.016 \ [0.093, \ 0.105]$
Normalised Moment <sup>Y</sup>	$0.017 \pm 0.008 \; [0.014,  0.020]$	$0.008 \pm 0.006 \ [0.006, \ 0.010]$	$0.004 \pm 0.005 \; [0.002,  0.005]$	$0.005 \pm 0.003 \; [0.004,  0.006]$	$0.003 \pm 0.003 \; [0.002,  0.004]$	$0.005 \pm 0.004 \; [0.003,  0.006]$	$0.006 \pm 0.005 \ [0.004, \ 0.008]$
Normalised Moment <sup>Z</sup>	$0.010 \pm 0.005 \ [0.008, \ 0.012]$	$0.005 \pm 0.003 \; [0.004,  0.006]$	$0.004 \pm 0.004 \; [0.003,  0.006]$	$0.001 \pm 0.001 \; [0.001,  0.002]$	$0.002 \pm 0.002 \; [0.001,  0.002]$	$0.005 \pm 0.003 \; [0.004,  0.006]$	$0.005 \pm 0.003 \; [0.004,  0.006]$
Normalised Power <sup>x</sup>	$1.24 \pm 0.20$ [1.17, 1.32]	$1.28 \pm 0.23$ [1.19, 1.36]	$1.20\pm 0.24\ [1.11,\ 1.29]$	$1.19\pm 0.24\ [1.10,\ 1.28]$	$1.25 \pm 0.27$ [1.15, 1.35]	$1.35\pm0.34\;[1.22,1.48]$	$1.31 \pm 0.26$ [1.22, 1.41]
Normalised Power <sup>Y</sup>	$0.10\pm0.05\ [0.09,0.12]$	$0.14\pm0.06\;[0.12,0.17]$	$0.13\pm 0.06\;[0.11,0.15]$	$0.10\pm0.05\;[0.09,0.12]$	$0.15\pm0.09\;[0.12,0.19]$	$0.24\pm0.09\;[0.21,0.28]$	$0.22\pm0.08\;[0.19,0.25]$
Normalised Power <sup>z</sup>	$0.08\pm0.03\;[0.06,0.09]$	$0.09\pm0.03\;[0.08,0.10]$	$0.09\pm0.04\;[0.08,0.11]$	$0.23\pm0.06\;[0.21,0.26]$	$0.21\pm 0.06\ [0.19, 0.24]$	$0.06\pm0.03\;[0.05,0.07]$	$0.06\pm0.02\;[0.05,0.07]$
Velocity <sup>X</sup> ( $^{\circ} \cdot s^{-1}$ )	$907\pm 68\;[881,933]$	941 ± 72 [914, 968]	$949 \pm 89 \ [916, 983]$	923 ± 77 [894, 952]	$942\pm92\ [907,976]$	906 ± 91 [872, 941]	883 ± 86 [851, 916]
Velocity <sup>Y</sup> ( $^{\circ} \cdot s^{-1}$ )	97 ± 48 [79, 115]	88 ± 40 [73, 103]	88 ± 34 [75, 100]	$110 \pm 42$ [94, 126]	97 ± 37 [83, 111]	131 ± 46 [114, 148]	118 ± 50 [100, 137]
Velocity <sup>Z</sup> ( $^{\circ} \cdot s^{-1}$ )	135 ± 50 [116, 154]	171 ± 72 [144, 198]	200 ± 74 [172, 228]	143 ± 54 [122, 163]	151 ± 67 [126, 176]	191 ± 62 [168, 215]	189 ± 60 [166, 211]
Angle <sup>X</sup> (°)	$103 \pm 4$ [101, 104]	$104 \pm 5$ [102, 106]	$102 \pm 4$ [100, 103]	$106 \pm 5 \ [104, 107]$	$107 \pm 4$ [105, 108]	$103 \pm 4$ [101, 105]	104 ± 5 [102, 106]
Angle <sup>Y</sup> (°)	2 ± 3 [1, 3]	-3 ± 3 [-4, -2]	-2 ± 4 [-3, 0]	-3 ± 4 [-5, -1]	-5 ± 4 [-7, -3]	-13 ± 5 [-15, -11]	-13 ± 4 [-15, -11]
Angle <sup>z</sup> (°)	-7 ± 5 [-9, -6]	-4 ± 5 [-6, -2]	-6 ± 4 [-8, -4]	-6 ± 9 [-9, -2]	-3 ± 5 [-5, -1]	7 ± 4 [6, 9]	6 ± 5 [5, 8]
Excursion <sup>x</sup> (°)	64 ± 7 [61, 66]	68 ± 6 [66, 71]	69 ± 5 [67, 71]	67 ± 7 [65, 70]	68 ± 7 [65, 70]	70 ± 6 [68, 72]	70 ± 6 [68, 72]
Excursion <sup>Y</sup> (°)	20 ± 4 [19, 21]	22 ± 4 [20, 23]	21 ± 4 [20, 23]	24 ± 4 [22, 25]	24 ± 5 [22, 25]	20 ± 5 [18, 22]	$20 \pm 4$ [18, 21]
Excursion <sup>z</sup> (°)	11 ± 4 [10, 13]	16 ± 5 [14, 18]	15 ± 6 [13, 17]	17 ± 5 [15, 19]	18 ± 6 [16, 21]	21 ± 6 [18, 23]	20 ± 7 [18, 23]
vGRF (BW)	$1.94 \pm 0.45 \ [1.77,  2.11]$	$1.92\pm0.47\ [1.74,2.10]$	$2.17\pm 0.61\; [1.94, 2.40]$	$1.88 \pm 0.36 \ [1.75,  2.02]$	$1.92\pm0.42\;[1.76,2.07]$	$2.16\pm 0.60\; [1.93, 2.39]$	$1.91 \pm 0.54  [1.71,  2.12]$
TTP vGRF (s)	$0.09\pm0.02\;[0.08,0.10]$	$0.08\pm0.02\;[0.07,0.09]$	$0.09\pm0.02\;[0.08,0.09]$	$0.08 \pm 0.03 \; [0.07,  0.09]$	$0.09\pm0.02\;[0.08,0.10]$	$0.09\pm0.01\;[0.08,0.09]$	$0.09\pm0.02\;[0.08,0.09]$
Loading rate (BW $\cdot$ s <sup>-1</sup> )	26.9 ± 13.3 [21.9, 32.0]	29.6 ± 13.1 [24.6, 34.5]	31.3 ± 17.0 [24.9, 37.7]	33.6 ± 20.2 [25.9, 41.2]	28.0 ± 17.6 [21.4, 34.7]	27.2 ± 10.1 [23.4, 31.0]	$25.8 \pm 13.4 \ [20.8,  30.9]$
Jump height (cm)	42.2 ± 7.7 [39.2, 45.1]	$40.7\pm7.1[38.0,43.4]$	$38.4 \pm 6.7 \; [35.9,  40.9]$	$40.0\pm 6.5\;[37.6,42.5]$	$39.0 \pm 6.3 \; [36.6, 41.3]$	$38.4\pm 6.6\;[35.9,40.8]$	$38.9\pm 6.8\;[36.4,41.5]$

## 488 SUPPLEMENTARY MATERIAL 3

489 Mean  $\pm$  SD [95% CI] of ankle mechanics and vGRF across women and men.

	Women	Men
Moment <sup>x</sup>	0.092 ± 0.013 [0.085 ,0.099]	0.103 ± 0.016 [0.095 ,0.111]
Moment <sup>v</sup>	0.006 ± 0.006 [0.003 ,0.009]	0.007 ± 0.007 [0.003 ,0.011]
Moment <sup>z</sup>	0.004 ± 0.004 [0.002 ,0.006]	0.005 ± 0.004 [0.003 ,0.007]
Power <sup>x</sup>	1.17 ± 0.22 [1.05 ,1.29]	1.34 ± 0.26 [1.21 ,1.48]
Power <sup>v</sup>	0.14 ± 0.07 [0.10 ,0.18]	0.17 ± 0.09 [0.12 ,0.22]
Power <sup>z</sup>	0.12 ± 0.08 [0.07 ,0.16]	0.12 ± 0.08 [0.08 ,0.16]
Velocity <sup>x</sup>	922 ± 68 [885 ,960]	921 ± 97 [870 ,972]
Velocity <sup>Y</sup>	105 ± 47 [79 ,130]	103 ± 42 [81 ,126]
Velocity <sup>z</sup>	178 ± 72 [138 ,217]	161 ± 60 [129 ,192]
Angle <sup>x</sup>	105 ± 5 [102 ,107]	103 ± 4 [101 ,106]
Angle <sup>v</sup>	-5 ± 7 [-9 ,-1]	-5 ± 6 [-8 ,-2]
Angle <sup>z</sup>	-3 ± 7 [-7 ,1]	-1 ± 9 [-5 ,4]
Excursion <sup>x</sup>	70 ± 5 [67 ,73]	66 ± 7 [62, 70]
Excursion <sup>Y</sup>	21 ± 5 [18 ,23]	22 ± 3 [20 ,24]
Excursion <sup>z</sup>	16 ± 6 [13 ,19]	18 ± 7 [14 ,21]
vGRF	1.88 ± 0.43 [1.65 ,2.12]	2.08 ± 0.55 [1.79 ,2.37]
TTP vGRF	0.09 ± 0.02 [0.08 ,0.10]	0.08 ± 0.02 [0.07 ,0.09]
Loading rate	25.9 ± 14.9 [17.8 ,34.0]	31.7 ± 15.1 [23.8 ,39.6]
Jump height	33.6 ± 3.3 [31.8 ,35.4]	45.3 ± 3.9 [43.2 ,47.3]

#### 491 DISCLOSURES

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- 506
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- 511